

Supplementary file

Article's Title;

A new intestinal model for analysis of drug absorption and interactions considering physiological translocation of contents

Authors;

Satoshi Asano, Aoi Yoshitomo, Shizuka Hozuki, Hiromi Sato, Yasuhiro Kazuki, and Akihiro Hisaka

Journal Title;

Drug Metabolism and Disposition

Supplementary text 1

Model construction in esophagus, stomach, enterocytes, lamina propria, portal vein, central and peripheral compartment

In ATOM, the concentration profiles of drugs in the tissues except for the intestine are expressed by the following differential equations S1-8.

Esophagus:

$$\frac{dC_{es}}{dt} = -k_{es}C_{es} \quad (S1)$$

Stomach:

$$\frac{dC_{sto}}{dt} = k_{es}C_{es}V_{es}/V_{sto} - k_{sto}C_{sto} \quad (S2)$$

where C_{es} , C_{sto} , k_{es} , k_{sto} , V_{es} , and V_{sto} represent drug concentrations, elimination rate constants, and volumes for the esophagus and stomach, respectively. At the initial condition, all doses and drinking water were located in the esophagus. It was assumed that the drinking water does not change the volumes in the esophagus and stomach and moves with the drug in accordance with equations S1 and S2. k_{es} and k_{sto} were used in both drugs and water simulations because their movements were assumed to be the same in the esophagus and stomach.

Enterocytes and lamina propria:

$$\frac{\partial C_{ent,z}}{\partial t} = PS_{a,in,z} \frac{f_{lum}C_{lum,z}V_{lum}}{V_{water}+V_{lum}} - (PS_{a,out,z} + CL_{ent,z} + PS_{b,out,z})f_{ent}C_{ent,z} + f_{pro}PS_{b,in,z}C_{pro,z} \quad (S3)$$

$$\frac{\partial C_{pro,z}}{\partial t} = PS_{b,in,z}f_{ent}C_{ent,z} - \left(\frac{Q_{pro,z}}{f_b} + f_{pro}PS_{b,in,z}\right)C_{pro,z} \quad (S4)$$

where $C_{pro,z}$ is the drug concentration in the lamina propria, including blood capillaries at location z . $PS_{b,in,z}$ and $PS_{b,out,z}$ are the permeability clearance of reuptake from the lamina propria to enterocytes and of efflux from enterocytes to lamina propria, respectively, via the basolateral membrane at location z . $CL_{ent,z}$ represents intestinal intrinsic clearance in enterocytes at location z . $Q_{pro,z}$ represents blood flow of the blood capillaries in the lamina propria at location z . f_{ent} and f_{pro} represent the unbound fraction of the drug in the enterocytes and lamina propria, respectively. f_{pro} was assumed to be 1. In this study, f_{ent} values were tentatively assumed to be equal to f_b . However, it does not affect the availability as shown in a sensitivity analysis of f_{ent} values on availability of midazolam in a linear condition (Supplemental Fig. 5).

Portal vein and liver:

$$V_{pv} \frac{dC_{pv}}{dt} = \sum_z \frac{Q_{pro,z}}{f_b} C_{pro,z} - Q_{pv} C_{pv} \quad (S5)$$

$$V_{liver} \frac{dC_{liver}}{dt} = R_B (Q_{pv} C_{pv} + Q_{ha} C_p) - \left(\frac{R_B (Q_{pv} + Q_{ha})}{K_{p,liver}} + f_h CL_{int} \right) C_{liver} \quad (S6)$$

where C_p , C_{pv} , V_{pv} , and Q_{pv} represent plasma concentration in systemic circulation, plasma concentration, volume, and blood flow in the portal vein, respectively. C_{liver} , V_{liver} , and Q_{ha} represent drug concentration, volume, and blood flow in the liver and blood flow in the hepatic artery, respectively. R_B , $K_{p,liver}$, f_h , and CL_{int} represent the blood/plasma partition coefficient, liver/plasma partition coefficient, unbound fraction in the liver and hepatic intrinsic clearance, respectively.

Central and peripheral compartments:

$$V_d \frac{dC_p}{dt} = \frac{R_B(Q_{pv}+Q_{ha})}{K_{p,liver}} C_{liver} + \sum_{i=1}^n k_{i1} X_{peri,i} - (R_B Q_{ha} + \sum_{i=1}^n k_{1i} + CL_R) C_p \quad (S7)$$

$$\frac{dX_{peri,i}}{dt} = k_{1i} V_d C_p - k_{i1} X_{peri,i}$$

($i = 0$ for itraconazole, $i = 1$ for midazolam and clarithromycin, $i = 2$ for digoxin) (S8).

where V_d and CL_R represent the distribution volume in the central compartment (rapid equilibrium is assumed between plasma concentration) and renal plasma clearance, respectively. For peripheral compartments, $X_{peri,i}$ is the drug amount in the i -th peripheral compartment, and k_{1i} and k_{i1} represent distribution constants from the central to peripheral compartment and peripheral to central compartment, respectively. CL_R is the sum of renal clearance mediated by P-gp ($CL_{R,Pgp}$) and that by other mechanisms ($CL_{R,nonPgp}$).

Model structure of the intestine in ATOM and CAT

CYP3A and P-gp expression levels in each location, pH changes in the lumen, surface area in enterocytes, volume of enterocytes and lamina propria, and blood flow in the lamina propria were shown using equations S9-15. The relative P-gp expression level in each location was shown because the absolute P-gp amount was not reported. Blood flow in the lamina propria (Q_{pro}) was assumed to be 18,000 mL/h, which assumes that the blood flow into the superior mesenteric artery is 37,200 mL/h accounting for 10% of the cardiac output, and 80 % of the blood flow of the superior mesenteric artery flows into the mucosa, and then 60% of the mucosal blood flows into the epithelial cells of the villi (Jamei et al., 2009)

CYP3A expression:

$$\text{Exp}_{\text{CYP3A},z} = \frac{\text{Exp}_{\text{CYP3A,whole}}}{L_{\text{si}}} \left(1 - \frac{z}{L_{\text{si}}}\right) \quad (\text{S9})$$

Relative P-gp expression:

$$\text{Exp}_{\text{Pgp},z} = \frac{\text{Exp}_{\text{Pgp,whole}}}{L_{\text{si}}} \left(\frac{z}{L_{\text{si}}}\right) \quad (\text{S10})$$

pH changes in the lumen:

$$\text{pH}_{\text{lumen},z} = 5.85 + \text{pH}_{\text{grad}} \frac{z}{L_{\text{si}}} \quad (\text{S11})$$

Surface area in enterocytes:

$$S_{\text{ent},z} = \pi(r_{\text{in}} + r_z) \sqrt{(r_{\text{in}} - r_z)^2 + L_z^2} \text{ PE VE} \quad (\text{S12})$$

Volume of enterocytes:

$$V_{\text{ent},z} = S_{\text{ent},z} T_{\text{ent}} \quad (\text{S13})$$

Volume of lamina propria:

$$V_{\text{lam},z} = \frac{S_{\text{ent}} H_{\text{villi}}}{\text{VE}} - V_{\text{ent},z} \quad (\text{S14})$$

Blood flow in lamina propria:

$$Q_{\text{pro},z} = Q_{\text{pro}} \frac{S_{\text{ent},z}}{S_{\text{ent,whole}}} \quad (\text{S15})$$

where L_{si} , $\text{Exp}_{\text{CYP3A,whole}}$, $\text{Exp}_{\text{Pgp,whole}}$, and r_{in} represent the total normalized length of the intestine ($L_{\text{si}} = 1$), the total expression level of CYP3A and P-gp in the intestine, and radius in the inlet of the small intestine, respectively. z is within the range of 0 and L_{si} ($0 \leq z \leq L_{\text{si}} = 1$).

PE, VE, H_{villi}, S_{ent,whole}, T_{ent}, and ME represent plicate expansion, villi expansion, height of villi, total surface area of enterocytes, height of enterocytes, and microvilli expansion, respectively. The absolute expression level of P-gp has not been clearly reported; therefore, it was expressed as a relative expression level and the whole expression level was set to 1. The values of these parameters were obtained from the previous report by Ando et al. (2015).

Membrane permeability model between *in vitro* and *in vivo*

Equations S16-19 were used to calculate *in vivo* permeability coefficients from *in vitro* permeability using the concept shown in Supplemental Fig. 4, which was same with TLM (Ando et al., 2015). Apparent permeability in Caco-2 cells (P_{app,Caco-2}) was transferred into the permeability of a single membrane (P_{s,Caco-2}) using equation S16 from the previous report by Gertz et al. (2010).

$$P_{s,Caco-2} = \frac{1+ME_{Caco-2}}{ME_{Caco-2}} P_{app,Caco-2} \quad (S16)$$

where ME_{Caco-2} represents the surface area ratio in apical and basolateral membranes in Caco-2 cells and was set as 4 based on a previous report by Ohura et al. (2011).

Then, *in vivo* membrane permeability (P_{in vivo}) was calculated from P_{s,Caco-2} using equation S17.

$$P_{in\ vivo} = P_{s,Caco-2} \text{ psf}_{passive} \quad (S17)$$

where psf_{passive} represents a scaling factor regarding the difference in passive transport between *in vitro* and *in vivo*, which was obtained from approximation of the simulated and reported F_A , and psf_{passive} was set as 2.23 based on the previous report by Ando et al. (2015).

According to the definition of membrane permeability clearance in apical and basolateral membranes (Supplemental Fig. 4), $P_{\text{in vivo}}$ is equal to the passive permeability from cells to apical side (P_2), from cells to basolateral side (P_3), and from basolateral side to cells (P_4) (equation S18).

$$P_{\text{in vivo}} = P_2 = P_3 = P_4 \quad (\text{S18})$$

On the other hand, pH values in the lumen are lower than those in the enterocytes (pH 7.4), which leads to changes in the ionized fraction of the drug, depending on pKa values. In this study, it was assumed that the drug transported by passive diffusion is nonionic. Therefore, for P_1 , the membrane permeation coefficient depending on the pKa values of the drug and the pH gradients in both the lumen and enterocytes was calculated according to equation S19.

$$P_{1,z} = P_{\text{in vivo}} \frac{1 + 10^{\text{pH}_{\text{Caco-2}} - \text{pK}_{\text{aacid}} + 10^{\text{pK}_{\text{abase}} - \text{pH}_{\text{Caco-2}}}}{1 + 10^{\text{pH}_{\text{lumen,z}} - \text{pK}_{\text{aacid}} + 10^{\text{pK}_{\text{abase}} - \text{pH}_{\text{lumen,z}}}} \quad (\text{S19})$$

where $P_{1,z}$, $\text{pH}_{\text{Caco-2}}$, pK_{aacid} , and pK_{abase} represent P_1 at position z , pH in Caco-2, acid pKa, and base pKa of the drug, respectively. In this study, $\text{pH}_{\text{Caco-2}}$ was assumed to be 7.4.

Permeability on the apical ($P_{1,z}$, and P_2) and basolateral sides (P_3 and P_4) can be transferred into permeability clearance (PS) using equations S20-24.

$$PS_{\text{a,in,z}} = P_{1,z} S_{\text{abs,api}} \quad (\text{S20})$$

$$PS_{a,out,z} = P_2 S_{abs,api} + PS_{a,Pgp,z} \quad (S21)$$

$$PS_{b,in,z} = P_3 S_{abs,bas} \quad (S22)$$

$$PS_{b,out,z} = P_4 S_{abs,bas} \quad (S23)$$

$$S_{abs,api} = ME_{in\ vivo} S_{abs,bas} \quad (S24)$$

where $S_{abs,api}$, $S_{abs,bas}$, $PS_{a,Pgp,z}$, and $ME_{in\ vivo}$ represent the surface area on the apical side, surface area on the basolateral side, transport clearance by P-gp, and surface area ratio between apical and basolateral side in humans, respectively. In this study, $ME_{in\ vivo}$ was set to 20. $PS_{a,Pgp,z}$, and intrinsic clearance by CYP3A ($CL_{ent,z}$) in enterocytes were calculated using equations S25 and S26.

$$PS_{a,Pgp,z} = \frac{V_{max,Pgp} Exp_{Pgp,z} psf_{Pgp}}{K_{m,Pgp,u} + C_{ent,z}} \quad (S25)$$

$$CL_{ent,z} = \frac{V_{max,CYP3A} Exp_{CYP3A,z} psf_{CYP3A}}{K_{m,CYP3A,u} + C_{ent,z}} \quad (S26)$$

where $V_{max,Pgp}$, $V_{max,CYP3A}$, $K_{m,Pgp,u}$, $K_{m,CYP3A,u}$, psf_{Pgp} , and psf_{CYP3A} represent V_{max} for P-gp and CYP3A, K_m values based on unbound concentrations for P-gp and CYP3A, the scaling factor for transport clearance by P-gp, and intrinsic clearance by CYP3A between *in vitro* and *in vivo*, respectively. In this study, psf_{CYP3A} was assumed to be 1. Therefore, the scaling

factors used in ATOM are only $psf_{passive}$ and psf_{pgp} . The values of these parameters above were obtained from a previous report by Ando et al. (2015).

Parameter estimation of water distribution in the stomach and intestine

Water distribution was simulated in both ATOM and ACAT models by optimizing the secretion clearance and absorption rate using the reported water distribution in the stomach and small intestine after water intake by Mudie et al. (2014). Equations S27-29 were used for the simulation of water movement. The initial water volume was also obtained from the same report.

Esophagus:

$$\frac{dX_{water,es}}{dt} = -k_{es}X_{water,es} \quad (S27)$$

Stomach:

$$\frac{dX_{water,sto}}{dt} = k_{es}X_{water,es}V_{es}/V_{sto} - k_{sto}X_{water,sto} - k_{water,sto}X_{water,z} + Se_{water,sto} \quad (S28)$$

Lumen:

$$\frac{\partial X_{lum,z}}{\partial t} = D_z \frac{\partial^2 X_{lum,z}}{\partial z^2} - M_t \frac{\partial X_{lum,z}}{\partial z} - k_{water,abs}X_{water,z} + Se_{water,abs} \quad (S29)$$

where $X_{water,es}$, $X_{water,sto}$, and $X_{water,z}$ represent the amount of inflating water in the esophagus, stomach, and lumen at position z , respectively. k_{es} , k_{sto} , V_{es} , and V_{sto} represent the transit rate of drug (or water) from the esophagus to the stomach, from the stomach to the small

intestine, and volume of the esophagus and stomach, respectively. $k_{\text{water,sto}}$ and $k_{\text{water,abs}}$ are the water absorption rates in the stomach and lumen, respectively. $Se_{\text{water,sto}}$ and $Se_{\text{water,abs}}$ are water secretion clearances in the stomach and lumen, respectively. The transit rate from the esophagus to the stomach (k_{es}), water absorption rate ($k_{\text{water,sto}}$ and k_{water}), and secretion clearance ($Se_{\text{water,sto}}$ and $Se_{\text{water,z}}$) were optimized using reported luminal water volume after oral intake of 240 mL water as reported by Mudie et al. (2014). The simulated water distribution and estimated parameters are shown in Supplemental Fig. 1 and Table S1, respectively.

Sensitivity analysis of f_{ent} on the accumulation of midazolam into the portal vein in a linear condition

Sensitivity analysis of f_{ent} on drug accumulation into the portal vein was performed using pharmacokinetic parameters of midazolam with different f_{ent} values ($f_{\text{ent}} = 1, 0.5, 0.1$ and 0.01) at 0.001 mg. Simulation conditions were same with the ones in Fig. 6. In the simulation, the optimized dispersion numbers and intestinal flow rates determined using the $^{99\text{m}}\text{Tc}$ -DTPA distribution of subject A (Haruta et al., 2002) were used shown in Fig. 2A.

Estimation of pharmacokinetic parameters of midazolam, digoxin, itraconazole and clarithromycin

Distribution constants between central and peripheral compartments (k_{12} and k_{21}), distribution volume in the central compartment (V_{central}) and hepatic intrinsic clearance (CL_{int}) were optimized using the plasma concentration profile of midazolam after intravenous injection as reported by Link et al. (2008).

Regarding digoxin, V_{max} for P-gp ($V_{\text{max,Pgp}}$) was optimized by a fitting analysis to the reported F_A value in a previous report by Elmeliegy et al. (2020). Distribution constants (k_{12} ,

k_{13} , k_{21} , k_{31}) were optimized using the reported plasma concentration profile of digoxin after intravenous injection as reported by Ding et al. (2004).

Regarding itraconazole, no peripheral compartment model was applied, according to the previous report by Kudo et al. (2013). The optimization process for obtaining pharmacokinetic parameters was not conducted because all parameters were obtained from the previous reports or in silico software. Observed plasma concentration profile of itraconazole was not shown in the DI study with midazolam (Templeton et al., 2010). Therefore, the reported plasma concentration profile of itraconazole 3 days after oral administration of 100 mg twice daily in another study (Jakkola et al., 2015) was adopted for verification for predicting plasma concentration of itraconazole (Supplemental Fig. 6A).

Distribution volume in central compartment (V_{central}) were optimized using reported plasma concentration profile of clarithromycin after intravenous injection (Lappin et al., 2011). Distribution constants and intrinsic clearance of clarithromycin (k_{12} , k_{21} , CL_{int}) in oral administration were thought to be independent of that in intravenous administration because the distribution and elimination phase could not be reproduced using optimized parameters using the plasma concentration profile of clarithromycin in intravenous dosing as reported by Lappin et al. (2011). Hence, in this study, these parameters were directly optimized using the plasma concentration of clarithromycin after oral dosing. Unbound fraction in the liver (f_h) was calculated using equations S30 and S31 according to the previous reports by Kudo et al. (2013) and Poulin et al. (2002).

$$K_{p,\text{liver}} = \frac{0.02289 \cdot P + 0.72621}{0.001719 \cdot P + 0.960581} \cdot f_p / f_h \quad (\text{S30})$$

$$P = 10^{\text{Log}P} \quad (\text{S31})$$

where $K_{p,liver}$ and LogP represent liver/plasma partition coefficient and logarithm partition coefficient, respectively. Reported plasma concentration profile of clarithromycin 2 days after oral administration of 250 mg twice daily (Rengelshausen et al., 2003) was adopted for verification for predicting plasma concentration of clarithromycin (Supplemental Fig. 6B).

References for Supplementary text

1. Jamei M, Turner D, Yang J, Neuhoff S, Polak S, Rostami-Hodjegan A, Tucker G (2009) Population-based mechanistic prediction of oral drug absorption. *AAPS J.* **11**(2):225-237.
2. Ando H, Hisaka A, Suzuki H (2015) A new physiologically based pharmacokinetic model for the prediction of gastrointestinal drug absorption: translocation model. *Drug Metab Dispos.* **43**(4):590-602.
3. Asaumi R, Toshimoto K, Tobe Y, Hashizume K, Nunoya KI, Imawaka H, Lee W, Sugiyama Y (2018) Comprehensive PBPK Model of Rifampicin for Quantitative Prediction of Complex Drug-Drug Interactions: CYP3A/2C9 Induction and OATP Inhibition Effects. *CPT Pharmacometrics Syst Pharmacol.* **7**(3):186-196.
4. Gertz M, Harrison A, Houston JB, Galetin A (2010) Prediction of human intestinal first-pass metabolism of 25 CYP3A substrates from in vitro clearance and permeability data. *Drug Metab Dispos.* **38**(7):1147-1158.
5. Link B, Haschke M, Grignaschi N, Bodmer M, Aschmann YZ, Wenk M, Krähenbühl S (2008) Pharmacokinetics of intravenous and oral midazolam in plasma and saliva in humans: usefulness of saliva as matrix for CYP3A phenotyping. *Br J Clin Pharmacol.* **66**(4):473-484.
6. Lin X, Skolnik S, Chen X, Wang J (2011) Attenuation of intestinal absorption by major efflux transporters: quantitative tools and strategies using a Caco-2 model. *Drug Metab Dispos.* **39**(2):265-274.
7. Elmeliegy M, Vourvahis M, Guo C, Wang DD (2020) Effect of P-glycoprotein (P-gp) Inducers on Exposure of P-gp Substrates: Review of Clinical Drug-Drug Interaction Studies. *Clin Pharmacokinet.* **59**(6):699-714.

8. Collett A, Tanianis-Hughes J, Hallifax D, Warhurst G (2004) Predicting P-glycoprotein effects on oral absorption: correlation of transport in Caco-2 with drug pharmacokinetics in wild-type and *mdr1a(-/-)* mice in vivo. *Pharm Res.* **21**(5):819-826.
9. Neuhoff S, Yeo KR, Barter Z, Jamei M, Turner DB, Rostami-Hodjegan A (2013) Application of permeability-limited physiologically-based pharmacokinetic models: part I-digoxin pharmacokinetics incorporating P-glycoprotein-mediated efflux. *J Pharm Sci.* **102**(9):3145-60.
10. Ding R, Tayrouz Y, Riedel KD, Burhenne J, Weiss J, Mikus G, Haefeli WE (2004) Substantial pharmacokinetic interaction between digoxin and ritonavir in healthy volunteers. *Clin Pharmacol Ther.* **76**(1):73-84.
11. Rengelshausen J, Göggelmann C, Burhenne J, Riedel KD, Ludwig J, Weiss J, Mikus G, Walter-Sack I, Haefeli WE (2003) Contribution of increased oral bioavailability and reduced nonglomerular renal clearance of digoxin to the digoxin-clarithromycin interaction. *Br J Clin Pharmacol.* **56**(1):32-38.
12. Berben P, Brouwers J, Augustijns P (2018) Assessment of Passive Intestinal Permeability Using an Artificial Membrane Insert System. *J Pharm Sci.* **107**(1):250-256.
13. Isoherranen N, Kunze KL, Allen KE, Nelson WL, Thummel KE (2004) Role of itraconazole metabolites in CYP3A4 inhibition. *Drug Metab Dispos.* **32**(10):1121-1131.
14. Kudo T, Hisaka A, Sugiyama Y, Ito K (2013) Analysis of the repaglinide concentration increase produced by gemfibrozil and itraconazole based on the inhibition of the hepatic uptake transporter and metabolic enzymes. *Drug Metab Dispos.* **41**(2):362-371.
15. Nožinić D, Milić A, Mikac L, Ralić J, Padovan J, Antolović R (2010) Assessment of Macrolide Transport Using PAMPA, Caco-2 and MDCKII-hMDR1 Assays. *Croat Chem Acta.* **83**(3): 323-331.

16. Yoshikado T, Maeda K, Kusuvara H, Furihata KI, Sugiyama Y (2017) Quantitative Analyses of the Influence of Parameters Governing Rate-Determining Process of Hepatic Elimination of Drugs on the Magnitudes of Drug-Drug Interactions via Hepatic OATPs and CYP3A Using Physiologically Based Pharmacokinetic Models. *J Pharm Sci.* **106**(9):2739-2750.
17. Hanke N, Frechen S, Moj D, Britz H, Eissing T, Wendl T, Lehr T (2018) PBPK Models for CYP3A4 and P-gp DDI Prediction: A Modeling Network of Rifampicin, Itraconazole, Clarithromycin, Midazolam, Alfentanil, and Digoxin. *CPT Pharmacometrics Syst Pharmacol.* **7**(10):647-659.
18. Moj D, Hanke N, Britz H, Frechen S, Kanacher T, Wendl T, Haefeli WE, Lehr T (2017) Clarithromycin, Midazolam, and Digoxin: Application of PBPK Modeling to Gain New Insights into Drug-Drug Interactions and Co-medication Regimens. *AAPS J.* **19**(1):298-312.
19. Quinney SK, Zhang X, Lucksiri A, Gorski JC, Li L, Hall SD (2010) Physiologically based pharmacokinetic model of mechanism-based inhibition of CYP3A by clarithromycin. *Drug Metab Dispos.* **38**(2):241-248.
20. Lappin G, Shishikura Y, Jochemsen R, Weaver RJ, Gesson C, Brian Houston J, Oosterhuis B, Bjerrum OJ, Gryniewicz G, Alder J, Rowland M, Garner C (2011) Comparative pharmacokinetics between a microdose and therapeutic dose for clarithromycin, sumatriptan, propafenone, paracetamol (acetaminophen), and phenobarbital in human volunteers. *Eur J Pharm Sci.* **43**(3):141-150.
21. Ohura K, Nozawa T, Murakami K, Imai T (2011) Evaluation of transport mechanism of prodrugs and parent drugs formed by intracellular metabolism in Caco-2 cells with modified carboxylesterase activity: temocapril as a model case. *J Pharm Sci.* **100**(9):3985-3994.

22. Mudie DM, Murray K, Hoad CL, Pritchard SE, Garnett MC, Amidon GL, Gowland PA, Spiller RC, Amidon GE, Marciani L (2014) Quantification of gastrointestinal liquid volumes and distribution following a 240 mL dose of water in the fasted state. *Mol Pharm.* **11**(9):3039-3047.
23. Poulin P, Theil FP (2002) Prediction of pharmacokinetics prior to in vivo studies. II. Generic physiologically based pharmacokinetic models of drug disposition. *J Pharm Sci.* **91**(5):1358-1370.
24. Rodrigues AD, Roberts EM, Mulford DJ, Yao Y, Ouellet D (1997) Oxidative metabolism of clarithromycin in the presence of human liver microsomes. Major role for the cytochrome P4503A (CYP3A) subfamily. *Drug Metab Dispos.* **25**(5):623-630.
25. Heikkinen AT, Baneyx G, Caruso A, Parrott N (2012) Application of PBPK modeling to predict human intestinal metabolism of CYP3A substrates - an evaluation and case study using GastroPlus. *Eur J Pharm Sci.* **47**(2):375-386.
26. Prueksaritanont T, Gorham LM, Ma B, Liu L, Yu X, Zhao JJ, Slaughter DE, Arison BH, Vyas KP (1997) In vitro metabolism of simvastatin in humans [SBT]identification of metabolizing enzymes and effect of the drug on hepatic P450s. *Drug Metab Dispos.* **25**(10):1191-1199.
27. Haruta S, Kawai K, Nishii R, Jinnouchi S, Ogawara Ki, Higaki K, Tamura S, Arimori K, Kimura T (2002) Prediction of plasma concentration-time curve of orally administered theophylline based on a scintigraphic monitoring of gastrointestinal transit in human volunteers. *Int J Pharm.* **21**;233(1-2):179-190.
28. Watari R, Kakiki M, Yamasaki C, Ishida Y, Tateno C, Kuroda Y, Ishida S, Kusano K (2019) Prediction of Human Hepatic Clearance for Cytochrome P450 Substrates via a New Culture Method Using the Collagen Vitrigel Membrane Chamber and Fresh Hepatocytes Isolated from Liver Humanized Mice. *Biol Pharm Bull.* **42**(3):348-353.

29. Jaakkola T, Backman JT, Neuvonen M, Neuvonen PJ (2005) Effects of gemfibrozil, itraconazole, and their combination on the pharmacokinetics of pioglitazone. *Clin Pharmacol Ther.* **77**(5):404-414.
30. Takano J, Maeda K, Bolger MB, Sugiyama Y (2016) The Prediction of the Relative Importance of CYP3A/P-glycoprotein to the Nonlinear Intestinal Absorption of Drugs by Advanced Compartmental Absorption and Transit Model. *Drug Metab Dispos.* **44**(11):1808-1818.
31. Schiller C, Fröhlich CP, Giessmann T, Siegmund W, Mönnikes H, Hosten N, Weitschies W (2005) Intestinal fluid volumes and transit of dosage forms as assessed by magnetic resonance imaging. *Aliment Pharmacol Ther.* **22**(10):971-979.
32. Poirier A, Cascais AC, Bader U, Portmann R, Brun ME, Walter I, Hillebrecht A, Ullah M, Funk C (2014) Calibration of in vitro multidrug resistance protein 1 substrate and inhibition assays as a basis to support the prediction of clinically relevant interactions in vivo. *Drug Metab Dispos.* **42**(9):1411-1122.
33. Templeton I, Peng CC, Thummel KE, Davis C, Kunze KL, Isoherranen N (2010) Accurate prediction of dose-dependent CYP3A4 inhibition by itraconazole and its metabolites from in vitro inhibition data. *Clin Pharmacol Ther.* **88**(4):499-505.
34. Heizmann P, Eckert M, Ziegler WH (1983) Pharmacokinetics and bioavailability of midazolam in man. *Br J Clin Pharmacol.* **16** Suppl 1(Suppl 1):43S-49S.
35. Prueksaritanont T, Gorham LM, Ma B, Liu L, Yu X, Zhao JJ, Slaughter DE, Arison BH, Vyas KP (1997) In vitro metabolism of simvastatin in humans [SBT]identification of metabolizing enzymes and effect of the drug on hepatic P450s. *Drug Metab Dispos.* **25**(10):1191-1199.

Legends for Supplementary Figures

Supplemental Fig. 1 Prediction of intestinal water profile in the stomach and small intestine after a water intake of 240 mL.

Open and closed circles represent the observed water volume in the stomach and whole intestine, respectively, as reported by Mudie et al. (2014). Initial values in the stomach and small intestine were also obtained from the same report. Optimized parameters in this analysis are shown in Supplemental Table S1.

Supplemental Fig. 2 Simulated movements of ^{99m}Tc -DTPA in the gastrointestinal tract by ATOM with fixed dispersion number.

In panel A, open circles, closed circles, open squares, and open triangles represent the observed distributions in the stomach, upper intestine, lower intestine, and caecum/colon, respectively. The observed ^{99m}Tc -DTPA distribution in the lumen was obtained from a previous report by Haruta et al. (2002), which reported its distribution in two subjects. In this analysis, the observed ^{99m}Tc -DTPA distribution in the small intestine of subject A in the fasted state was used. The lines represent the simulated ^{99m}Tc -DTPA distributions in each organ. In ATOM, distributions at 40 locations were simulated, and 24 segments were assigned in the upper intestine and the other 16 segments in the lower intestine corresponding to the CATmodel using the index of the length from the inlet in the intestine. In panel B, the fixed dispersion number was optimized by fitting analysis using the luminal ^{99m}Tc -DTPA distribution of subject A in the fasted condition. The fixed dispersion number was optimized as 0.812.

Supplemental Fig. 3 Simulated movements of ^{99m}Tc -DTPA in the gastrointestinal tract using CAT model with the reported transit times to the observed distribution.

Reported transit times were referenced from a previous report by Heikkinen et al. (2012), as shown in Supplemental Table S3. Open circles, closed circles, open squares and open triangles represent the observed ^{99m}Tc -DTPA distributions in the stomach, upper intestine, lower intestine and caecum/colon, respectively, as reported by Haruta et al. (2002). The lines represent the simulated ^{99m}Tc -DTPA distributions in each organ. CAT model assumes that the small intestine is divided into six portions.

Supplemental Fig. 4 Definitions of apical and basolateral permeability.

$S_{\text{abs,api}}$ and $S_{\text{abs,bas}}$ represent the surface areas of the apical and basolateral membranes, respectively. P_1 , P_2 , P_3 , and P_4 represent the passive permeability from the lumen to enterocytes, enterocytes to the lumen, enterocytes to the lamina propria and blood capillaries, and blood capillaries to enterocytes, respectively. P_{Pgp} represents the active transport clearance of P-gp.

Supplemental Fig. 5 Effect of f_{ent} on the midazolam accumulation into the portal vein in linear conditions.

Red, blue, black and green lines represent the cumulative transfer of midazolam with $f_{\text{ent}} = 1$, 0.5, 0.1 and 0.01 into the portal vein simulated by ATOM with optimized transit times, respectively. Dose was set to 0.001 mg. The simulation was performed in the same condition with the one used in the analysis of Fig. 6.

Supplemental Fig. 6 Plasma concentration of itraconazole (A) and clarithromycin (B) in DI simulations.

In panel A, solid line represents the predicted blood concentration of itraconazole after oral administration of 100 mg twice daily. Solid circle symbol and error bars represent the mean

plasma concentration of itraconazole and the SDs reported by Jakkola et al. (2015). In panel B, solid line represents predicted plasma concentration of clarithromycin after oral administration of 250 mg twice daily. Solid circle symbol and error bars represent the mean plasma concentration of clarithromycin and the SDs reported by Rengelshausen et al. (2003).

Supplementary text 2

; Model equations used in ATOM

; Main model equation: Line 7 - 2252

; Preparative calculation equation: Line 2245 - 2845

@at 0:

; Initial water volume in the first location of the intestine

$$y1 = Wvol_int_up_r/3,$$

$$y2 = Wvol_int_up_r/3,$$

$$y3 = Wvol_int_up_r/3,$$

; Initial water volume in the second location of the intestine

$$y4 = Wvol_int_up_l/11,$$

$$y5 = Wvol_int_up_l/11,$$

$$y6 = Wvol_int_up_l/11,$$

$$y7 = Wvol_int_up_l/11,$$

$$y8 = Wvol_int_up_l/11,$$

$$y9 = Wvol_int_up_l/11,$$

$$y10 = Wvol_int_up_l/11,$$

$$y11 = Wvol_int_up_l/11,$$

$$y12 = Wvol_int_up_l/11,$$

$$y13 = Wvol_int_up_l/11,$$

$$y14 = Wvol_int_up_l/11,$$

; Initial water volume in the third location of the intestine

y15=Wvol_int_low_l/18,

y16=Wvol_int_low_l/18,

y17=Wvol_int_low_l/18,

y18=Wvol_int_low_l/18,

y19=Wvol_int_low_l/18,

y20=Wvol_int_low_l/18,

y21=Wvol_int_low_l/18,

y22=Wvol_int_low_l/18,

y23=Wvol_int_low_l/18,

y24=Wvol_int_low_l/18,

y25=Wvol_int_low_l/18,

y26=Wvol_int_low_l/18,

y27=Wvol_int_low_l/18,

y28=Wvol_int_low_l/18,

y29=Wvol_int_low_l/18,

y30=Wvol_int_low_l/18,

y31=Wvol_int_low_l/18,

y32=Wvol_int_low_l/18,

; Initial water volume in the last location of the intestine

y33=Wvol_int_low_r/8,

y34=Wvol_int_low_r/8,

y35=Wvol_int_low_r/8,

y36=Wvol_int_low_r/8,

$y_{37} = W_{vol_int_low_r}/8,$

$y_{38} = W_{vol_int_low_r}/8,$

$y_{39} = W_{vol_int_low_r}/8,$

$y_{40} = W_{vol_int_low_r}/8,$

; Initial water volume in the colon/caecum

$y_{41} = W_{vol_int_col},$

; Initial water volume in the stomach

$y_{43} = W_{vol_int},$

; Initial water volume in the whole small intestine

$y_{46} = W_{vol_int_low_l},$

; Water intake volume

$y_{50} = W_{vol_ini},$

; Concentration of perpetrator in the esophagus

$y_{320} = dose_inh/Ves,$

; Concentration of substrate in the esophagus (administered at time=Lag)

@at Lag:

$y_{100} = dose/Ves,$

@from 0:

; Membrane permeability of substrate

$$P_{\text{pass_lum_a1}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum1}-\text{pKa_acid})}}$$

$$+10^{(\text{pKa_base}-\text{pH_lum1})}),$$

$$P_{\text{Spass_lum_a1}} = P_{\text{pass_lum_a1}} \text{ ME Sent1},$$

$$P_{\text{Spass_a1}} = P_{\text{invivo}} \text{ ME Sent1},$$

$$P_{\text{Spass_b1}} = P_{\text{invivo}} \text{ Sent1},$$

$$P_{\text{Sap1}} = P_{\text{Spass_lum_a1}},$$

$$P_{\text{Sbp1}} = P_{\text{Spass_b1}},$$

$$P_{\text{Sbx1}} = P_{\text{Spass_b1}},$$

$$P_{\text{Spgp1}} = \text{psf_Pgp} * V_{\text{max_Pgp}} * A_{\text{rel_Pgp1}} / (K_{\text{m_Pgp}} + \text{fent} * y_{101} / V_{\text{ent1}}),$$

$$P_{\text{Sax1}} = (P_{\text{Spass_a1}} + P_{\text{Spgp1}}),$$

$$CL1 = V_{\text{max_3A4}} * A_{\text{rel_3A4_1}}$$

$$/ (K_{\text{m_3A4}} + \text{fent} * y_{101} / V_{\text{ent1}}) / (1 + (\text{fent_inh} * y_{231} / V_{\text{ent1}}) / K_{\text{i_3A4}}),$$

$$P_{\text{pass_lum_a2}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum2}-\text{pKa_acid})}}$$

$$+10^{(\text{pKa_base}-\text{pH_lum2})}),$$

$$P_{\text{Spass_lum_a2}} = P_{\text{pass_lum_a2}} \text{ ME Sent2},$$

$$P_{\text{Spass_a2}} = P_{\text{invivo}} \text{ ME Sent2},$$

$$P_{\text{Spass_b2}} = P_{\text{invivo}} \text{ Sent2},$$

$$P_{\text{Sap2}} = P_{\text{Spass_lum_a2}},$$

$$P_{\text{Sbp2}} = P_{\text{Spass_b2}},$$

$$P_{\text{Sbx2}} = P_{\text{Spass_b2}},$$

$$P_{\text{Spgp2}} = \text{psf_Pgp} * V_{\text{max_Pgp}} * A_{\text{rel_Pgp2}} / (K_{\text{m_Pgp}} + \text{fent} * y_{102} / V_{\text{ent2}}),$$

$$PSax2 = (PSpass_a2 + PSpgp2),$$

$$CL2 = Vmax_3A4 * Arel_3A4_2$$

$$/(Km_3A4 + fent * y102 / Vent2) / (1 + (fent_inh * y232 / Vent2) / Ki_3A4),$$

$$Ppass_lum_a3 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum3 - pKa_acid)}$$

$$+ 10^{(pKa_base - pH_lum3)}),$$

$$PSpass_lum_a3 = Ppass_lum_a3 ME Sent3,$$

$$PSpass_a3 = P_invivo ME Sent3,$$

$$PSpass_b3 = P_invivo Sent3,$$

$$PSap3 = PSpass_lum_a3,$$

$$PSbp3 = PSpass_b3,$$

$$PSbx3 = PSpass_b3,$$

$$PSpgp3 = psf_Pgp Vmax_Pgp Arel_Pgp3 / (Km_Pgp + fent y103 / Vent3),$$

$$PSax3 = (PSpass_a3 + PSpgp3),$$

$$CL3 = Vmax_3A4 Arel_3A4_3 / (Km_3A4 + fent y103 / Vent3) / (1 + (fent_inh * y233 / Vent3) / Ki_3A4),$$

$$Ppass_lum_a4 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum4 - pKa_acid)} + 10^{(pKa_base - pH_lum4)}),$$

$$PSpass_a4 = P_invivo ME Sent4,$$

$$PSpass_b4 = P_invivo Sent4,$$

$$PSpass_lum_a4 = Ppass_lum_a4 ME Sent4,$$

$$PSap4 = PSpass_lum_a4,$$

$$PSbp4 = PSpass_b4,$$

$$PSbx4 = PSpass_b4,$$

$$PSpgp4 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp4 } / (Km_Pgp + fent \ y104 / Vent4),$$

$$PSax4 = (PSpass_a4 + PSpgp4),$$

$$CL4 = \text{ Vmax_3A4 Arel_3A4_4 } / (Km_3A4 + fent \ y104 / Vent4) / (1 + (fent_inh * y234 / Vent4) / Ki_3A4),$$

$$Ppass_lum_a5 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum5 - pKa_acid)} + 10^{(pKa_base - pH_lum5)}),$$

$$PSpass_a5 = P_invivo \text{ ME Sent5},$$

$$PSpass_b5 = P_invivo \text{ Sent5},$$

$$PSpass_lum_a5 = Ppass_lum_a5 \text{ ME Sent5},$$

$$PSap5 = PSpass_lum_a5,$$

$$PSbp5 = PSpass_b5,$$

$$PSbx5 = PSpass_b5,$$

$$PSpgp5 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp5 } / (Km_Pgp + fent \ y105 / Vent5),$$

$$PSax5 = (PSpass_a5 + PSpgp5),$$

$$CL5 = \text{ Vmax_3A4 Arel_3A4_5 } / (Km_3A4 + fent \ y105 / Vent5) / (1 + (fent_inh * y235 / Vent5) / Ki_3A4),$$

$$Ppass_lum_a6 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum6 - pKa_acid)} + 10^{(pKa_base - pH_lum6)}),$$

$$PSpass_a6 = P_invivo \text{ ME Sent6},$$

$$PSpass_b6 = P_invivo \text{ Sent6},$$

$$PSpass_lum_a6 = Ppass_lum_a6 \text{ ME Sent6},$$

$$PSap6 = PSpass_lum_a6,$$

$$PSbp6 = PSpass_b6,$$

$$PSbx6 = PSpass_b6,$$

$$PSpgp6 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp6} / (\text{Km_Pgp} + \text{fent y106/Vent6}),$$

$$PSax6 = (\text{PSpass_a6} + \text{PSpgp6}),$$

$$CL6 = \text{Vmax_3A4 Arel_3A4_6} / (\text{Km_3A4} + \text{fent y106/Vent6}) / (1 + (\text{fent_inh} * \text{y236/Vent6}) / \text{Ki_3A4}),$$

$$Ppass_lum_a7 = P_invivo (1 + 10^{(\text{pH_Caco2} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_Caco2})}) / (1 + 10^{(\text{pH_lum7} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_lum7})}),$$

$$PSpass_a7 = P_invivo \text{ ME Sent7},$$

$$PSpass_b7 = P_invivo \text{ Sent7},$$

$$PSpass_lum_a7 = Ppass_lum_a7 \text{ ME Sent7},$$

$$PSap7 = PSpass_lum_a7,$$

$$PSbp7 = PSpass_b7,$$

$$PSbx7 = PSpass_b7,$$

$$PSpgp7 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp7} / (\text{Km_Pgp} + \text{fent y107/Vent7}),$$

$$PSax7 = (\text{PSpass_a7} + \text{PSpgp7}),$$

$$CL7 = \text{Vmax_3A4 Arel_3A4_7} / (\text{Km_3A4} + \text{fent y107/Vent7}) / (1 + (\text{fent_inh} * \text{y237/Vent7}) / \text{Ki_3A4}),$$

$$Ppass_lum_a8 = P_invivo (1 + 10^{(\text{pH_Caco2} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_Caco2})}) / (1 + 10^{(\text{pH_lum8} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_lum8})}),$$

$$PSpass_a8 = P_invivo \text{ ME Sent8},$$

$$PSpass_b8 = P_invivo \text{ Sent8},$$

$$PSpass_lum_a8 = Ppass_lum_a8 \text{ ME Sent8},$$

$$PSap8 = PSpass_lum_a4,$$

$$PSbp8 = PSpass_b8,$$

$$PSbx8 = (PSpass_b8),$$

$$PSpgp8 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp8 } / (Km_Pgp + fent \ y108 / Vent8),$$

$$PSax8 = (PSpass_a8 + PSpgp8),$$

$$CL8 = \text{ Vmax_3A4 Arel_3A4_8 } / (Km_3A4 + fent \ y108 / Vent8) / (1 + (fent_inh * y238 / Vent8) / Ki_3A4),$$

$$Ppass_lum_a9 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum9 - pKa_acid)} + 10^{(pKa_base - pH_lum9)}),$$

$$PSpass_a9 = P_invivo \text{ ME Sent9},$$

$$PSpass_b9 = P_invivo \text{ Sent9},$$

$$PSpass_lum_a9 = Ppass_lum_a9 \text{ ME Sent9},$$

$$PSap9 = PSpass_lum_a9,$$

$$PSbp9 = PSpass_b9,$$

$$PSbx9 = PSpass_b9,$$

$$PSpgp9 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp9 } / (Km_Pgp + fent \ y109 / Vent9),$$

$$PSax9 = (PSpass_a9 + PSpgp9),$$

$$CL9 = \text{ Vmax_3A4 Arel_3A4_9 } / (Km_3A4 + fent \ y109 / Vent9) / (1 + (fent_inh * y239 / Vent9) / Ki_3A4),$$

$$Ppass_lum_a10 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum10 - pKa_acid)} + 10^{(pKa_base - pH_lum10)}),$$

$$PSpass_a10 = P_invivo \text{ ME Sent10},$$

$$PSpass_b10 = P_invivo \text{ Sent10},$$

$PS_{pass_lum_a10} = P_{pass_lum_a10} ME_{Sent10}$,
 $PS_{ap10} = PS_{pass_lum_a10}$,
 $PS_{bp10} = PS_{pass_b10}$,
 $PS_{bx10} = PS_{pass_b10}$,
 $PS_{pgp10} = \frac{psf_Pgp V_{max_Pgp} A_{rel_Pgp10}}{(K_{m_Pgp} + fent_{y110}/Vent10)}$,
 $PS_{ax10} = (PS_{pass_a10} + PS_{pgp10})$,
 $CL10 = \frac{V_{max_3A4} A_{rel_3A4_10}}{(K_{m_3A4} + fent_{y110}/Vent10) / (1 + (fent_inh * y_{240}/Vent10) / K_{i_3A4})}$,

$P_{pass_lum_a11} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum11} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum11})})}$,
 $PS_{pass_a11} = P_{invivo} ME_{Sent11}$,
 $PS_{pass_b11} = P_{invivo} Sent11$,
 $PS_{pass_lum_a11} = P_{pass_lum_a11} ME_{Sent11}$,
 $PS_{ap11} = PS_{pass_lum_a11}$,
 $PS_{bp11} = PS_{pass_b11}$,
 $PS_{bx11} = PS_{pass_b11}$,
 $PS_{pgp11} = \frac{psf_Pgp V_{max_Pgp} A_{rel_Pgp11}}{(K_{m_Pgp} + fent_{y111}/Vent11)}$,
 $PS_{ax11} = (PS_{pass_a11} + PS_{pgp11})$,
 $CL11 = \frac{V_{max_3A4} A_{rel_3A4_11}}{(K_{m_3A4} + fent_{y111}/Vent11) / (1 + (fent_inh * y_{241}/Vent11) / K_{i_3A4})}$,

$P_{pass_lum_a12} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum12} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum12})})}$,
 $PS_{pass_a12} = P_{invivo} ME_{Sent12}$,

$$PS_{pass_b12} = P_{invivo} Sent12,$$

$$PS_{pass_lum_a12} = P_{pass_lum_a12} ME Sent12,$$

$$PS_{ap12} = PS_{pass_lum_a12},$$

$$PS_{bp12} = PS_{pass_b12},$$

$$PS_{bx12} = PS_{pass_b12},$$

$$PS_{pgp12} = \text{psf_Pgp } V_{max_Pgp} A_{rel_Pgp12} / (K_{m_Pgp} + f_{ent} y_{112} / V_{ent12}),$$

$$PS_{ax12} = (PS_{pass_a12} + PS_{pgp12}),$$

$$CL_{12} = \frac{V_{max_3A4} A_{rel_3A4_12}}{(K_{m_3A4} + f_{ent} y_{112} / V_{ent12}) / (1 + (f_{ent_inh} * y_{242} / V_{ent12}) / K_{i_3A4})},$$

$$P_{pass_lum_a13} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum13} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum13})})},$$

$$PS_{pass_a13} = P_{invivo} ME Sent13,$$

$$PS_{pass_b13} = P_{invivo} Sent13,$$

$$PS_{pass_lum_a13} = P_{pass_lum_a13} ME Sent13,$$

$$PS_{ap13} = PS_{pass_lum_a13},$$

$$PS_{bp13} = PS_{pass_b13},$$

$$PS_{bx13} = PS_{pass_b13},$$

$$PS_{pgp13} = \text{psf_Pgp } V_{max_Pgp} A_{rel_Pgp13} / (K_{m_Pgp} + f_{ent} y_{113} / V_{ent13}),$$

$$PS_{ax13} = (PS_{pass_a13} + PS_{pgp13}),$$

$$CL_{13} = \frac{V_{max_3A4} A_{rel_3A4_13}}{(K_{m_3A4} + f_{ent} y_{113} / V_{ent13}) / (1 + (f_{ent_inh} * y_{243} / V_{ent13}) / K_{i_3A4})},$$

$$P_{pass_lum_a14} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum14} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum14})})},$$

$$PSpass_a14 = P_invivo \text{ ME Sent14},$$

$$PSpass_b14 = P_invivo \text{ Sent14},$$

$$PSpass_lum_a14 = Ppass_lum_a14 \text{ ME Sent14},$$

$$PSap14 = PSpass_lum_a14,$$

$$PSbp14 = PSpass_b14,$$

$$PSbx14 = PSpass_b14,$$

$$PSpgp14 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp14 } / (Km_Pgp + fent \text{ y114/Vent14}),$$

$$PSax14 = (PSpass_a14 + PSpgp14),$$

$$CL14 = \text{ Vmax_3A4 Arel_3A4_14 } / (Km_3A4 + fent \text{ y114/Vent14}) / (1 + (fent_inh * y244 / Vent14) / Ki_3A4),$$

$$Ppass_lum_a15 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum15 - pKa_acid)} + 10^{(pKa_base - pH_lum15)}),$$

$$PSpass_a15 = P_invivo \text{ ME Sent15},$$

$$PSpass_b15 = P_invivo \text{ Sent15},$$

$$PSpass_lum_a15 = Ppass_lum_a15 \text{ ME Sent15},$$

$$PSap15 = PSpass_lum_a15,$$

$$PSbp15 = PSpass_b15,$$

$$PSbx15 = PSpass_b15,$$

$$PSpgp15 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp15 } / (Km_Pgp + fent \text{ y115/Vent15}),$$

$$PSax15 = (PSpass_a15 + PSpgp15),$$

$$CL15 = \text{ Vmax_3A4 Arel_3A4_15 } / (Km_3A4 + fent \text{ y115/Vent15}) / (1 + (fent_inh * y245 / Vent15) / Ki_3A4),$$

$$P_{\text{pass_lum_a16}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2}))}}{(1+10^{(\text{pH_lum16}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_lum16}))},$$

$$P_{\text{Spass_a16}} = P_{\text{invivo}} \text{ME Sent16},$$

$$P_{\text{Spass_b16}} = P_{\text{invivo}} \text{Sent16},$$

$$P_{\text{Spass_lum_a16}} = P_{\text{pass_lum_a16}} \text{ME Sent16},$$

$$P_{\text{Sap16}} = P_{\text{Spass_lum_a16}},$$

$$P_{\text{Sbp16}} = P_{\text{Spass_b16}},$$

$$P_{\text{Sbx16}} = P_{\text{Spass_b16}},$$

$$P_{\text{Spgp16}} = \text{psf_Pgp} \frac{V_{\text{max_Pgp}} \text{Arel_Pgp16}}{(K_{\text{m_Pgp}} + \text{fent y116/Vent16})},$$

$$P_{\text{Sax16}} = (P_{\text{Spass_a16}} + P_{\text{Spgp16}}),$$

$$CL_{16} = \frac{V_{\text{max_3A4}} \text{Arel_3A4_16}}{(K_{\text{m_3A4}} + \text{fent y116/Vent16}) / (1 + (\text{fent_inh} * \text{y246/Vent16}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a17}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2}))}}{(1+10^{(\text{pH_lum17}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_lum17}))},$$

$$P_{\text{Spass_a17}} = P_{\text{invivo}} \text{ME Sent17},$$

$$P_{\text{Spass_b17}} = P_{\text{invivo}} \text{Sent17},$$

$$P_{\text{Spass_lum_a17}} = P_{\text{pass_lum_a17}} \text{ME Sent17},$$

$$P_{\text{Sap17}} = P_{\text{Spass_lum_a17}},$$

$$P_{\text{Sbp17}} = P_{\text{Spass_b17}},$$

$$P_{\text{Sbx17}} = P_{\text{Spass_b17}},$$

$$P_{\text{Spgp17}} = \text{psf_Pgp} \frac{V_{\text{max_Pgp}} \text{Arel_Pgp17}}{(K_{\text{m_Pgp}} + \text{fent y117/Vent17})},$$

$$P_{\text{Sax17}} = (P_{\text{Spass_a17}} + P_{\text{Spgp17}}),$$

$$CL_{17} = \frac{V_{\text{max_3A4}} \text{Arel_3A4_17}}{(K_{\text{m_3A4}} + \text{fent y117/Vent17}) / (1 + (\text{fent_inh} * \text{y247/Vent17}) / K_{\text{i_3A4}})},$$

$$P_{pass_lum_a18} = P_{invivo} \frac{(1+10^{(pH_Caco2-pKa_acid)}+10^{(pKa_base-pH_Caco2)})}{(1+10^{(pH_lum18-pKa_acid)}+10^{(pKa_base-pH_lum18)})}$$
,

$$P_{Spass_a18} = P_{invivo} ME_{Sent18}$$
,

$$P_{Spass_b18} = P_{invivo} Sent18$$
,

$$P_{Spass_lum_a18} = P_{pass_lum_a18} ME_{Sent18}$$
,

$$P_{Sap18} = P_{Spass_lum_a18}$$
,

$$P_{Sbp18} = P_{Spass_b18}$$
,

$$P_{Sbx18} = P_{Spass_b18}$$
,

$$P_{Spgp18} = psf_Pgp \frac{Vmax_Pgp Arel_Pgp18}{(Km_Pgp+fent y118/Vent18)}$$
,

$$P_{Sax18} = (P_{Spass_a18} + P_{Spgp18})$$
,

$$CL18 = \frac{Vmax_3A4 Arel_3A4_18}{(Km_3A4+fent y118/Vent18)/(1+(fent_inh*y248/Vent18)/Ki_3A4)}$$
,

$$P_{pass_lum_a19} = P_{invivo} \frac{(1+10^{(pH_Caco2-pKa_acid)}+10^{(pKa_base-pH_Caco2)})}{(1+10^{(pH_lum19-pKa_acid)}+10^{(pKa_base-pH_lum19)})}$$
,

$$P_{Spass_a19} = P_{invivo} ME_{Sent19}$$
,

$$P_{Spass_b19} = P_{invivo} Sent19$$
,

$$P_{Spass_lum_a19} = P_{pass_lum_a19} ME_{Sent19}$$
,

$$P_{Sap19} = P_{Spass_lum_a19}$$
,

$$P_{Sbp19} = P_{Spass_b19}$$
,

$$P_{Sbx19} = P_{Spass_b19}$$
,

$$P_{Spgp19} = psf_Pgp \frac{Vmax_Pgp Arel_Pgp19}{(Km_Pgp+fent y119/Vent19)}$$
,

$$P_{Sax19} = (P_{Spass_a19} + P_{Spgp19})$$
,

$$CL19 = \frac{V_{max_3A4} A_{rel_3A4_19}}{(K_{m_3A4} + f_{ent} y_{119}/V_{ent19}) / (1 + (f_{ent_inh} * y_{249}/V_{ent19}) / K_{i_3A4})}$$

$$P_{pass_lum_a20} = P_{invivo} \frac{(1 + 10^{(pH_Caco2 - pK_{a_acid})}) + 10^{(pK_{a_base} - pH_Caco2)}}{(1 + 10^{(pH_lum20 - pK_{a_acid})}) + 10^{(pK_{a_base} - pH_lum20)}}$$

$$P_{Spass_a20} = P_{invivo} ME_{Sent20}$$

$$P_{Spass_b20} = P_{invivo} Sent20$$

$$P_{Spass_lum_a20} = P_{pass_lum_a20} ME_{Sent20}$$

$$P_{Sap20} = P_{Spass_lum_a20}$$

$$P_{Sbp20} = P_{Spass_b20}$$

$$P_{Sbx20} = P_{Spass_b20}$$

$$P_{Spgp20} = \frac{psf_Pgp V_{max_Pgp} A_{rel_Pgp20}}{(K_{m_Pgp} + f_{ent} y_{120}/V_{ent20})}$$

$$P_{Sax20} = (P_{Spass_a20} + P_{Spgp20})$$

$$CL20 = \frac{V_{max_3A4} A_{rel_3A4_20}}{(K_{m_3A4} + f_{ent} y_{120}/V_{ent20}) / (1 + (f_{ent_inh} * y_{250}/V_{ent20}) / K_{i_3A4})}$$

$$P_{pass_lum_a21} = P_{invivo} \frac{(1 + 10^{(pH_Caco2 - pK_{a_acid})}) + 10^{(pK_{a_base} - pH_Caco2)}}{(1 + 10^{(pH_lum21 - pK_{a_acid})}) + 10^{(pK_{a_base} - pH_lum21)}}$$

$$P_{Spass_a21} = P_{invivo} ME_{Sent21}$$

$$P_{Spass_b21} = P_{invivo} Sent21$$

$$P_{Spass_lum_a21} = P_{pass_lum_a21} ME_{Sent21}$$

$$P_{Sap21} = P_{Spass_lum_a21}$$

$$P_{Sbp21} = P_{Spass_b21}$$

$$P_{Sbx21} = P_{Spass_b21}$$

$$P_{Spgp21} = \frac{psf_Pgp V_{max_Pgp} A_{rel_Pgp21}}{(K_{m_Pgp} + f_{ent} y_{121}/V_{ent21})}$$

$$PSax21 = (PSpass_a21 + PSpgp21),$$

$$CL21 = \frac{Vmax_3A4 \text{ Arel_3A4_21}}{(Km_3A4 + fent y121/Vent21) / (1 + (fent_inh * y251/Vent21) / Ki_3A4)},$$

$$Ppass_lum_a22 = P_invivo \frac{(1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)})}{(1 + 10^{(pH_lum22 - pKa_acid)} + 10^{(pKa_base - pH_lum22)}),$$

$$PSpass_a22 = P_invivo \text{ ME Sent22},$$

$$PSpass_b22 = P_invivo \text{ Sent22},$$

$$PSpass_lum_a22 = Ppass_lum_a22 \text{ ME Sent22},$$

$$PSap22 = PSpass_lum_a22,$$

$$PSbp22 = PSpass_b22,$$

$$PSbx22 = PSpass_b22,$$

$$PSpgp22 = psf_Pgp \frac{Vmax_Pgp \text{ Arel_Pgp22}}{(Km_Pgp + fent y122/Vent22)},$$

$$PSax22 = (PSpass_a22 + PSpgp22),$$

$$CL22 = \frac{Vmax_3A4 \text{ Arel_3A4_22}}{(Km_3A4 + fent y122/Vent22) / (1 + (fent_inh * y252/Vent22) / Ki_3A4)},$$

$$Ppass_lum_a23 = P_invivo \frac{(1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)})}{(1 + 10^{(pH_lum23 - pKa_acid)} + 10^{(pKa_base - pH_lum23)}),$$

$$PSpass_a23 = P_invivo \text{ ME Sent23},$$

$$PSpass_b23 = P_invivo \text{ Sent23},$$

$$PSpass_lum_a23 = Ppass_lum_a23 \text{ ME Sent23},$$

$$PSap23 = PSpass_lum_a23,$$

$$PSbp23 = PSpass_b23,$$

$$PSbx23 = PSpass_b23,$$

$$PSpgp23 = \text{psf_Pgp } V_{\text{max_Pgp}} \text{ Arel_Pgp23} / (K_{\text{m_Pgp}} + \text{fent } y_{123}/V_{\text{ent23}}),$$

$$PSax23 = (P_{\text{Spass_a23}} + PSpgp23),$$

$$CL23 = \frac{V_{\text{max_3A4}} \text{ Arel_3A4_23}}{(K_{\text{m_3A4}} + \text{fent } y_{123}/V_{\text{ent23}}) / (1 + (\text{fent_inh} * y_{253}/V_{\text{ent23}}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a24}} = P_{\text{invivo}} \frac{(1 + 10^{(\text{pH_Caco2} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_Caco2})})}{(1 + 10^{(\text{pH_lum24} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_lum24})}),$$

$$P_{\text{Spass_a24}} = P_{\text{invivo}} \text{ ME Sent24},$$

$$P_{\text{Spass_b24}} = P_{\text{invivo}} \text{ Sent24},$$

$$P_{\text{Spass_lum_a24}} = P_{\text{pass_lum_a24}} \text{ ME Sent24},$$

$$P_{\text{Sap24}} = P_{\text{Spass_lum_a24}},$$

$$P_{\text{Sbp24}} = P_{\text{Spass_b24}},$$

$$P_{\text{Sbx24}} = P_{\text{Spass_b24}},$$

$$PSpgp24 = \text{psf_Pgp } V_{\text{max_Pgp}} \text{ Arel_Pgp24} / (K_{\text{m_Pgp}} + \text{fent } y_{124}/V_{\text{ent24}}),$$

$$PSax24 = (P_{\text{Spass_a24}} + PSpgp24),$$

$$CL24 = \frac{V_{\text{max_3A4}} \text{ Arel_3A4_24}}{(K_{\text{m_3A4}} + \text{fent } y_{124}/V_{\text{ent24}}) / (1 + (\text{fent_inh} * y_{254}/V_{\text{ent24}}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a25}} = P_{\text{invivo}} \frac{(1 + 10^{(\text{pH_Caco2} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_Caco2})})}{(1 + 10^{(\text{pH_lum25} - \text{pKa_acid})} + 10^{(\text{pKa_base} - \text{pH_lum25})}),$$

$$P_{\text{Spass_a25}} = P_{\text{invivo}} \text{ ME Sent25},$$

$$P_{\text{Spass_b25}} = P_{\text{invivo}} \text{ Sent25},$$

$$P_{\text{Spass_lum_a25}} = P_{\text{pass_lum_a25}} \text{ ME Sent25},$$

$$P_{\text{Sap25}} = P_{\text{Spass_lum_a25}},$$

$$P_{\text{Sbp25}} = P_{\text{Spass_b25}},$$

$$PSbx25 = PSpass_b25,$$

$$PSpgp25 = psf_Pgp \frac{Vmax_Pgp \ Arel_Pgp25}{(Km_Pgp + fent \ y125/Vent25)},$$

$$PSax25 = (PSpass_a25 + PSpgp25),$$

$$CL25 = \frac{Vmax_3A4 \ Arel_3A4_25}{(Km_3A4 + fent \ y125/Vent25) / (1 + (fent_inh * y255/Vent25) / Ki_3A4)},$$

$$Ppass_lum_a26 = P_invivo \frac{(1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)})}{(1 + 10^{(pH_lum26 - pKa_acid)} + 10^{(pKa_base - pH_lum26)}),$$

$$PSpass_a26 = P_invivo \ ME \ Sent26,$$

$$PSpass_b26 = P_invivo \ Sent26,$$

$$PSpass_lum_a26 = Ppass_lum_a26 \ ME \ Sent26,$$

$$PSap26 = PSpass_lum_a26,$$

$$PSbp26 = PSpass_b26,$$

$$PSbx26 = PSpass_b26,$$

$$PSpgp26 = psf_Pgp \frac{Vmax_Pgp \ Arel_Pgp26}{(Km_Pgp + fent \ y126/Vent26)},$$

$$PSax26 = (PSpass_a26 + PSpgp26),$$

$$CL26 = \frac{Vmax_3A4 \ Arel_3A4_26}{(Km_3A4 + fent \ y126/Vent26) / (1 + (fent_inh * y256/Vent26) / Ki_3A4)},$$

$$Ppass_lum_a27 = P_invivo \frac{(1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)})}{(1 + 10^{(pH_lum27 - pKa_acid)} + 10^{(pKa_base - pH_lum27)}),$$

$$PSpass_a27 = P_invivo \ ME \ Sent27,$$

$$PSpass_b27 = P_invivo \ Sent27,$$

$$PSpass_lum_a27 = Ppass_lum_a27 \ ME \ Sent27,$$

$$PSap27 = PSpass_lum_a27,$$

$$PS_{bp27} = P_{Spass_b27},$$

$$PS_{bx27} = P_{Spass_b27},$$

$$PS_{pgp27} = \text{psf_Pgp } V_{\text{max_Pgp}} A_{\text{rel_Pgp27}} / (K_{\text{m_Pgp}} + f_{\text{ent}} y_{127} / V_{\text{ent27}}),$$

$$PS_{ax27} = (P_{Spass_a27} + PS_{pgp27}),$$

$$CL_{27} = \frac{V_{\text{max_3A4}} A_{\text{rel_3A4_27}}}{(K_{\text{m_3A4}} + f_{\text{ent}} y_{127} / V_{\text{ent27}}) (1 + (f_{\text{ent_inh}} * y_{257} / V_{\text{ent27}}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a28}} = P_{\text{invivo}} \frac{(1 + 10^{(\text{pH_Caco2} - \text{pKa_acid})}) + 10^{(\text{pKa_base} - \text{pH_Caco2})}}{(1 + 10^{(\text{pH_lum28} - \text{pKa_acid})}) + 10^{(\text{pKa_base} - \text{pH_lum28})}},$$

$$P_{Spass_a28} = P_{\text{invivo}} ME_{\text{Sent28}},$$

$$P_{Spass_b28} = P_{\text{invivo}} Sent_{28},$$

$$P_{Spass_lum_a28} = P_{\text{pass_lum_a28}} ME_{\text{Sent28}},$$

$$P_{Sap28} = P_{Spass_lum_a28},$$

$$P_{Sbp28} = P_{Spass_b28},$$

$$P_{Sbx28} = P_{Spass_b28},$$

$$PS_{pgp28} = \text{psf_Pgp } V_{\text{max_Pgp}} A_{\text{rel_Pgp28}} / (K_{\text{m_Pgp}} + f_{\text{ent}} y_{128} / V_{\text{ent28}}),$$

$$PS_{ax28} = (P_{Spass_a28} + PS_{pgp28}),$$

$$CL_{28} = \frac{V_{\text{max_3A4}} A_{\text{rel_3A4_28}}}{(K_{\text{m_3A4}} + f_{\text{ent}} y_{128} / V_{\text{ent28}}) (1 + (f_{\text{ent_inh}} * y_{258} / V_{\text{ent28}}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a29}} = P_{\text{invivo}} \frac{(1 + 10^{(\text{pH_Caco2} - \text{pKa_acid})}) + 10^{(\text{pKa_base} - \text{pH_Caco2})}}{(1 + 10^{(\text{pH_lum29} - \text{pKa_acid})}) + 10^{(\text{pKa_base} - \text{pH_lum29})}},$$

$$P_{Spass_a29} = P_{\text{invivo}} ME_{\text{Sent29}},$$

$$P_{Spass_b29} = P_{\text{invivo}} Sent_{29},$$

$$P_{Spass_lum_a29} = P_{\text{pass_lum_a29}} ME_{\text{Sent29}},$$

$$PSap29 = PSpass_lum_a29,$$

$$PSbp29 = PSpass_b29,$$

$$PSbx29 = PSpass_b29,$$

$$PSpgp29 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp29 } / (Km_Pgp + fent \ y129 / Vent29),$$

$$PSax29 = (PSpass_a29 + PSpgp29),$$

$$CL29 = \text{ Vmax_3A4 Arel_3A4_29 } / (Km_3A4 + fent$$

$$y129 / Vent29) / (1 + (fent_inh * y259 / Vent29) / Ki_3A4),$$

$$Ppass_lum_a30 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum30 - pKa_acid)} + 10^{(pKa_base - pH_lum30)}),$$

$$PSpass_a30 = P_invivo \text{ ME Sent30},$$

$$PSpass_b30 = P_invivo \text{ Sent30},$$

$$PSpass_lum_a30 = Ppass_lum_a30 \text{ ME Sent30},$$

$$PSap30 = PSpass_lum_a30,$$

$$PSbp30 = PSpass_b30,$$

$$PSbx30 = PSpass_b30,$$

$$PSpgp30 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp30 } / (Km_Pgp + fent \ y130 / Vent30),$$

$$PSax30 = (PSpass_a30 + PSpgp30),$$

$$CL30 = \text{ Vmax_3A4 Arel_3A4_30 } / (Km_3A4 + fent$$

$$y130 / Vent30) / (1 + (fent_inh * y260 / Vent30) / Ki_3A4),$$

$$Ppass_lum_a31 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum31 - pKa_acid)} + 10^{(pKa_base - pH_lum31)}),$$

$$PSpass_a31 = P_invivo \text{ ME Sent31},$$

$$PSpass_b31 = P_invivo \text{ Sent31},$$

$PS_{pass_lum_a31} = P_{pass_lum_a31} ME_{Sent31}$,
 $PS_{ap31} = PS_{pass_lum_a31}$,
 $PS_{bp31} = PS_{pass_b31}$,
 $PS_{bx31} = PS_{pass_b31}$,
 $PS_{pgp31} = \frac{psf_Pgp \cdot V_{max_Pgp} \cdot A_{rel_Pgp31}}{(K_{m_Pgp} + f_{ent} \cdot y_{131}/V_{ent31})}$,
 $PS_{ax31} = (PS_{pass_a31} + PS_{pgp31})$,
 $CL_{31} = \frac{V_{max_3A4} \cdot A_{rel_3A4_31}}{(K_{m_3A4} + f_{ent} \cdot y_{131}/V_{ent31}) / (1 + (f_{ent_inh} \cdot y_{261}/V_{ent31}) / K_{i_3A4})}$,

$P_{pass_lum_a32} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum32} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum32})})}$,
 $PS_{pass_a32} = P_{invivo} ME_{Sent32}$,
 $PS_{pass_b32} = P_{invivo} Sent32$,
 $PS_{pass_lum_a32} = P_{pass_lum_a32} ME_{Sent32}$,
 $PS_{ap32} = PS_{pass_lum_a32}$,
 $PS_{bp32} = PS_{pass_b32}$,
 $PS_{bx32} = PS_{pass_b32}$,
 $PS_{pgp32} = \frac{psf_Pgp \cdot V_{max_Pgp} \cdot A_{rel_Pgp32}}{(K_{m_Pgp} + f_{ent} \cdot y_{132}/V_{ent32})}$,
 $PS_{ax32} = (PS_{pass_a32} + PS_{pgp32})$,
 $CL_{32} = \frac{V_{max_3A4} \cdot A_{rel_3A4_32}}{(K_{m_3A4} + f_{ent} \cdot y_{132}/V_{ent32}) / (1 + (f_{ent_inh} \cdot y_{262}/V_{ent32}) / K_{i_3A4})}$,

$P_{pass_lum_a33} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum33} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum33})})}$,
 $PS_{pass_a33} = P_{invivo} ME_{Sent33}$,

$$PSpass_b33 = P_invivo \text{ Sent33},$$

$$Ppass_lum_a33 = Ppass_lum_a33 \text{ ME Sent33},$$

$$PSap33 = PSpass_lum_a33,$$

$$PSbp33 = PSpass_b33,$$

$$PSbx33 = PSpass_b33,$$

$$PSpgp33 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp33 } / (Km_Pgp + fent \text{ y133/Vent33}),$$

$$PSax33 = (PSpass_a33 + PSpgp33),$$

$$CL33 = \text{ Vmax_3A4 Arel_3A4_33 } / (Km_3A4 + fent \text{ y133/Vent33}) / (1 + (fent_inh * y263/Vent33) / Ki_3A4),$$

$$Ppass_lum_a34 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum34 - pKa_acid)} + 10^{(pKa_base - pH_lum34)}),$$

$$PSpass_a34 = P_invivo \text{ ME Sent34},$$

$$PSpass_b34 = P_invivo \text{ Sent34},$$

$$PSpass_lum_a34 = Ppass_lum_a34 \text{ ME Sent34},$$

$$PSap34 = PSpass_lum_a34,$$

$$PSbp34 = PSpass_b34,$$

$$PSbx34 = PSpass_b34,$$

$$PSpgp34 = psf_Pgp \text{ Vmax_Pgp Arel_Pgp34 } / (Km_Pgp + fent \text{ y134/Vent34}),$$

$$PSax34 = (PSpass_a34 + PSpgp34),$$

$$CL34 = \text{ Vmax_3A4 Arel_3A4_34 } / (Km_3A4 + fent \text{ y134/Vent34}) / (1 + (fent_inh * y264/Vent34) / Ki_3A4),$$

$$Ppass_lum_a35 = P_invivo (1 + 10^{(pH_Caco2 - pKa_acid)} + 10^{(pKa_base - pH_Caco2)}) / (1 + 10^{(pH_lum35 - pKa_acid)} + 10^{(pKa_base - pH_lum35)}),$$

$$PS_{pass_a35} = P_{invivo} ME_{Sent35},$$

$$PS_{pass_b35} = P_{invivo} Sent35,$$

$$PS_{pass_lum_a35} = P_{pass_lum_a35} ME_{Sent35},$$

$$PS_{ap35} = PS_{pass_lum_a35},$$

$$PS_{bp35} = PS_{pass_b35},$$

$$PS_{bx35} = PS_{pass_b35},$$

$$PS_{pgp35} = psf_Pgp \frac{V_{max_Pgp} A_{rel_Pgp35}}{(K_{m_Pgp} + f_{ent} y_{135}/V_{ent35})},$$

$$PS_{ax35} = (PS_{pass_a35} + PS_{pgp35}),$$

$$CL_{35} = \frac{V_{max_3A4} A_{rel_3A4_35}}{(K_{m_3A4} + f_{ent} y_{135}/V_{ent35}) / (1 + (f_{ent_inh} * y_{265}/V_{ent35}) / K_{i_3A4})},$$

$$P_{pass_lum_a36} = P_{invivo} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{Caco2})})}{(1 + 10^{(pH_{lum36} - pK_{a_acid})} + 10^{(pK_{a_base} - pH_{lum36})})},$$

$$PS_{pass_a36} = P_{invivo} ME_{Sent36},$$

$$PS_{pass_b36} = P_{invivo} Sent36,$$

$$PS_{pass_lum_a36} = P_{pass_lum_a36} ME_{Sent36},$$

$$PS_{ap36} = PS_{pass_lum_a36},$$

$$PS_{bp36} = PS_{pass_b36},$$

$$PS_{bx36} = PS_{pass_b36},$$

$$PS_{pgp36} = psf_Pgp \frac{V_{max_Pgp} A_{rel_Pgp36}}{(K_{m_Pgp} + f_{ent} y_{136}/V_{ent36})},$$

$$PS_{ax36} = (PS_{pass_a36} + PS_{pgp36}),$$

$$CL_{36} = \frac{V_{max_3A4} A_{rel_3A4_36}}{(K_{m_3A4} + f_{ent} y_{136}/V_{ent36}) / (1 + (f_{ent_inh} * y_{266}/V_{ent36}) / K_{i_3A4})},$$

$$P_{\text{pass_lum_a37}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2}))}}{(1+10^{(\text{pH_lum37}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_lum37}))},$$

$$P_{\text{Spass_a37}} = P_{\text{invivo}} \text{ME Sent37},$$

$$P_{\text{Spass_b37}} = P_{\text{invivo}} \text{Sent37},$$

$$P_{\text{Spass_lum_a37}} = P_{\text{pass_lum_a37}} \text{ME Sent37},$$

$$P_{\text{Sap37}} = P_{\text{Spass_lum_a37}},$$

$$P_{\text{Sbp37}} = P_{\text{Spass_b37}},$$

$$P_{\text{Sbx37}} = P_{\text{Spass_b37}},$$

$$P_{\text{Spgp37}} = \text{psf_Pgp} \frac{V_{\text{max_Pgp}} \text{Arel_Pgp37}}{(K_{\text{m_Pgp}} + \text{fent y137/Vent37})},$$

$$P_{\text{Sax37}} = (P_{\text{Spass_a37}} + P_{\text{Spgp37}}),$$

$$CL_{37} = \frac{V_{\text{max_3A4}} \text{Arel_3A4_37}}{(K_{\text{m_3A4}} + \text{fent y137/Vent37}) / (1 + (\text{fent_inh} * \text{y267/Vent37}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a38}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2}))}}{(1+10^{(\text{pH_lum38}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_lum38}))},$$

$$P_{\text{Spass_a38}} = P_{\text{invivo}} \text{ME Sent38},$$

$$P_{\text{Spass_b38}} = P_{\text{invivo}} \text{Sent38},$$

$$P_{\text{Spass_lum_a38}} = P_{\text{pass_lum_a38}} \text{ME Sent38},$$

$$P_{\text{Sap38}} = P_{\text{Spass_lum_a38}},$$

$$P_{\text{Sbp38}} = P_{\text{Spass_b38}},$$

$$P_{\text{Sbx38}} = P_{\text{Spass_b38}},$$

$$P_{\text{Spgp38}} = \text{psf_Pgp} \frac{V_{\text{max_Pgp}} \text{Arel_Pgp38}}{(K_{\text{m_Pgp}} + \text{fent y138/Vent38})},$$

$$P_{\text{Sax38}} = (P_{\text{Spass_a38}} + P_{\text{Spgp38}}),$$

$$CL_{38} = \frac{V_{\text{max_3A4}} \text{Arel_3A4_38}}{(K_{\text{m_3A4}} + \text{fent y138/Vent38}) / (1 + (\text{fent_inh} * \text{y268/Vent38}) / K_{\text{i_3A4}})},$$

$$P_{\text{pass_lum_a39}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum39}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_lum39})})}$$
,

$$P_{\text{Spass_a39}} = P_{\text{invivo}} \text{ME Sent39}$$
,

$$P_{\text{Spass_b39}} = P_{\text{invivo}} \text{Sent39}$$
,

$$P_{\text{Spass_lum_a39}} = P_{\text{pass_lum_a39}} \text{ME Sent39}$$
,

$$P_{\text{Sap39}} = P_{\text{Spass_lum_a39}}$$
,

$$P_{\text{Sbp39}} = P_{\text{Spass_b39}}$$
,

$$P_{\text{Sbx39}} = P_{\text{Spass_b39}}$$
,

$$P_{\text{Spgp39}} = \text{psf_Pgp} \frac{V_{\text{max_Pgp}} \text{Arel_Pgp39}}{(K_{\text{m_Pgp}} + \text{fent y139/Vent39})}$$
,

$$P_{\text{Sax39}} = (P_{\text{Spass_a39}} + P_{\text{Spgp39}})$$
,

$$CL_{39} = \frac{V_{\text{max_3A4}} \text{Arel_3A4_39}}{(K_{\text{m_3A4}} + \text{fent y139/Vent39}) / (1 + (\text{fent_inh} * \text{y269/Vent39}) / K_{\text{i_3A4}})}$$
,

$$P_{\text{pass_lum_a40}} = P_{\text{invivo}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum40}-\text{pKa_acid})}+10^{(\text{pKa_base}-\text{pH_lum40})})}$$
,

$$P_{\text{Spass_a40}} = P_{\text{invivo}} \text{ME Sent40}$$
,

$$P_{\text{Spass_b40}} = P_{\text{invivo}} \text{Sent40}$$
,

$$P_{\text{Spass_lum_a40}} = P_{\text{pass_lum_a40}} \text{ME Sent40}$$
,

$$P_{\text{Sap40}} = P_{\text{Spass_lum_a40}}$$
,

$$P_{\text{Sbp40}} = P_{\text{Spass_b40}}$$
,

$$P_{\text{Sbx40}} = P_{\text{Spass_b40}}$$
,

$$P_{\text{Spgp40}} = \text{psf_Pgp} \frac{V_{\text{max_Pgp}} \text{Arel_Pgp40}}{(K_{\text{m_Pgp}} + \text{fent y140/Vent40})}$$
,

$$P_{\text{Sax40}} = (P_{\text{Spass_a40}} + P_{\text{Spgp40}})$$
,

$$CL40 = \frac{V_{max_3A4} A_{rel_3A4_40}}{(K_m_3A4 + f_{ent} y_{140} / V_{ent40}) (1 + (f_{ent_inh} y_{270} / V_{ent40}) / K_i_3A4)},$$

; Water volume in the small intestine at each location (substrate)

$$y_1' = (kg * y_{43}) V_g \text{ div} / V + (c_{3a_1} - k_{w_1}) * y_1 + c_{4a_2} * y_2 + c_{5_3} * y_3 + sw_1,$$

$$y_2' = c_{2a_1} * y_1 + c_{3_2_kw} * y_2 + c_{4_3} * y_3 + c_{5_4} * y_4 + sw_2,$$

$$y_3' = c_{1_1} * y_1 + c_{2_2} * y_2 + c_{3_3_kw} * y_3 + c_{4_4} * y_4 + c_{5_5} * y_5 + sw_3,$$

$$y_4' = c_{1_2} * y_2 + c_{2_3} * y_3 + c_{3_4_kw} * y_4 + c_{4_5} * y_5 + c_{5_6} * y_6 + sw_4,$$

$$y_5' = c_{1_3} * y_3 + c_{2_4} * y_4 + c_{3_5_kw} * y_5 + c_{4_6} * y_6 + c_{5_7} * y_7 + sw_5,$$

$$y_6' = c_{1_4} * y_4 + c_{2_5} * y_5 + c_{3_6_kw} * y_6 + c_{4_7} * y_7 + c_{5_8} * y_8 + sw_6,$$

$$y_7' = c_{1_5} * y_5 + c_{2_6} * y_6 + c_{3_7_kw} * y_7 + c_{4_8} * y_8 + c_{5_9} * y_9 + sw_7,$$

$$y_8' = c_{1_6} * y_6 + c_{2_7} * y_7 + c_{3_8_kw} * y_8 + c_{4_9} * y_9 + c_{5_10} * y_{10} + sw_8,$$

$$y_9' = c_{1_7} * y_7 + c_{2_8} * y_8 + c_{3_9_kw} * y_9 + c_{4_10} * y_{10} + c_{5_11} * y_{11} + sw_9,$$

$$y_{10}' = c_{1_8} * y_8 + c_{2_9} * y_9 + c_{3_10_kw} * y_{10} + c_{4_11} * y_{11} + c_{5_12} * y_{12} + sw_{10},$$

$$y_{11}' = c_{1_9} * y_9 + c_{2_10} * y_{10} + c_{3_11_kw} * y_{11} + c_{4_12} * y_{12} + c_{5_13} * y_{13} + sw_{11},$$

$$y_{12}' = c_{1_10} * y_{10} + c_{2_11} * y_{11} + c_{3_12_kw} * y_{12} + c_{4_13} * y_{13} + c_{5_14} * y_{14} + sw_{12},$$

$$y_{13}' = c_{1_11} * y_{11} + c_{2_12} * y_{12} + c_{3_13_kw} * y_{13} + c_{4_14} * y_{14} + c_{5_15} * y_{15} + sw_{13},$$

$$y_{14}' = c_{1_12} * y_{12} + c_{2_13} * y_{13} + c_{3_14_kw} * y_{14} + c_{4_15} * y_{15} + c_{5_16} * y_{16} + sw_{14},$$

$$y_{15}' = c_{1_13} * y_{13} + c_{2_14} * y_{14} + c_{3_15_kw} * y_{15} + c_{4_16} * y_{16} + c_{5_17} * y_{17} + sw_{15},$$

$$y_{16}' = c_{1_14} * y_{14} + c_{2_15} * y_{15} + c_{3_16_kw} * y_{16} + c_{4_17} * y_{17} + c_{5_18} * y_{18} + sw_{16},$$

$$y_{17}' = c_{1_15} * y_{15} + c_{2_16} * y_{16} + c_{3_17_kw} * y_{17} + c_{4_18} * y_{18} + c_{5_19} * y_{19} + sw_{17},$$

$$y_{18}' = c_{1_16} * y_{16} + c_{2_17} * y_{17} + c_{3_18_kw} * y_{18} + c_{4_19} * y_{19} + c_{5_20} * y_{20} + sw_{18},$$

$$y_{19}' = c_{1_17} * y_{17} + c_{2_18} * y_{18} + c_{3_19_kw} * y_{19} + c_{4_20} * y_{20} + c_{5_21} * y_{21} + sw_{19},$$

$$y_{20}' = c_{1_18} * y_{18} + c_{2_19} * y_{19} + c_{3_20_kw} * y_{20} + c_{4_21} * y_{21} + c_{5_22} * y_{22} + sw_{20},$$

$$y_{21}' = c_{1_19} * y_{19} + c_{2_20} * y_{20} + c_{3_21_kw} * y_{21} + c_{4_22} * y_{22} + c_{5_23} * y_{23} + sw_{21},$$

$$\begin{aligned}
y_{22}' &= c_{1_20} * y_{20} + c_{2_21} * y_{21} + c_{3_22_kw} * y_{22} + c_{4_23} * y_{23} + c_{5_24} * y_{24} + sw_{22}, \\
y_{23}' &= c_{1_21} * y_{21} + c_{2_22} * y_{22} + c_{3_23_kw} * y_{23} + c_{4_24} * y_{24} + c_{5_25} * y_{25} + sw_{23}, \\
y_{24}' &= c_{1_22} * y_{22} + c_{2_23} * y_{23} + c_{3_24_kw} * y_{24} + c_{4_25} * y_{25} + c_{5_26} * y_{26} + sw_{24}, \\
y_{25}' &= c_{1_23} * y_{23} + c_{2_24} * y_{24} + c_{3_25_kw} * y_{25} + c_{4_26} * y_{26} + c_{5_27} * y_{27} + sw_{25}, \\
y_{26}' &= c_{1_24} * y_{24} + c_{2_25} * y_{25} + c_{3_26_kw} * y_{26} + c_{4_27} * y_{27} + c_{5_28} * y_{28} + sw_{26}, \\
y_{27}' &= c_{1_25} * y_{25} + c_{2_26} * y_{26} + c_{3_27_kw} * y_{27} + c_{4_28} * y_{28} + c_{5_29} * y_{29} + sw_{27}, \\
y_{28}' &= c_{1_26} * y_{26} + c_{2_27} * y_{27} + c_{3_28_kw} * y_{28} + c_{4_29} * y_{29} + c_{5_30} * y_{30} + sw_{28}, \\
y_{29}' &= c_{1_27} * y_{27} + c_{2_28} * y_{28} + c_{3_29_kw} * y_{29} + c_{4_30} * y_{30} + c_{5_31} * y_{31} + sw_{29}, \\
y_{30}' &= c_{1_28} * y_{28} + c_{2_29} * y_{29} + c_{3_30_kw} * y_{30} + c_{4_31} * y_{31} + c_{5_32} * y_{32} + sw_{30}, \\
y_{31}' &= c_{1_29} * y_{29} + c_{2_30} * y_{30} + c_{3_31_kw} * y_{31} + c_{4_32} * y_{32} + c_{5_33} * y_{33} + sw_{31}, \\
y_{32}' &= c_{1_30} * y_{30} + c_{2_31} * y_{31} + c_{3_32_kw} * y_{32} + c_{4_33} * y_{33} + c_{5_34} * y_{34} + sw_{32}, \\
y_{33}' &= c_{1_31} * y_{31} + c_{2_32} * y_{32} + c_{3_33_kw} * y_{33} + c_{4_34} * y_{34} + c_{5_35} * y_{35} + sw_{33}, \\
y_{34}' &= c_{1_32} * y_{32} + c_{2_33} * y_{33} + c_{3_34_kw} * y_{34} + c_{4_35} * y_{35} + c_{5_36} * y_{36} + sw_{34}, \\
y_{35}' &= c_{1_33} * y_{33} + c_{2_34} * y_{34} + c_{3_35_kw} * y_{35} + c_{4_36} * y_{36} + c_{5_37} * y_{37} + sw_{35}, \\
y_{36}' &= c_{1_34} * y_{34} + c_{2_35} * y_{35} + c_{3_36_kw} * y_{36} + c_{4_37} * y_{37} + c_{5_38} * y_{38} + sw_{36}, \\
y_{37}' &= c_{1_35} * y_{35} + c_{2_36} * y_{36} + c_{3_37_kw} * y_{37} + c_{4_38} * y_{38} + c_{5_39} * y_{39} + sw_{37}, \\
y_{38}' &= c_{1_36} * y_{36} + c_{2_37} * y_{37} + c_{3_38_kw} * y_{38} + c_{4_39} * y_{39} + c_{5_40} * y_{40} + sw_{38}, \\
y_{39}' &= c_{1_37} * y_{37} + c_{2_38} * y_{38} + c_{3_39_kw} * y_{39} + c_{4a_40} * y_{40} + sw_{39}, \\
y_{40}' &= c_{1_38} * y_{38} + c_{2b_39} * y_{39} + (c_{3b_40} - kw_{40}) * y_{40} + sw_{40},
\end{aligned}$$

; Water volume in the caecum/colon

$$y_{41}' = ((9.0 y_{40} - y_{39}) / 8.0) Q - (kw_{col} + krec) * y_{41} + sw_{col},$$

; Water volume in feces (assumed to be 0)

$$y_{42}' = krec * y_{41},$$

; Water volume in stomach

$$y_{43}' = k_a * y_{50} - (k_g + k_{w_gut}) * y_{43} + s_{w_gut},$$

; Water volume in the upper small intestine (not used in this study)

$$y_{44} = (y_1 + y_2 + y_3 + y_4 + y_5 + y_6 + y_7 + y_8 + y_9 + y_{10} + y_{11} + y_{12} + y_{13} + y_{14} + y_{15} + y_{16} + y_{17} + y_{18} + y_{19} + y_{20} + y_{21} + y_{22} + y_{23} + y_{24}),$$

; Water volume in the lower small intestine (not used in this study)

$$y_{45} = (y_{25} + y_{26} + y_{27} + y_{28} + y_{29} + y_{30} + y_{31} + y_{32} + y_{33} + y_{34} + y_{35} + y_{36} + y_{37} + y_{38} + y_{39} + y_{40}),$$

; Water volume in the whole small intestine

$$y_{46} =$$

$$y_1 + y_2 + y_3 + y_4 + y_5 + y_6 + y_7 + y_8 + y_9 + y_{10} + y_{11} + y_{12} + y_{13} + y_{14} + y_{15} + y_{16} + y_{17} + y_{18} + y_{19} + y_{20} + y_{21} + y_{22} + y_{23} + y_{24} + y_{25} + y_{26} + y_{27} + y_{28} + y_{29} + y_{30} + y_{31} + y_{32} + y_{33} + y_{34} + y_{35} + y_{36} + y_{37} + y_{38} + y_{39} + y_{40},$$

; Water volume in distal jejunum and proximal ileum (not used in this study)

$$y_{48} =$$

$$(y_{12} + y_{13} + y_{14} + y_{15} + y_{16} + y_{17} + y_{18} + y_{19} + y_{20} + y_{21} + y_{22} + y_{23} + y_{24} + y_{25} + y_{26} + y_{27} + y_{28} + y_{29} + y_{30}),$$

; Water volume in distal ileum (not used in this study)

$$y_{49} = (y_{31} + y_{32} + y_{33} + y_{34} + y_{35} + y_{36} + y_{37} + y_{38} + y_{39} + y_{40}),$$

; Water volume in the esophagus)

$$y50' = -ka*y50,$$

; Following is the codes about a substrate

; Drug concentration in the small intestine

$$y51' = (kg * y93) * Vg \text{ div} / V + c3a_1*y51 + c4a_2*y52 + c5_3*y53 -$$

$$PSap1*y51/y1+PSax1*fent*y101/Vent1/(V/div),$$

if y51 < 0 then y51=0 endif,

$$y52' = c2a_1*y51 + c3_2*y52 + c4_3*y53 + c5_4*y54 -$$

$$PSap2*y52/y2+PSax2*fent*y102/Vent2/(V/div),$$

if y52 < 0 then y52=0 endif,

$$y53' = c1_1*y51 + c2_2*y52 + c3_3*y53 + c4_4*y54 + c5_5*y55 -$$

$$PSap3*y53/y3+PSax3*fent*y103/Vent3/(V/div),$$

if y53 < 0 then y53=0 endif,

$$y54' = c1_2*y52 + c2_3*y53 + c3_4*y54 + c4_5*y55 + c5_6*y56 -$$

$$PSap4*y54/y4+PSax4*fent*y104/Vent4/(V/div),$$

if y54 < 0 then y54=0 endif,

$$y55' = c1_3*y53 + c2_4*y54 + c3_5*y55 + c4_6*y56 + c5_7*y57 -$$

$$PSap5*y55/y5+PSax5*fent*y105/Vent5/(V/div),$$

if y55 < 0 then y55=0 endif,

$$y56' = c1_4*y54 + c2_5*y55 + c3_6*y56 + c4_7*y57 + c5_8*y58 -$$

$$PSap6*y56/y6+PSax6*fent*y106/Vent6/(V/div),$$

if y56 < 0 then y56=0 endif,

$$y57' = c1_5*y55 + c2_6*y56 + c3_7*y57 + c4_8*y58 + c5_9*y59 -$$

$$PSap7*y57/y7+PSax7*fent*y107/Vent7/(V/div),$$

if y57 < 0 then y57=0 endif,

$$y58' = c1_6*y56 + c2_7*y57 + c3_8*y58 + c4_9*y59 + c5_10*y60 -$$

$$PSap8*y58/y8 + PSax8*fent*y108/Vent8/(V/div),$$

if y58 < 0 then y58=0 endif,

$$y59' = c1_7*y57 + c2_8*y58 + c3_9*y59 + c4_10*y60 + c5_11*y61 -$$

$$PSap9*y59/y9 + PSax9*fent*y109/Vent9/(V/div),$$

if y59 < 0 then y59=0 endif,

$$y60' = c1_8*y58 + c2_9*y59 + c3_10*y60 + c4_11*y61 + c5_12*y62 -$$

$$PSap10*y60/y10 + PSax10*fent*y110/Vent10/(V/div),$$

if y60 < 0 then y60=0 endif,

$$y61' = c1_9*y59 + c2_10*y60 + c3_11*y61 + c4_12*y62 + c5_13*y63 -$$

$$PSap11*y61/y11 + PSax11*fent*y111/Vent11/(V/div),$$

if y61 < 0 then y61=0 endif,

$$y62' = c1_10*y60 + c2_11*y61 + c3_12*y62 + c4_13*y63 + c5_14*y64 -$$

$$PSap12*y62/y12 + PSax12*fent*y112/Vent12/(V/div),$$

if y62 < 0 then y62=0 endif,

$$y63' = c1_11*y61 + c2_12*y62 + c3_13*y63 + c4_14*y64 + c5_15*y65 -$$

$$PSap13*y63/y13 + PSax13*fent*y113/Vent13/(V/div),$$

if y63 < 0 then y63=0 endif,

$$y64' = c1_12*y62 + c2_13*y63 + c3_14*y64 + c4_15*y65 + c5_16*y66 -$$

$$PSap14*y64/y14 + PSax14*fent*y114/Vent14/(V/div),$$

if y64 < 0 then y64=0 endif,

$$y65' = c1_13*y63 + c2_14*y64 + c3_15*y65 + c4_16*y66 + c5_17*y67 -$$

$$PSap15*y65/y15 + PSax15*fent*y115/Vent15/(V/div),$$

if y65 < 0 then y65=0 endif,

$$y66' = c1_{14}*y64 + c2_{15}*y65 + c3_{16}*y66 + c4_{17}*y67 + c5_{18}*y68-$$

$$PSap16*y66/y16+PSax16*fent*y116/Vent16/(V/div),$$

if y66 < 0 then y66=0 endif,

$$y67' = c1_{15}*y65 + c2_{16}*y66 + c3_{17}*y67 + c4_{18}*y68 + c5_{19}*y69-$$

$$PSap17*y67/y17+PSax17*fent*y117/Vent17/(V/div),$$

if y67 < 0 then y67=0 endif,

$$y68' = c1_{16}*y66 + c2_{17}*y67 + c3_{18}*y68 + c4_{19}*y69 + c5_{20}*y70-$$

$$PSap18*y68/y18+PSax18*fent*y118/Vent18/(V/div),$$

if y68 < 0 then y68=0 endif,

$$y69' = c1_{17}*y67 + c2_{18}*y68 + c3_{19}*y69 + c4_{20}*y70 + c5_{21}*y71-$$

$$PSap19*y69/y19+PSax19*fent*y119/Vent19/(V/div),$$

if y69 < 0 then y69=0 endif,

$$y70' = c1_{18}*y68 + c2_{19}*y69 + c3_{20}*y70 + c4_{21}*y71 + c5_{22}*y72-$$

$$PSap20*y70/y20+PSax20*fent*y120/Vent20/(V/div),$$

if y70 < 0 then y70=0 endif,

$$y71' = c1_{19}*y69 + c2_{20}*y70 + c3_{21}*y71 + c4_{22}*y72 + c5_{23}*y73-$$

$$PSap21*y71/y21+PSax21*fent*y121/Vent21/(V/div),$$

if y71 < 0 then y71=0 endif,

$$y72' = c1_{20}*y70 + c2_{21}*y71 + c3_{22}*y72 + c4_{23}*y73 + c5_{24}*y74-$$

$$PSap22*y72/y22+PSax22*fent*y122/Vent22/(V/div),$$

if y72 < 0 then y72=0 endif,

$$y73' = c1_{21}*y71 + c2_{22}*y72 + c3_{23}*y73 + c4_{24}*y74 + c5_{25}*y75-$$

$$PSap23*y73/y23+PSax23*fent*y123/Vent23/(V/div),$$

if y73 < 0 then y73=0 endif,

$$y74' = c1_22*y72 + c2_23*y73 + c3_24*y74 + c4_25*y75 + c5_26*y76 -$$

$$PSap24*y74/y24 + PSax24*fent*y124/Vent24/(V/div),$$

if y74 < 0 then y74=0 endif,

$$y75' = c1_23*y73 + c2_24*y74 + c3_25*y75 + c4_26*y76 + c5_27*y77 -$$

$$PSap25*y75/y25 + PSax25*fent*y125/Vent25/(V/div),$$

if y75 < 0 then y75=0 endif,

$$y76' = c1_24*y74 + c2_25*y75 + c3_26*y76 + c4_27*y77 + c5_28*y78 -$$

$$PSap26*y76/y26 + PSax26*fent*y126/Vent26/(V/div),$$

if y76 < 0 then y76=0 endif,

$$y77' = c1_25*y75 + c2_26*y76 + c3_27*y77 + c4_28*y78 + c5_29*y79 -$$

$$PSap27*y77/y27 + PSax27*fent*y127/Vent27/(V/div),$$

if y77 < 0 then y77=0 endif,

$$y78' = c1_26*y76 + c2_27*y77 + c3_28*y78 + c4_29*y79 + c5_30*y80 -$$

$$PSap28*y78/y28 + PSax28*fent*y128/Vent28/(V/div),$$

if y78 < 0 then y78=0 endif,

$$y79' = c1_27*y77 + c2_28*y78 + c3_29*y79 + c4_30*y80 + c5_31*y81 -$$

$$PSap29*y79/y29 + PSax29*fent*y129/Vent29/(V/div),$$

if y79 < 0 then y79=0 endif,

$$y80' = c1_28*y78 + c2_29*y79 + c3_30*y80 + c4_31*y81 + c5_32*y82 -$$

$$PSap30*y80/y30 + PSax30*fent*y130/Vent30/(V/div),$$

if y80 < 0 then y80=0 endif,

$$y81' = c1_29*y79 + c2_30*y80 + c3_31*y81 + c4_32*y82 + c5_33*y83 -$$

$$PSap31*y81/y31 + PSax31*fent*y131/Vent31/(V/div),$$

if y81 < 0 then y81=0 endif,

$$y_{82}' = c_{1_30} * y_{80} + c_{2_31} * y_{81} + c_{3_32} * y_{82} + c_{4_33} * y_{83} + c_{5_34} * y_{84} -$$

$$PSap_{32} * y_{82} / y_{32} + PSax_{32} * fent * y_{132} / Vent_{32} / (V / div),$$

if $y_{82} < 0$ then $y_{82} = 0$ endif,

$$y_{83}' = c_{1_31} * y_{81} + c_{2_32} * y_{82} + c_{3_33} * y_{83} + c_{4_34} * y_{84} + c_{5_35} * y_{85} -$$

$$PSap_{33} * y_{83} / y_{33} + PSax_{33} * fent * y_{133} / Vent_{33} / (V / div),$$

if $y_{83} < 0$ then $y_{83} = 0$ endif,

$$y_{84}' = c_{1_32} * y_{82} + c_{2_33} * y_{83} + c_{3_34} * y_{84} + c_{4_35} * y_{85} + c_{5_36} * y_{86} -$$

$$PSap_{34} * y_{84} / y_{34} + PSax_{34} * fent * y_{134} / Vent_{34} / (V / div),$$

if $y_{84} < 0$ then $y_{84} = 0$ endif,

$$y_{85}' = c_{1_33} * y_{83} + c_{2_34} * y_{84} + c_{3_35} * y_{85} + c_{4_36} * y_{86} + c_{5_37} * y_{87} -$$

$$PSap_{35} * y_{85} / y_{35} + PSax_{35} * fent * y_{135} / Vent_{35} / (V / div),$$

if $y_{85} < 0$ then $y_{85} = 0$ endif,

$$y_{86}' = c_{1_34} * y_{84} + c_{2_35} * y_{85} + c_{3_36} * y_{86} + c_{4_37} * y_{87} + c_{5_38} * y_{88} -$$

$$PSap_{36} * y_{86} / y_{36} + PSax_{36} * fent * y_{136} / Vent_{36} / (V / div),$$

if $y_{86} < 0$ then $y_{86} = 0$ endif,

$$y_{87}' = c_{1_35} * y_{85} + c_{2_36} * y_{86} + c_{3_37} * y_{87} + c_{4_38} * y_{88} + c_{5_39} * y_{89} -$$

$$PSap_{37} * y_{87} / y_{37} + PSax_{37} * fent * y_{137} / Vent_{37} / (V / div),$$

if $y_{87} < 0$ then $y_{87} = 0$ endif,

$$y_{88}' = c_{1_36} * y_{86} + c_{2_37} * y_{87} + c_{3_38} * y_{88} + c_{4_39} * y_{89} + c_{5_40} * y_{90} -$$

$$PSap_{38} * y_{88} / y_{38} + PSax_{38} * fent * y_{138} / Vent_{38} / (V / div),$$

if $y_{88} < 0$ then $y_{88} = 0$ endif,

$$y_{89}' = c_{1_37} * y_{87} + c_{2_38} * y_{88} + c_{3_39} * y_{89} + c_{4a_40} * y_{90} -$$

$$PSap_{39} * y_{89} / y_{39} + PSax_{39} * fent * y_{139} / Vent_{39} / (V / div),$$

if $y_{89} < 0$ then $y_{89} = 0$ endif,

$$y90' = c1_{38} * y88 + c2b_{39} * y89 + c3b_{40} * y90 -$$

$$PSap40 * y90 / y40 + PSax40 * fent * y140 / Vent40 / (V / div),$$

if $y90 < 0$ then $y90 = 0$ endif,

; Drug amount in the colon

$$y91' = ((9.0 * y90 - y89) / 8.0) * Q - krec * y91,$$

; Drug amount in the feces

$$y92' = krec * y91 * Vcaecol,$$

; Drug concentration in the stomach

$$y93' = ka * y100 * Ves / Vg - kg * y93,$$

; % of dose in stomach (used in the analysis of ^{99m}Tc -DTPA)

$$y94 = y93 * Vg / dose * 100,$$

; % of dose in jejunum (used in the analysis of ^{99m}Tc -DTPA)

$$y95 = (y51 + y52 + y53 + y54 + y55 + y56 + y57 + y58 + y59 + y60 + y61 + y62 + y63 + y64 + y65 + y66 + y67 + y68 + y69 + y70) * V / div / dose * 100,$$

; % of dose in ileum (used in the analysis of ^{99m}Tc -DTPA)

$$y96 = (y71 + y72 + y73 + y74 + y75 + y76 + y77 + y78 + y79 + y80 + y81 + y82 + y83 + y84 + y85 + y86 + y87 + y88 + y89 + y90) * V / div / dose * 100,$$

; % of dose in colon (used in the analysis of ^{99m}Tc -DTPA)

$$y97 = y91 Vc / dose * 100,$$

; % of dose in whole lumen (not used in this study)

$$y98 = y95 + y96 + y97,$$

; Drug amount in the gastrointestinal tract (not used in this study)

$$y99 = y94 + y95 + y96 + y97,$$

; Drug concentration in the esophagus

$$y100' = -ka * y100,$$

; Drug amount in the enterocytes

$$y101' = PSap1 * y51 * (V/div) / y1 - (PSax1 + CL1 + PSbp1) * fent * y101 / Vent1 + PSbx1 * y141 / Vlam1,$$

if y101 < 0 then y101=0 endif,

$$y102' = PSap2 * y52 * (V/div) / y2 - (PSax2 + CL2 + PSbp2) * fent * y102 / Vent2 + PSbx2 * y142 / Vlam2,$$

if y102 < 0 then y102=0 endif,

$$y103' = PSap3 * y53 * (V/div) / y3 - (PSax3 + CL3 + PSbp3) * fent * y103 / Vent3 + PSbx3 * y143 / Vlam3,$$

if y103 < 0 then y103=0 endif,

$$y104' = PSap4 * y54 * (V/div) / y4 - (PSax4 + CL4 + PSbp4) * fent * y104 / Vent4 + PSbx4 * y144 / Vlam4,$$

if y104 < 0 then y104=0 endif,

$$y105' = PSap5 * y55 * (V/div) / y5 - (PSax5 + CL5 + PSbp5) * fent * y105 / Vent5 + PSbx5 * y145 / Vlam5,$$

if y105 < 0 then y105=0 endif,

$$y106' = PSap6 * y56 * (V/div) / y6 - (PSax6 + CL6 + PSbp6) * fent * y106 / Vent6 + PSbx6 * y146 / Vlam6,$$

if y106 < 0 then y106=0 endif,

$$y107' = PSap7 * y57 * (V/div) / y7 - (PSax7 + CL7 + PSbp7) * fent * y107 / Vent7 + PSbx7 * y147 / Vlam7,$$

if $y_{107} < 0$ then $y_{107}=0$ endif,
 $y_{108}'=PSap8*y_{58}*(V/div)/y_8-(PSax8+CL8+PSbp8)*fent*y_{108}/Vent8+PSbx8*y_{148}/Vlam8,$
 if $y_{108} < 0$ then $y_{108}=0$ endif,
 $y_{109}'=PSap9*y_{59}*(V/div)/y_9-(PSax9+CL9+PSbp9)*fent*y_{109}/Vent9+PSbx9*y_{149}/Vlam9,$
 if $y_{109} < 0$ then $y_{109}=0$ endif,
 $y_{110}'=PSap10*y_{60}*(V/div)/y_{10}-$
 $(PSax10+CL10+PSbp10)*fent*y_{110}/Vent10+PSbx10*y_{150}/Vlam10,$
 if $y_{110} < 0$ then $y_{110}=0$ endif,
 $y_{111}'=PSap11*y_{61}*(V/div)/y_{11}-$
 $(PSax11+CL11+PSbp11)*fent*y_{111}/Vent11+PSbx11*y_{151}/Vlam11,$
 if $y_{111} < 0$ then $y_{111}=0$ endif,
 $y_{112}'=PSap12*y_{62}*(V/div)/y_{12}-$
 $(PSax12+CL12+PSbp12)*fent*y_{112}/Vent12+PSbx12*y_{152}/Vlam12,$
 if $y_{112} < 0$ then $y_{112}=0$ endif,
 $y_{113}'=PSap13*y_{63}*(V/div)/y_{13}-$
 $(PSax13+CL13+PSbp13)*fent*y_{113}/Vent13+PSbx13*y_{153}/Vlam13,$
 if $y_{113} < 0$ then $y_{113}=0$ endif,
 $y_{114}'=PSap14*y_{64}*(V/div)/y_{14}-$
 $(PSax14+CL14+PSbp14)*fent*y_{114}/Vent14+PSbx14*y_{154}/Vlam14,$
 if $y_{114} < 0$ then $y_{114}=0$ endif,
 $y_{115}'=PSap15*y_{65}*(V/div)/y_{15}-$
 $(PSax15+CL15+PSbp15)*fent*y_{115}/Vent15+PSbx15*y_{155}/Vlam15,$
 if $y_{115} < 0$ then $y_{115}=0$ endif,
 $y_{116}'=PSap16*y_{66}*(V/div)/y_{16}-$
 $(PSax16+CL16+PSbp16)*fent*y_{116}/Vent16+PSbx16*y_{156}/Vlam16,$

if $y_{116} < 0$ then $y_{116}=0$ endif,
 $y_{117}'=PS_{ap17} \cdot y_{67} \cdot (V/div)/y_{17}-$
 $(PS_{ax17}+CL_{17}+PS_{bp17}) \cdot f_{ent} \cdot y_{117}/Vent_{17}+PS_{bx17} \cdot y_{157}/V_{lam17},$
 if $y_{117} < 0$ then $y_{117}=0$ endif,
 $y_{118}'=PS_{ap18} \cdot y_{68} \cdot (V/div)/y_{18}-$
 $(PS_{ax18}+CL_{18}+PS_{bp18}) \cdot f_{ent} \cdot y_{118}/Vent_{18}+PS_{bx18} \cdot y_{158}/V_{lam18},$
 if $y_{118} < 0$ then $y_{118}=0$ endif,
 $y_{119}'=PS_{ap19} \cdot y_{69} \cdot (V/div)/y_{19}-$
 $(PS_{ax19}+CL_{19}+PS_{bp19}) \cdot f_{ent} \cdot y_{119}/Vent_{19}+PS_{bx19} \cdot y_{159}/V_{lam19},$
 if $y_{119} < 0$ then $y_{119}=0$ endif,
 $y_{120}'=PS_{ap20} \cdot y_{70} \cdot (V/div)/y_{20}-$
 $(PS_{ax20}+CL_{20}+PS_{bp20}) \cdot f_{ent} \cdot y_{120}/Vent_{20}+PS_{bx20} \cdot y_{160}/V_{lam20},$
 if $y_{120} < 0$ then $y_{120}=0$ endif,
 $y_{121}'=PS_{ap21} \cdot y_{71} \cdot (V/div)/y_{21}-$
 $(PS_{ax21}+CL_{21}+PS_{bp21}) \cdot f_{ent} \cdot y_{121}/Vent_{21}+PS_{bx21} \cdot y_{161}/V_{lam21},$
 if $y_{121} < 0$ then $y_{121}=0$ endif,
 $y_{122}'=PS_{ap22} \cdot y_{72} \cdot (V/div)/y_{22}-$
 $(PS_{ax22}+CL_{22}+PS_{bp22}) \cdot f_{ent} \cdot y_{122}/Vent_{22}+PS_{bx22} \cdot y_{162}/V_{lam22},$
 if $y_{122} < 0$ then $y_{122}=0$ endif,
 $y_{123}'=PS_{ap23} \cdot y_{73} \cdot (V/div)/y_{23}-$
 $(PS_{ax23}+CL_{23}+PS_{bp23}) \cdot f_{ent} \cdot y_{123}/Vent_{23}+PS_{bx23} \cdot y_{163}/V_{lam23},$
 if $y_{123} < 0$ then $y_{123}=0$ endif,
 $y_{124}'=PS_{ap24} \cdot y_{74} \cdot (V/div)/y_{24}-$
 $(PS_{ax24}+CL_{24}+PS_{bp24}) \cdot f_{ent} \cdot y_{124}/Vent_{24}+PS_{bx24} \cdot y_{164}/V_{lam24},$
 if $y_{124} < 0$ then $y_{124}=0$ endif,

$y_{125}' = PS_{ap25} * y_{75} * (V/div) / y_{25} -$
 $(PS_{ax25} + CL_{25} + PS_{bp25}) * f_{ent} * y_{125} / Vent_{25} + PS_{bx25} * y_{165} / V_{lam25},$
 if $y_{125} < 0$ then $y_{125} = 0$ endif,
 $y_{126}' = PS_{ap26} * y_{76} * (V/div) / y_{26} -$
 $(PS_{ax26} + CL_{26} + PS_{bp26}) * f_{ent} * y_{126} / Vent_{26} + PS_{bx26} * y_{166} / V_{lam26},$
 if $y_{126} < 0$ then $y_{126} = 0$ endif,
 $y_{127}' = PS_{ap27} * y_{77} * (V/div) / y_{27} -$
 $(PS_{ax27} + CL_{27} + PS_{bp27}) * f_{ent} * y_{127} / Vent_{27} + PS_{bx27} * y_{167} / V_{lam27},$
 if $y_{127} < 0$ then $y_{127} = 0$ endif,
 $y_{128}' = PS_{ap28} * y_{78} * (V/div) / y_{28} -$
 $(PS_{ax28} + CL_{28} + PS_{bp28}) * f_{ent} * y_{128} / Vent_{28} + PS_{bx28} * y_{168} / V_{lam28},$
 if $y_{128} < 0$ then $y_{128} = 0$ endif,
 $y_{129}' = PS_{ap29} * y_{79} * (V/div) / y_{29} -$
 $(PS_{ax29} + CL_{29} + PS_{bp29}) * f_{ent} * y_{129} / Vent_{29} + PS_{bx29} * y_{169} / V_{lam29},$
 if $y_{129} < 0$ then $y_{129} = 0$ endif,
 $y_{130}' = PS_{ap30} * y_{80} * (V/div) / y_{30} -$
 $(PS_{ax30} + CL_{30} + PS_{bp30}) * f_{ent} * y_{130} / Vent_{30} + PS_{bx30} * y_{170} / V_{lam30},$
 if $y_{130} < 0$ then $y_{130} = 0$ endif,
 $y_{131}' = PS_{ap31} * y_{81} * (V/div) / y_{31} -$
 $(PS_{ax31} + CL_{31} + PS_{bp31}) * f_{ent} * y_{131} / Vent_{31} + PS_{bx31} * y_{171} / V_{lam31},$
 if $y_{131} < 0$ then $y_{131} = 0$ endif,
 $y_{132}' = PS_{ap32} * y_{82} * (V/div) / y_{32} -$
 $(PS_{ax32} + CL_{32} + PS_{bp32}) * f_{ent} * y_{132} / Vent_{32} + PS_{bx32} * y_{172} / V_{lam32},$
 if $y_{132} < 0$ then $y_{132} = 0$ endif,

$y_{133}' = PS_{ap33} * y_{83} * (V/div) / y_{33}$
 $(PS_{ax33} + CL_{33} + PS_{bp33}) * f_{ent} * y_{133} / Vent_{33} + PS_{bx33} * y_{173} / V_{lam33}$,
 if $y_{133} < 0$ then $y_{133} = 0$ endif,
 $y_{134}' = PS_{ap34} * y_{84} * (V/div) / y_{34}$
 $(PS_{ax34} + CL_{34} + PS_{bp34}) * f_{ent} * y_{134} / Vent_{34} + PS_{bx34} * y_{174} / V_{lam34}$,
 if $y_{134} < 0$ then $y_{134} = 0$ endif,
 $y_{135}' = PS_{ap35} * y_{85} * (V/div) / y_{35}$
 $(PS_{ax35} + CL_{35} + PS_{bp35}) * f_{ent} * y_{135} / Vent_{35} + PS_{bx35} * y_{175} / V_{lam35}$,
 if $y_{135} < 0$ then $y_{135} = 0$ endif,
 $y_{136}' = PS_{ap36} * y_{86} * (V/div) / y_{36}$
 $(PS_{ax36} + CL_{36} + PS_{bp36}) * f_{ent} * y_{136} / Vent_{36} + PS_{bx36} * y_{176} / V_{lam36}$,
 if $y_{136} < 0$ then $y_{136} = 0$ endif,
 $y_{137}' = PS_{ap37} * y_{87} * (V/div) / y_{37}$
 $(PS_{ax37} + CL_{37} + PS_{bp37}) * f_{ent} * y_{137} / Vent_{37} + PS_{bx37} * y_{177} / V_{lam37}$,
 if $y_{137} < 0$ then $y_{137} = 0$ endif,
 $y_{138}' = PS_{ap38} * y_{88} * (V/div) / y_{38}$
 $(PS_{ax38} + CL_{38} + PS_{bp38}) * f_{ent} * y_{138} / Vent_{38} + PS_{bx38} * y_{178} / V_{lam38}$,
 if $y_{138} < 0$ then $y_{138} = 0$ endif,
 $y_{139}' = PS_{ap39} * y_{89} * (V/div) / y_{39}$
 $(PS_{ax39} + CL_{39} + PS_{bp39}) * f_{ent} * y_{139} / Vent_{39} + PS_{bx39} * y_{179} / V_{lam39}$,
 if $y_{139} < 0$ then $y_{139} = 0$ endif,
 $y_{140}' = PS_{ap40} * y_{90} * (V/div) / y_{40}$
 $(PS_{ax40} + CL_{40} + PS_{bp40}) * f_{ent} * y_{140} / Vent_{40} + PS_{bx40} * y_{180} / V_{lam40}$,
 if $y_{140} < 0$ then $y_{140} = 0$ endif,

; Drug amount in the lamina propria

$$y_{141}' = PS_{bp1} * fent * y_{101} / Vent1 - (Q_{lam1} / fb + PS_{bx1}) * y_{141} / V_{lam1},$$

if $y_{141} < 0$ then $y_{141} = 0$ endif,

$$y_{142}' = PS_{bp2} * fent * y_{102} / Vent2 - (Q_{lam2} / fb + PS_{bx2}) * y_{142} / V_{lam2},$$

if $y_{142} < 0$ then $y_{142} = 0$ endif,

$$y_{143}' = PS_{bp3} * fent * y_{103} / Vent3 - (Q_{lam3} / fb + PS_{bx3}) * y_{143} / V_{lam3},$$

if $y_{143} < 0$ then $y_{143} = 0$ endif,

$$y_{144}' = PS_{bp4} * fent * y_{104} / Vent4 - (Q_{lam4} / fb + PS_{bx4}) * y_{144} / V_{lam4},$$

if $y_{144} < 0$ then $y_{144} = 0$ endif,

$$y_{145}' = PS_{bp5} * fent * y_{105} / Vent5 - (Q_{lam5} / fb + PS_{bx5}) * y_{145} / V_{lam5},$$

if $y_{145} < 0$ then $y_{145} = 0$ endif,

$$y_{146}' = PS_{bp6} * fent * y_{106} / Vent6 - (Q_{lam6} / fb + PS_{bx6}) * y_{146} / V_{lam6},$$

if $y_{146} < 0$ then $y_{146} = 0$ endif,

$$y_{147}' = PS_{bp7} * fent * y_{107} / Vent7 - (Q_{lam7} / fb + PS_{bx7}) * y_{147} / V_{lam7},$$

if $y_{147} < 0$ then $y_{147} = 0$ endif,

$$y_{148}' = PS_{bp8} * fent * y_{108} / Vent8 - (Q_{lam8} / fb + PS_{bx8}) * y_{148} / V_{lam8},$$

if $y_{148} < 0$ then $y_{148} = 0$ endif,

$$y_{149}' = PS_{bp9} * fent * y_{109} / Vent9 - (Q_{lam9} / fb + PS_{bx9}) * y_{149} / V_{lam9},$$

if $y_{149} < 0$ then $y_{149} = 0$ endif,

$$y_{150}' = PS_{bp10} * fent * y_{110} / Vent10 - (Q_{lam10} / fb + PS_{bx10}) * y_{150} / V_{lam10},$$

if $y_{150} < 0$ then $y_{150} = 0$ endif,

$$y_{151}' = PS_{bp11} * fent * y_{111} / Vent11 - (Q_{lam11} / fb + PS_{bx11}) * y_{151} / V_{lam11},$$

if $y_{151} < 0$ then $y_{151} = 0$ endif,

$$y_{152}' = PS_{bp12} * fent * y_{112} / Vent12 - (Q_{lam12} / fb + PS_{bx12}) * y_{152} / V_{lam12},$$

if $y_{152} < 0$ then $y_{152} = 0$ endif,

$y_{153}' = PS_{bp13} * f_{ent} * y_{113} / Vent_{13} - (Q_{lam13} / fb + PS_{bx13}) * y_{153} / V_{lam13}$,
 if $y_{153} < 0$ then $y_{153} = 0$ endif,
 $y_{154}' = PS_{bp14} * f_{ent} * y_{114} / Vent_{14} - (Q_{lam14} / fb + PS_{bx14}) * y_{154} / V_{lam14}$,
 if $y_{154} < 0$ then $y_{154} = 0$ endif,
 $y_{155}' = PS_{bp15} * f_{ent} * y_{115} / Vent_{15} - (Q_{lam15} / fb + PS_{bx15}) * y_{155} / V_{lam15}$,
 if $y_{155} < 0$ then $y_{155} = 0$ endif,
 $y_{156}' = PS_{bp16} * f_{ent} * y_{116} / Vent_{16} - (Q_{lam16} / fb + PS_{bx16}) * y_{156} / V_{lam16}$,
 if $y_{156} < 0$ then $y_{156} = 0$ endif,
 $y_{157}' = PS_{bp17} * f_{ent} * y_{117} / Vent_{17} - (Q_{lam17} / fb + PS_{bx17}) * y_{157} / V_{lam17}$,
 if $y_{157} < 0$ then $y_{157} = 0$ endif,
 $y_{158}' = PS_{bp18} * f_{ent} * y_{118} / Vent_{18} - (Q_{lam18} / fb + PS_{bx18}) * y_{158} / V_{lam18}$,
 if $y_{158} < 0$ then $y_{158} = 0$ endif,
 $y_{159}' = PS_{bp19} * f_{ent} * y_{119} / Vent_{19} - (Q_{lam19} / fb + PS_{bx19}) * y_{159} / V_{lam19}$,
 if $y_{159} < 0$ then $y_{159} = 0$ endif,
 $y_{160}' = PS_{bp20} * f_{ent} * y_{120} / Vent_{20} - (Q_{lam20} / fb + PS_{bx20}) * y_{160} / V_{lam20}$,
 if $y_{160} < 0$ then $y_{160} = 0$ endif,
 $y_{161}' = PS_{bp21} * f_{ent} * y_{121} / Vent_{21} - (Q_{lam21} / fb + PS_{bx21}) * y_{161} / V_{lam21}$,
 if $y_{161} < 0$ then $y_{161} = 0$ endif,
 $y_{162}' = PS_{bp22} * f_{ent} * y_{122} / Vent_{22} - (Q_{lam22} / fb + PS_{bx22}) * y_{162} / V_{lam22}$,
 if $y_{162} < 0$ then $y_{162} = 0$ endif,
 $y_{163}' = PS_{bp23} * f_{ent} * y_{123} / Vent_{23} - (Q_{lam23} / fb + PS_{bx23}) * y_{163} / V_{lam23}$,
 if $y_{163} < 0$ then $y_{163} = 0$ endif,
 $y_{164}' = PS_{bp24} * f_{ent} * y_{124} / Vent_{24} - (Q_{lam24} / fb + PS_{bx24}) * y_{164} / V_{lam24}$,
 if $y_{164} < 0$ then $y_{164} = 0$ endif,
 $y_{165}' = PS_{bp25} * f_{ent} * y_{125} / Vent_{25} - (Q_{lam25} / fb + PS_{bx25}) * y_{165} / V_{lam25}$,

if $y_{165} < 0$ then $y_{165}=0$ endif,
 $y_{166}' = PS_{bp26} * fent * y_{126} / Vent_{26} - (Q_{lam26} / fb + PS_{bx26}) * y_{166} / V_{lam26}$,
 if $y_{166} < 0$ then $y_{166}=0$ endif,
 $y_{167}' = PS_{bp27} * fent * y_{127} / Vent_{27} - (Q_{lam27} / fb + PS_{bx27}) * y_{167} / V_{lam27}$,
 if $y_{167} < 0$ then $y_{167}=0$ endif,
 $y_{168}' = PS_{bp28} * fent * y_{128} / Vent_{28} - (Q_{lam28} / fb + PS_{bx28}) * y_{168} / V_{lam28}$,
 if $y_{168} < 0$ then $y_{168}=0$ endif,
 $y_{169}' = PS_{bp29} * fent * y_{129} / Vent_{29} - (Q_{lam29} / fb + PS_{bx29}) * y_{169} / V_{lam29}$,
 if $y_{169} < 0$ then $y_{169}=0$ endif,
 $y_{170}' = PS_{bp30} * fent * y_{130} / Vent_{30} - (Q_{lam30} / fb + PS_{bx30}) * y_{170} / V_{lam30}$,
 if $y_{170} < 0$ then $y_{170}=0$ endif,
 $y_{171}' = PS_{bp31} * fent * y_{131} / Vent_{31} - (Q_{lam31} / fb + PS_{bx31}) * y_{171} / V_{lam31}$,
 if $y_{171} < 0$ then $y_{171}=0$ endif,
 $y_{172}' = PS_{bp32} * fent * y_{132} / Vent_{32} - (Q_{lam32} / fb + PS_{bx32}) * y_{172} / V_{lam32}$,
 if $y_{172} < 0$ then $y_{172}=0$ endif,
 $y_{173}' = PS_{bp33} * fent * y_{133} / Vent_{33} - (Q_{lam33} / fb + PS_{bx33}) * y_{173} / V_{lam33}$,
 if $y_{173} < 0$ then $y_{173}=0$ endif,
 $y_{174}' = PS_{bp34} * fent * y_{134} / Vent_{34} - (Q_{lam34} / fb + PS_{bx34}) * y_{174} / V_{lam34}$,
 if $y_{174} < 0$ then $y_{174}=0$ endif,
 $y_{175}' = PS_{bp35} * fent * y_{135} / Vent_{35} - (Q_{lam35} / fb + PS_{bx35}) * y_{175} / V_{lam35}$,
 if $y_{175} < 0$ then $y_{175}=0$ endif,
 $y_{176}' = PS_{bp36} * fent * y_{136} / Vent_{36} - (Q_{lam36} / fb + PS_{bx36}) * y_{176} / V_{lam36}$,
 if $y_{176} < 0$ then $y_{176}=0$ endif,
 $y_{177}' = PS_{bp37} * fent * y_{137} / Vent_{37} - (Q_{lam37} / fb + PS_{bx37}) * y_{177} / V_{lam37}$,
 if $y_{177} < 0$ then $y_{177}=0$ endif,

$$y178' = PS_{bp38} * f_{ent} * y138 / V_{ent38} - (Q_{lam38} / f_b + PS_{bx38}) * y178 / V_{lam38},$$

if $y178 < 0$ then $y178=0$ endif,

$$y179' = PS_{bp39} * f_{ent} * y139 / V_{ent39} - (Q_{lam39} / f_b + PS_{bx39}) * y179 / V_{lam39},$$

if $y179 < 0$ then $y179=0$ endif,

$$y180' = PS_{bp40} * f_{ent} * y140 / V_{ent40} - (Q_{lam40} / f_b + PS_{bx40}) * y180 / V_{lam40},$$

if $y180 < 0$ then $y180=0$ endif,

; Drug accumulated amount in the portal vein

$$y181' =$$

$$\begin{aligned} & (y141 / V_{lam1} * Q_{lam1} + y142 / V_{lam2} * Q_{lam2} + y143 / V_{lam3} * Q_{lam3} + y144 / V_{lam4} * Q_{lam4} + y145 \\ & / V_{lam5} * Q_{lam5} + y146 / V_{lam6} * Q_{lam6} + y147 / V_{lam7} * Q_{lam7} + y148 / V_{lam8} * Q_{lam8} + y149 / V_{la} \\ & m9 * Q_{lam9} + y150 / V_{lam10} * Q_{lam10} + y151 / V_{lam11} * Q_{lam11} + y152 / V_{lam12} * Q_{lam12} + y153 / V_{la} \\ & m13 * Q_{lam13} + y154 / V_{lam14} * Q_{lam14} + y155 / V_{lam15} * Q_{lam15} + y156 / V_{lam16} * Q_{lam16} + y1 \\ & 57 / V_{lam17} * Q_{lam17} + y158 / V_{lam18} * Q_{lam18} + y159 / V_{lam19} * Q_{lam19} + y160 / V_{lam20} * Q_{lam20} \\ & + y161 / V_{lam21} * Q_{lam21} + y162 / V_{lam22} * Q_{lam22} + y163 / V_{lam23} * Q_{lam23} + y164 / V_{lam24} * Q_{la} \\ & m24 + y165 / V_{lam25} * Q_{lam25} + y166 / V_{lam26} * Q_{lam26} + y167 / V_{lam27} * Q_{lam27} + y168 / V_{lam28} \\ & * Q_{lam28} + y169 / V_{lam29} * Q_{lam29} + y170 / V_{lam30} * Q_{lam30} + y171 / V_{lam31} * Q_{lam31} + y172 / V_{la} \\ & m32 * Q_{lam32} + y173 / V_{lam33} * Q_{lam33} + y174 / V_{lam34} * Q_{lam34} + y175 / V_{lam35} * Q_{lam35} + y176 \\ & / V_{lam36} * Q_{lam36} + y177 / V_{lam37} * Q_{lam37} + y178 / V_{lam38} * Q_{lam38} + y179 / V_{lam39} * Q_{lam39} + \\ & y180 / V_{lam40} * Q_{lam40}) / f_b, \end{aligned}$$

; F_A of a substrate

$$y182 = 1 - y91 / \text{dose},$$

; F_{AFG} of a substrate

$y_{183} = y_{181}/\text{dose}$,

; F_G of a substrate

$y_{184} = y_{183}/y_{182}$,

; Intestinal clearance amount (not used in this study)

$y_{185}' = CL_1 * y_{101}/Vent_1 + CL_2 * y_{102}/Vent_2 + CL_3 * y_{103}/Vent_3 + CL_4 * y_{104}/Vent_4 + CL_5 * y_{105}/Vent_5 + CL_6 * y_{106}/Vent_6 + CL_7 * y_{107}/Vent_7 + CL_8 * y_{108}/Vent_8 + CL_9 * y_{109}/Vent_9 + CL_{10} * y_{110}/Vent_{10} + CL_{11} * y_{111}/Vent_{11} + CL_{12} * y_{112}/Vent_{12} + CL_{13} * y_{113}/Vent_{13} + CL_{14} * y_{114}/Vent_{14} + CL_{15} * y_{115}/Vent_{15} + CL_{16} * y_{116}/Vent_{16} + CL_{17} * y_{117}/Vent_{17} + CL_{18} * y_{118}/Vent_{18} + CL_{19} * y_{119}/Vent_{19} + CL_{20} * y_{120}/Vent_{20} + CL_{21} * y_{121}/Vent_{21} + CL_{22} * y_{122}/Vent_{22} + CL_{23} * y_{123}/Vent_{23} + CL_{24} * y_{124}/Vent_{24} + CL_{25} * y_{125}/Vent_{25} + CL_{26} * y_{126}/Vent_{26} + CL_{27} * y_{127}/Vent_{27} + CL_{28} * y_{128}/Vent_{28} + CL_{29} * y_{129}/Vent_{29} + CL_{30} * y_{130}/Vent_{30} + CL_{31} * y_{131}/Vent_{31} + CL_{32} * y_{132}/Vent_{32} + CL_{33} * y_{133}/Vent_{33} + CL_{34} * y_{134}/Vent_{34} + CL_{35} * y_{135}/Vent_{35} + CL_{36} * y_{136}/Vent_{36} + CL_{37} * y_{137}/Vent_{37} + CL_{38} * y_{138}/Vent_{38} + CL_{39} * y_{139}/Vent_{39} + CL_{40} * y_{140}/Vent_{40}$,

; Drug amount in the portal vein

$y_{186}' =$

$(y_{141}/V_{lam1} * Q_{lam1} + y_{142}/V_{lam2} * Q_{lam2} + y_{143}/V_{lam3} * Q_{lam3} + y_{144}/V_{lam4} * Q_{lam4} + y_{145}/V_{lam5} * Q_{lam5} + y_{146}/V_{lam6} * Q_{lam6} + y_{147}/V_{lam7} * Q_{lam7} + y_{148}/V_{lam8} * Q_{lam8} + y_{149}/V_{lam9} * Q_{lam9} + y_{150}/V_{lam10} * Q_{lam10} + y_{151}/V_{lam11} * Q_{lam11} + y_{152}/V_{lam12} * Q_{lam12} + y_{153}/V_{lam13} * Q_{lam13} + y_{154}/V_{lam14} * Q_{lam14} + y_{155}/V_{lam15} * Q_{lam15} + y_{156}/V_{lam16} * Q_{lam16} + y_{157}/V_{lam17} * Q_{lam17} + y_{158}/V_{lam18} * Q_{lam18} + y_{159}/V_{lam19} * Q_{lam19} + y_{160}/V_{lam20} * Q_{lam20} + y_{161}/V_{lam21} * Q_{lam21} + y_{162}/V_{lam22} * Q_{lam22} + y_{163}/V_{lam23} * Q_{lam23} + y_{164}/V_{lam24} * Q_{lam24} + y_{165}/V_{lam25} * Q_{lam25} + y_{166}/V_{lam26} * Q_{lam26} + y_{167}/V_{lam27} * Q_{lam27} + y_{168}/V_{lam28} * Q_{lam28}$

*Qlam28+y169/Vlam29*Qlam29+y170/Vlam30*Qlam30+y171/Vlam31*Qlam31+y172/Vlam32*Qlam32+y173/Vlam33*Qlam33+y174/Vlam34*Qlam34+y175/Vlam35*Qlam35+y176/Vlam36*Qlam36+y177/Vlam37*Qlam37+y178/Vlam38*Qlam38+y179/Vlam39*Qlam39+y180/Vlam40*Qlam40)/fb-Qpv*y186/Vpv,

; Drug concentration in the liver

y187'=(Qpv*y186/Vpv-Qh*y187/Kp_liver*Rb-fb*Rb/Kp_liver*CLint_h/(1+fb_inh*y330/Ki_3A4)*y187+Qha*y188)/Vliver,

; Drug concentration in the blood

y188'=(Qh*y187/Kp_liver*Rb-Qha*y188-k12*y188*Vb+k21*y189)/Vb,

; Drug amount in the peripheral compartment 1

; The number of compartments can be increased as necessary

y189'=k12*y188*Vb-k21*y189,

; Drug concentration in the plasma (unit: umol/L)

y190=y188/MW/Rb*1000,

; Following is the codes about an inhibitor

; Membrane permeability of an inhibitor

Ppass_lum_a1_inh = P_invivo_inh (1+10^(pH_Caco2-pKa_acid_inh)+10^(pKa_base_inh-pH_Caco2))/(1+10^(pH_lum1-pKa_acid_inh)+10^(pKa_base_inh-pH_lum1)),

PSpass_lum_a1_inh= Ppass_lum_a1_inh ME Sent1,

$$PSpass_a1_inh = P_invivo_inh \text{ ME Sent1},$$

$$PSpass_b1_inh = P_invivo_inh \text{ Sent1},$$

$$PSap1_inh = PSpass_lum_a1_inh,$$

$$PSbp1_inh = PSpass_b1_inh,$$

$$PSbx1_inh = PSpass_b1_inh,$$

$$PSpgp1_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp1 / (Km_Pgp_inh + fent_inh * y231 / Vent1),$$

$$PSax1_inh = (PSpass_a1_inh + PSpgp1_inh),$$

$$CL1_inh = Vmax_3A4_inh * Arel_3A4_1 / (Km_3A4_inh + fent_inh * y231 / Vent1),$$

$$Ppass_lum_a2_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_lum2)}),$$

$$PSpass_lum_a2_inh = Ppass_lum_a2_inh \text{ ME Sent2},$$

$$PSpass_a2_inh = P_invivo_inh \text{ ME Sent2},$$

$$PSpass_b2_inh = P_invivo_inh \text{ Sent2},$$

$$PSap2_inh = PSpass_lum_a2_inh,$$

$$PSbp2_inh = PSpass_b2_inh,$$

$$PSbx2_inh = PSpass_b2_inh,$$

$$PSpgp2_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp2 / (Km_Pgp_inh + fent_inh * y232 / Vent2),$$

$$PSax2_inh = (PSpass_a2_inh + PSpgp2_inh),$$

$$CL2_inh = Vmax_3A4_inh * Arel_3A4_2 / (Km_3A4_inh + fent_inh * y232 / Vent2),$$

$$Ppass_lum_a3_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum3 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_lum3)}),$$

$$PS_{pass_lum_a3_inh} = P_{pass_lum_a3_inh} ME_{Sent3},$$

$$PS_{pass_a3_inh} = P_{invivo_inh} ME_{Sent3},$$

$$PS_{pass_b3_inh} = P_{invivo_inh} Sent3,$$

$$PS_{ap3_inh} = PS_{pass_lum_a3_inh},$$

$$PS_{bp3_inh} = PS_{pass_b3_inh},$$

$$PS_{bx3_inh} = PS_{pass_b3_inh},$$

$$PS_{pgp3_inh} = psf_{Pgp} * V_{max_Pgp_inh} * A_{rel_Pgp3} / (K_{m_Pgp_inh} + f_{ent_inh} * y_{233} / V_{ent3}),$$

$$PS_{ax3_inh} = (PS_{pass_a3_inh} + PS_{pgp3_inh}),$$

$$CL_{3_inh} = V_{max_3A4_inh} * A_{rel_3A4_3} / (K_{m_3A4_inh} + f_{ent_inh} * y_{233} / V_{ent3}),$$

$$P_{pass_lum_a4_inh} = P_{invivo_inh} (1 + 10^{(pH_{Caco2} - pK_{a_acid_inh})} + 10^{(pK_{a_base_inh} - pH_{Caco2})}) / (1 + 10^{(pH_{lum4} - pK_{a_acid_inh})}$$

$$+ 10^{(pK_{a_base_inh} - pH_{lum4})}),$$

$$PS_{pass_lum_a4_inh} = P_{pass_lum_a4_inh} ME_{Sent4},$$

$$PS_{pass_a4_inh} = P_{invivo_inh} ME_{Sent4},$$

$$PS_{pass_b4_inh} = P_{invivo_inh} Sent4,$$

$$PS_{ap4_inh} = PS_{pass_lum_a4_inh},$$

$$PS_{bp4_inh} = PS_{pass_b4_inh},$$

$$PS_{bx4_inh} = PS_{pass_b4_inh},$$

$$PS_{pgp4_inh} = psf_{Pgp} * V_{max_Pgp_inh} * A_{rel_Pgp4} / (K_{m_Pgp_inh} + f_{ent_inh} * y_{234} / V_{ent4}),$$

$$PS_{ax4_inh} = (PS_{pass_a4_inh} + PS_{pgp4_inh}),$$

$$CL_{4_inh} = V_{max_3A4_inh} * A_{rel_3A4_4} / (K_{m_3A4_inh} + f_{ent_inh} * y_{234} / V_{ent4}),$$

$$P_{pass_lum_a5_inh} = P_{invivo_inh} (1 + 10^{(pH_{Caco2} - pK_{a_acid_inh})} + 10^{(pK_{a_base_inh} - pH_{Caco2})}) / (1 + 10^{(pH_{lum5} - pK_{a_acid_inh})}$$

$+10^{(pKa_base_inh-pH_lum5)}$),
 $PSpass_lum_a5_inh = Ppass_lum_a5_inh ME Sent5$,
 $PSpass_a5_inh = P_invivo_inh ME Sent5$,
 $PSpass_b5_inh = P_invivo_inh Sent5$,
 $PSap5_inh = PSpass_lum_a5_inh$,
 $PSbp5_inh = PSpass_b5_inh$,
 $PSbx5_inh = PSpass_b5_inh$,
 $PSpgp5_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp5 / (Km_Pgp_inh + fent_inh * y235 / Vent5)$,
 $PSax5_inh = (PSpass_a5_inh + PSpgp5_inh)$,
 $CL5_inh = Vmax_3A4_inh * Arel_3A4_5 / (Km_3A4_inh + fent_inh * y235 / Vent5)$,

$Ppass_lum_a6_inh = P_invivo_inh (1 + 10^{(pH_Caco2-pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum6-pKa_acid_inh)} + 10^{(pKa_base_inh - pH_lum6)})$),
 $PSpass_lum_a6_inh = Ppass_lum_a6_inh ME Sent6$,
 $PSpass_a6_inh = P_invivo_inh ME Sent6$,
 $PSpass_b6_inh = P_invivo_inh Sent6$,
 $PSap6_inh = PSpass_lum_a6_inh$,
 $PSbp6_inh = PSpass_b6_inh$,
 $PSbx6_inh = PSpass_b6_inh$,
 $PSpgp6_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp6 / (Km_Pgp_inh + fent_inh * y236 / Vent6)$,
 $PSax6_inh = (PSpass_a6_inh + PSpgp6_inh)$,
 $CL6_inh = Vmax_3A4_inh * Arel_3A4_6 / (Km_3A4_inh + fent_inh * y236 / Vent6)$,

$$P_{\text{pass_lum_a7_inh}} = P_{\text{invivo_inh}} (1+10^{(\text{pH_Caco2}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_Caco2})})/(1+10^{(\text{pH_lum7}-\text{pKa_acid_inh})}$$

$$+10^{(\text{pKa_base_inh}-\text{pH_lum7})}),$$

$$P_{\text{Spass_lum_a7_inh}} = P_{\text{pass_lum_a7_inh}} \text{ ME Sent7},$$

$$P_{\text{Spass_a7_inh}} = P_{\text{invivo_inh}} \text{ ME Sent7},$$

$$P_{\text{Spass_b7_inh}} = P_{\text{invivo_inh}} \text{ Sent7},$$

$$P_{\text{Sap7_inh}} = P_{\text{Spass_lum_a7_inh}},$$

$$P_{\text{Sbp7_inh}} = P_{\text{Spass_b7_inh}},$$

$$P_{\text{Sbx7_inh}} = P_{\text{Spass_b7_inh}},$$

$$P_{\text{Spgp7_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp7}} / (K_{\text{m_Pgp_inh}} + \text{fent_inh} * y_{237} / V_{\text{ent7}}),$$

$$P_{\text{Sax7_inh}} = (P_{\text{Spass_a7_inh}} + P_{\text{Spgp7_inh}}),$$

$$CL_{7_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_7}} / (K_{\text{m_3A4_inh}} + \text{fent_inh} * y_{237} / V_{\text{ent7}}),$$

$$P_{\text{pass_lum_a8_inh}} = P_{\text{invivo_inh}} (1+10^{(\text{pH_Caco2}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_Caco2})})/(1+10^{(\text{pH_lum8}-\text{pKa_acid_inh})}$$

$$+10^{(\text{pKa_base_inh}-\text{pH_lum8})}),$$

$$P_{\text{Spass_lum_a8_inh}} = P_{\text{pass_lum_a8_inh}} \text{ ME Sent8},$$

$$P_{\text{Spass_a8_inh}} = P_{\text{invivo_inh}} \text{ ME Sent8},$$

$$P_{\text{Spass_b8_inh}} = P_{\text{invivo_inh}} \text{ Sent8},$$

$$P_{\text{Sap8_inh}} = P_{\text{Spass_lum_a8_inh}},$$

$$P_{\text{Sbp8_inh}} = P_{\text{Spass_b8_inh}},$$

$$P_{\text{Sbx8_inh}} = P_{\text{Spass_b8_inh}},$$

$$P_{\text{Spgp8_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp8}} / (K_{\text{m_Pgp_inh}} + \text{fent_inh} * y_{238} / V_{\text{ent8}}),$$

$$P_{\text{Sax8_inh}} = (P_{\text{Spass_a8_inh}} + P_{\text{Spgp8_inh}}),$$

$$CL_{8_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_8}} / (K_{\text{m_3A4_inh}} + \text{fent_inh} * y_{238} / V_{\text{ent8}}),$$

$$P_{\text{pass_lum_a9_inh}} = P_{\text{invivo_inh}} \left(\frac{1 + 10^{(\text{pH_Caco2} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_Caco2})}}{1 + 10^{(\text{pH_lum9} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_lum9})}} \right),$$

$$P_{\text{Spass_lum_a9_inh}} = P_{\text{pass_lum_a9_inh}} \text{ ME Sent9},$$

$$P_{\text{Spass_a9_inh}} = P_{\text{invivo_inh}} \text{ ME Sent9},$$

$$P_{\text{Spass_b9_inh}} = P_{\text{invivo_inh}} \text{ Sent9},$$

$$P_{\text{Sap9_inh}} = P_{\text{Spass_lum_a9_inh}},$$

$$P_{\text{Sbp9_inh}} = P_{\text{Spass_b9_inh}},$$

$$P_{\text{Sbx9_inh}} = P_{\text{Spass_b9_inh}},$$

$$P_{\text{Spgp9_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp9}} / (K_{\text{m_Pgp_inh}} + \text{fent_inh} * y_{239} / V_{\text{ent9}}),$$

$$P_{\text{Sax9_inh}} = (P_{\text{Spass_a9_inh}} + P_{\text{Spgp9_inh}}),$$

$$CL_{9_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_9}} / (K_{\text{m_3A4_inh}} + \text{fent_inh} * y_{239} / V_{\text{ent9}}),$$

$$P_{\text{pass_lum_a10_inh}} = P_{\text{invivo_inh}} \left(\frac{1 + 10^{(\text{pH_Caco2} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_Caco2})}}{1 + 10^{(\text{pH_lum10} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_lum10})}} \right),$$

$$P_{\text{Spass_lum_a10_inh}} = P_{\text{pass_lum_a10_inh}} \text{ ME Sent10},$$

$$P_{\text{Spass_a10_inh}} = P_{\text{invivo_inh}} \text{ ME Sent10},$$

$$P_{\text{Spass_b10_inh}} = P_{\text{invivo_inh}} \text{ Sent10},$$

$$P_{\text{Sap10_inh}} = P_{\text{Spass_lum_a10_inh}},$$

$$P_{\text{Sbp10_inh}} = P_{\text{Spass_b10_inh}},$$

$$P_{\text{Sbx10_inh}} = P_{\text{Spass_b10_inh}},$$

$$P_{\text{Spgp10_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp10}} / (K_{\text{m_Pgp_inh}} + \text{fent_inh} * y_{240} / V_{\text{ent10}}),$$

$$PSax10_inh = (PSpass_a10_inh + PSpgp10_inh),$$

$$CL10_inh = Vmax_3A4_inh * Arel_3A4_10 / (Km_3A4_inh + fent_inh * y240 / Vent10),$$

$$Ppass_lum_a11_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum11 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum11)}),$$

$$PSpass_lum_a11_inh = Ppass_lum_a11_inh ME Sent11,$$

$$PSpass_a11_inh = P_invivo_inh ME Sent11,$$

$$PSpass_b11_inh = P_invivo_inh Sent11,$$

$$PSap11_inh = PSpass_lum_a11_inh,$$

$$PSbp11_inh = PSpass_b11_inh,$$

$$PSbx11_inh = PSpass_b11_inh,$$

$$PSpgp11_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp11$$

$$/ (Km_Pgp_inh + fent_inh * y241 / Vent11),$$

$$PSax11_inh = (PSpass_a11_inh + PSpgp11_inh),$$

$$CL11_inh = Vmax_3A4_inh * Arel_3A4_11 / (Km_3A4_inh + fent_inh * y241 / Vent11),$$

$$Ppass_lum_a12_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum12 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum12)}),$$

$$PSpass_lum_a12_inh = Ppass_lum_a12_inh ME Sent12,$$

$$PSpass_a12_inh = P_invivo_inh ME Sent12,$$

$$PSpass_b12_inh = P_invivo_inh Sent12,$$

$$PSap12_inh = PSpass_lum_a12_inh,$$

$$PSbp12_inh = PSpass_b12_inh,$$

PSbx12_inh = PSpass_b12_inh,

PSpgp12_inh = psf_Pgp*Vmax_Pgp_inh*Arel_Pgp12

/(Km_Pgp_inh+fent_inh*y242/Vent12),

PSax12_inh = (PSpass_a12_inh+ PSpgp12_inh),

CL12_inh = Vmax_3A4_inh*Arel_3A4_12/(Km_3A4_inh+fent_inh*y242/Vent12),

Ppass_lum_a13_inh = P_invivo_inh (1+10^(pH_Caco2-pKa_acid_inh)+10^(pKa_base_inh-
pH_Caco2))/(1+10^(pH_lum13-pKa_acid_inh)

+10^(pKa_base_inh-pH_lum13)),

PSpass_lum_a13_inh= Ppass_lum_a13_inh ME Sent13,

PSpass_a13_inh = P_invivo_inh ME Sent13,

PSpass_b13_inh = P_invivo_inh Sent13,

PSap13_inh = PSpass_lum_a13_inh,

PSbp13_inh = PSpass_b13_inh,

PSbx13_inh = PSpass_b13_inh,

PSpgp13_inh = psf_Pgp*Vmax_Pgp_inh*Arel_Pgp13

/(Km_Pgp_inh+fent_inh*y243/Vent13),

PSax13_inh = (PSpass_a13_inh+ PSpgp13_inh),

CL13_inh = Vmax_3A4_inh*Arel_3A4_13/(Km_3A4_inh+fent_inh*y243/Vent13),

Ppass_lum_a14_inh = P_invivo_inh (1+10^(pH_Caco2-pKa_acid_inh)+10^(pKa_base_inh-
pH_Caco2))/(1+10^(pH_lum14-pKa_acid_inh)

+10^(pKa_base_inh-pH_lum14)),

PSpass_lum_a14_inh= Ppass_lum_a14_inh ME Sent14,

PSpass_a14_inh = P_invivo_inh ME Sent14,

$$P_{\text{Spass_b14_inh}} = P_{\text{invivo_inh}} \text{ Sent14},$$

$$P_{\text{Sap14_inh}} = P_{\text{Spass_lum_a14_inh}},$$

$$P_{\text{Sbp14_inh}} = P_{\text{Spass_b14_inh}},$$

$$P_{\text{Sbx14_inh}} = P_{\text{Spass_b14_inh}},$$

$$P_{\text{Spgp14_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp14}}$$

$$/ (K_{\text{m_Pgp_inh}} + f_{\text{ent_inh}} * y_{244} / V_{\text{ent14}}),$$

$$P_{\text{Sax14_inh}} = (P_{\text{Spass_a14_inh}} + P_{\text{Spgp14_inh}}),$$

$$CL_{14_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_14}} / (K_{\text{m_3A4_inh}} + f_{\text{ent_inh}} * y_{244} / V_{\text{ent14}}),$$

$$P_{\text{pass_lum_a15_inh}} = P_{\text{invivo_inh}} \frac{(1 + 10^{(\text{pH_Caco2} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_Caco2})})}{(1 + 10^{(\text{pH_lum15} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_lum15})}),$$

$$P_{\text{Spass_lum_a15_inh}} = P_{\text{pass_lum_a15_inh}} \text{ ME Sent15},$$

$$P_{\text{Spass_a15_inh}} = P_{\text{invivo_inh}} \text{ ME Sent15},$$

$$P_{\text{Spass_b15_inh}} = P_{\text{invivo_inh}} \text{ Sent15},$$

$$P_{\text{Sap15_inh}} = P_{\text{Spass_lum_a15_inh}},$$

$$P_{\text{Sbp15_inh}} = P_{\text{Spass_b15_inh}},$$

$$P_{\text{Sbx15_inh}} = P_{\text{Spass_b15_inh}},$$

$$P_{\text{Spgp15_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp15}}$$

$$/ (K_{\text{m_Pgp_inh}} + f_{\text{ent_inh}} * y_{245} / V_{\text{ent15}}),$$

$$P_{\text{Sax15_inh}} = (P_{\text{Spass_a15_inh}} + P_{\text{Spgp15_inh}}),$$

$$CL_{15_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_15}} / (K_{\text{m_3A4_inh}} + f_{\text{ent_inh}} * y_{245} / V_{\text{ent15}}),$$

$$P_{\text{pass_lum_a16_inh}} = P_{\text{invivo_inh}} \frac{(1 + 10^{(\text{pH_Caco2} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_Caco2})})}{(1 + 10^{(\text{pH_lum16} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_lum16})})}$$

$+10^{(pKa_base_inh-pH_lum16)},$
 $PSpass_lum_a16_inh = Ppass_lum_a16_inh ME Sent16,$
 $PSpass_a16_inh = P_invivo_inh ME Sent16,$
 $PSpass_b16_inh = P_invivo_inh Sent16,$
 $PSap16_inh = PSpass_lum_a16_inh,$
 $PSbp16_inh = PSpass_b16_inh,$
 $PSbx16_inh = PSpass_b16_inh,$
 $PSpgp16_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp16$
 $/(Km_Pgp_inh + fent_inh * y246 / Vent16),$
 $PSax16_inh = (PSpass_a16_inh + PSpgp16_inh),$
 $CL16_inh = Vmax_3A4_inh * Arel_3A4_16 / (Km_3A4_inh + fent_inh * y246 / Vent16),$

$Ppass_lum_a17_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum17 - pKa_acid_inh)}$
 $+ 10^{(pKa_base_inh - pH_lum17)}),$
 $PSpass_lum_a17_inh = Ppass_lum_a17_inh ME Sent17,$
 $PSpass_a17_inh = P_invivo_inh ME Sent17,$
 $PSpass_b17_inh = P_invivo_inh Sent17,$
 $PSap17_inh = PSpass_lum_a17_inh,$
 $PSbp17_inh = PSpass_b17_inh,$
 $PSbx17_inh = PSpass_b17_inh,$
 $PSpgp17_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp17$
 $/(Km_Pgp_inh + fent_inh * y247 / Vent17),$
 $PSax17_inh = (PSpass_a17_inh + PSpgp17_inh),$
 $CL17_inh = Vmax_3A4_inh * Arel_3A4_17 / (Km_3A4_inh + fent_inh * y247 / Vent17),$

$$P_{\text{pass_lum_a18_inh}} = P_{\text{invivo_inh}} \left(\frac{1 + 10^{(\text{pH_Caco2} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_Caco2})}}{1 + 10^{(\text{pH_lum18} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_lum18})}} \right),$$

$$P_{\text{Spass_lum_a18_inh}} = P_{\text{pass_lum_a18_inh}} \text{ ME Sent18},$$

$$P_{\text{Spass_a18_inh}} = P_{\text{invivo_inh}} \text{ ME Sent18},$$

$$P_{\text{Spass_b18_inh}} = P_{\text{invivo_inh}} \text{ Sent18},$$

$$P_{\text{Sap18_inh}} = P_{\text{Spass_lum_a18_inh}},$$

$$P_{\text{Sbp18_inh}} = P_{\text{Spass_b18_inh}},$$

$$P_{\text{Sbx18_inh}} = P_{\text{Spass_b18_inh}},$$

$$P_{\text{Spgp18_inh}} = \frac{\text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp18}}}{(K_{\text{m_Pgp_inh}} + \text{fent_inh} * y_{248} / V_{\text{ent18}})},$$

$$P_{\text{Sax18_inh}} = (P_{\text{Spass_a18_inh}} + P_{\text{Spgp18_inh}}),$$

$$CL_{18_inh} = \frac{V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_18}}}{(K_{\text{m_3A4_inh}} + \text{fent_inh} * y_{248} / V_{\text{ent18}})},$$

$$P_{\text{pass_lum_a19_inh}} = P_{\text{invivo_inh}} \left(\frac{1 + 10^{(\text{pH_Caco2} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_Caco2})}}{1 + 10^{(\text{pH_lum19} - \text{pKa_acid_inh})} + 10^{(\text{pKa_base_inh} - \text{pH_lum19})}} \right),$$

$$P_{\text{Spass_lum_a19_inh}} = P_{\text{pass_lum_a19_inh}} \text{ ME Sent19},$$

$$P_{\text{Spass_a19_inh}} = P_{\text{invivo_inh}} \text{ ME Sent19},$$

$$P_{\text{Spass_b19_inh}} = P_{\text{invivo_inh}} \text{ Sent19},$$

$$P_{\text{Sap19_inh}} = P_{\text{Spass_lum_a19_inh}},$$

$$P_{\text{Sbp19_inh}} = P_{\text{Spass_b19_inh}},$$

$$P_{\text{Sbx19_inh}} = P_{\text{Spass_b19_inh}},$$

$$PSpgp19_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp19$$

$$/(Km_Pgp_inh + fent_inh * y249 / Vent19),$$

$$PSax19_inh = (PSpass_a19_inh + PSpgp19_inh),$$

$$CL19_inh = Vmax_3A4_inh * Arel_3A4_19 / (Km_3A4_inh + fent_inh * y249 / Vent19),$$

$$Ppass_lum_a20_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh -$$

$$pH_Caco2)) / (1 + 10^{(pH_lum20 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum20)}),$$

$$PSpass_lum_a20_inh = Ppass_lum_a20_inh ME Sent20,$$

$$PSpass_a20_inh = P_invivo_inh ME Sent20,$$

$$PSpass_b20_inh = P_invivo_inh Sent20,$$

$$PSap20_inh = PSpass_lum_a20_inh,$$

$$PSbp20_inh = PSpass_b20_inh,$$

$$PSbx20_inh = PSpass_b20_inh,$$

$$PSpgp20_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp20$$

$$/(Km_Pgp_inh + fent_inh * y250 / Vent20),$$

$$PSax20_inh = (PSpass_a20_inh + PSpgp20_inh),$$

$$CL20_inh = Vmax_3A4_inh * Arel_3A4_20 / (Km_3A4_inh + fent_inh * y250 / Vent20),$$

$$Ppass_lum_a21_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh -$$

$$pH_Caco2)) / (1 + 10^{(pH_lum21 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum21)}),$$

$$PSpass_lum_a21_inh = Ppass_lum_a21_inh ME Sent21,$$

$$PSpass_a21_inh = P_invivo_inh ME Sent21,$$

$$PSpass_b21_inh = P_invivo_inh Sent21,$$

$$PSap21_inh = PSpass_lum_a21_inh,$$

$$PSbp21_inh = PSpass_b21_inh,$$

$$PSbx21_inh = PSpass_b21_inh,$$

$$PSpgp21_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp21$$

$$/(Km_Pgp_inh + fent_inh * y251 / Vent21),$$

$$PSax21_inh = (PSpass_a21_inh + PSpgp21_inh),$$

$$CL21_inh = Vmax_3A4_inh * Arel_3A4_21 / (Km_3A4_inh + fent_inh * y251 / Vent21),$$

$$Ppass_lum_a22_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum22 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum22)}),$$

$$PSpass_lum_a22_inh = Ppass_lum_a22_inh ME Sent22,$$

$$PSpass_a22_inh = P_invivo_inh ME Sent22,$$

$$PSpass_b22_inh = P_invivo_inh Sent22,$$

$$PSap22_inh = PSpass_lum_a22_inh,$$

$$PSbp22_inh = PSpass_b22_inh,$$

$$PSbx22_inh = PSpass_b22_inh,$$

$$PSpgp22_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp22$$

$$/(Km_Pgp_inh + fent_inh * y252 / Vent22),$$

$$PSax22_inh = (PSpass_a22_inh + PSpgp22_inh),$$

$$CL22_inh = Vmax_3A4_inh * Arel_3A4_22 / (Km_3A4_inh + fent_inh * y252 / Vent22),$$

$$Ppass_lum_a23_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum23 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum23)}),$$

PSpass_lum_a23_inh= Ppass_lum_a23_inh ME Sent23,

PSpass_a23_inh = P_invivo_inh ME Sent23,

PSpass_b23_inh = P_invivo_inh Sent23,

PSap23_inh = PSpass_lum_a23_inh,

PSbp23_inh = PSpass_b23_inh,

PSbx23_inh = PSpass_b23_inh,

PSpgp23_inh = psf_Pgp*Vmax_Pgp_inh*Arel_Pgp23

/(Km_Pgp_inh+fent_inh*y253/Vent23),

PSax23_inh = (PSpass_a23_inh+ PSpgp23_inh),

CL23_inh = Vmax_3A4_inh*Arel_3A4_23 /(Km_3A4_inh+fent_inh*y253/Vent23),

Ppass_lum_a24_inh = P_invivo_inh (1+10^(pH_Caco2-pKa_acid_inh)+10^(pKa_base_inh-
pH_Caco2))/(1+10^(pH_lum24-pKa_acid_inh)

+10^(pKa_base_inh-pH_lum24)),

PSpass_lum_a24_inh= Ppass_lum_a24_inh ME Sent24,

PSpass_a24_inh = P_invivo_inh ME Sent24,

PSpass_b24_inh = P_invivo_inh Sent24,

PSap24_inh = PSpass_lum_a24_inh,

PSbp24_inh = PSpass_b24_inh,

PSbx24_inh = PSpass_b24_inh,

PSpgp24_inh = psf_Pgp*Vmax_Pgp_inh*Arel_Pgp24

/(Km_Pgp_inh+fent_inh*y254/Vent24),

PSax24_inh = (PSpass_a24_inh+ PSpgp24_inh),

CL24_inh = Vmax_3A4_inh*Arel_3A4_24 /(Km_3A4_inh+fent_inh*y254/Vent24),

$$P_{\text{pass_lum_a25_inh}} = P_{\text{invivo_inh}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum25}-\text{pKa_acid_inh})}}$$

$$+10^{(\text{pKa_base_inh}-\text{pH_lum25})},$$

$$P_{\text{Spass_lum_a25_inh}} = P_{\text{pass_lum_a25_inh}} \text{ME Sent25},$$

$$P_{\text{Spass_a25_inh}} = P_{\text{invivo_inh}} \text{ME Sent25},$$

$$P_{\text{Spass_b25_inh}} = P_{\text{invivo_inh}} \text{Sent25},$$

$$P_{\text{Sap25_inh}} = P_{\text{Spass_lum_a25_inh}},$$

$$P_{\text{Sbp25_inh}} = P_{\text{Spass_b25_inh}},$$

$$P_{\text{Sbx25_inh}} = P_{\text{Spass_b25_inh}},$$

$$P_{\text{Spgp25_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp25}}$$

$$/(\text{Km_Pgp_inh} + \text{fent_inh} * y_{255} / V_{\text{ent25}}),$$

$$P_{\text{Sax25_inh}} = (P_{\text{Spass_a25_inh}} + P_{\text{Spgp25_inh}}),$$

$$CL_{25_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_25}} / (\text{Km_3A4_inh} + \text{fent_inh} * y_{255} / V_{\text{ent25}}),$$

$$P_{\text{pass_lum_a26_inh}} = P_{\text{invivo_inh}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum26}-\text{pKa_acid_inh})}}$$

$$+10^{(\text{pKa_base_inh}-\text{pH_lum26})},$$

$$P_{\text{Spass_lum_a26_inh}} = P_{\text{pass_lum_a26_inh}} \text{ME Sent26},$$

$$P_{\text{Spass_a26_inh}} = P_{\text{invivo_inh}} \text{ME Sent26},$$

$$P_{\text{Spass_b26_inh}} = P_{\text{invivo_inh}} \text{Sent26},$$

$$P_{\text{Sap26_inh}} = P_{\text{Spass_lum_a26_inh}},$$

$$P_{\text{Sbp26_inh}} = P_{\text{Spass_b26_inh}},$$

$$P_{\text{Sbx26_inh}} = P_{\text{Spass_b26_inh}},$$

$$P_{\text{Spgp26_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp26}}$$

$$/(\text{Km_Pgp_inh} + \text{fent_inh} * y_{256} / V_{\text{ent26}}),$$

$$PSax26_inh = (PSpass_a26_inh + PSpgp26_inh),$$

$$CL26_inh = Vmax_3A4_inh * Arel_3A4_26 / (Km_3A4_inh + fent_inh * y256 / Vent26),$$

$$Ppass_lum_a27_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum27 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum27)}),$$

$$PSpass_lum_a27_inh = Ppass_lum_a27_inh ME Sent27,$$

$$PSpass_a27_inh = P_invivo_inh ME Sent27,$$

$$PSpass_b27_inh = P_invivo_inh Sent27,$$

$$PSap27_inh = PSpass_lum_a27_inh,$$

$$PSbp27_inh = PSpass_b27_inh,$$

$$PSbx27_inh = PSpass_b27_inh,$$

$$PSpgp27_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp27$$

$$/ (Km_Pgp_inh + fent_inh * y257 / Vent27),$$

$$PSax27_inh = (PSpass_a27_inh + PSpgp27_inh),$$

$$CL27_inh = Vmax_3A4_inh * Arel_3A4_27 / (Km_3A4_inh + fent_inh * y257 / Vent27),$$

$$Ppass_lum_a28_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum28 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum28)}),$$

$$PSpass_lum_a28_inh = Ppass_lum_a28_inh ME Sent28,$$

$$PSpass_a28_inh = P_invivo_inh ME Sent28,$$

$$PSpass_b28_inh = P_invivo_inh Sent28,$$

$$PSap28_inh = PSpass_lum_a28_inh,$$

$$PSbp28_inh = PSpass_b28_inh,$$

$$PSbx28_inh = PSpass_b28_inh,$$

$$PSpgp28_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp28 / (Km_Pgp_inh + fent * y258 / Vent28),$$

$$PSax28_inh = (PSpass_a28_inh + PSpgp28_inh),$$

$$CL28_inh = Vmax_3A4_inh * Arel_3A4_28 / (Km_3A4_inh + fent_inh * y258 / Vent28),$$

$$Ppass_lum_a29_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum29 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_lum29)}),$$

$$PSpass_lum_a29_inh = Ppass_lum_a29_inh ME Sent29,$$

$$PSpass_a29_inh = P_invivo_inh ME Sent29,$$

$$PSpass_b29_inh = P_invivo_inh Sent29,$$

$$PSap29_inh = PSpass_lum_a29_inh,$$

$$PSbp29_inh = PSpass_b29_inh,$$

$$PSbx29_inh = PSpass_b29_inh,$$

$$PSpgp29_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp29 / (Km_Pgp_inh + fent * y259 / Vent29),$$

$$PSax29_inh = (PSpass_a29_inh + PSpgp29_inh),$$

$$CL29_inh = Vmax_3A4_inh * Arel_3A4_29 / (Km_3A4_inh + fent_inh * y259 / Vent29),$$

$$Ppass_lum_a30_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum30 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_lum30)}),$$

$$PSpass_lum_a30_inh = Ppass_lum_a30_inh ME Sent30,$$

$$PSpass_a30_inh = P_invivo_inh ME Sent30,$$

$$PSpass_b30_inh = P_invivo_inh Sent30,$$

$$PSap30_inh = PSpass_lum_a30_inh,$$

$$PSbp30_inh = PSpass_b30_inh,$$

$$PSbx30_inh = PSpass_b30_inh,$$

$$PSpgp30_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp30$$

$$/(Km_Pgp_inh + fent_inh * y260 / Vent30),$$

$$PSax30_inh = (PSpass_a30_inh + PSpgp30_inh),$$

$$CL30_inh = Vmax_3A4_inh * Arel_3A4_30 / (Km_3A4_inh + fent_inh * y260 / Vent30),$$

$$Ppass_lum_a31_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum31 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum31)}),$$

$$PSpass_lum_a31_inh = Ppass_lum_a31_inh ME Sent31,$$

$$PSpass_a31_inh = P_invivo_inh ME Sent31,$$

$$PSpass_b31_inh = P_invivo_inh Sent31,$$

$$PSap31_inh = PSpass_lum_a31_inh,$$

$$PSbp31_inh = PSpass_b31_inh,$$

$$PSbx31_inh = PSpass_b31_inh,$$

$$PSpgp31_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp31$$

$$/(Km_Pgp_inh + fent_inh * y261 / Vent31),$$

$$PSax31_inh = (PSpass_a31_inh + PSpgp31_inh),$$

$$CL31_inh = Vmax_3A4_inh * Arel_3A4_31 / (Km_3A4_inh + fent_inh * y261 / Vent31),$$

$$Ppass_lum_a32_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum32 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum32)}),$$

$$PSpass_lum_a32_inh = Ppass_lum_a32_inh ME Sent32,$$

$PS_{pass_a32_inh} = P_{invivo_inh} ME_{Sent32},$
 $PS_{pass_b32_inh} = P_{invivo_inh} Sent32,$
 $PS_{ap32_inh} = PS_{pass_lum_a32_inh},$
 $PS_{bp32_inh} = PS_{pass_b32_inh},$
 $PS_{bx32_inh} = PS_{pass_b32_inh},$
 $PS_{pgp32_inh} = \frac{psf_Pgp * V_{max_Pgp_inh} * A_{rel_Pgp32}}{(K_{m_Pgp_inh} + f_{ent_inh} * y_{262} / V_{ent32})},$
 $PS_{ax32_inh} = (PS_{pass_a32_inh} + PS_{pgp32_inh}),$
 $CL_{32_inh} = \frac{V_{max_3A4_inh} * A_{rel_3A4_32}}{(K_{m_3A4_inh} + f_{ent_inh} * y_{262} / V_{ent32})},$

$P_{pass_lum_a33_inh} = P_{invivo_inh} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid_inh})} + 10^{(pK_{a_base_inh} - pH_{Caco2})})}{(1 + 10^{(pH_{lum33} - pK_{a_acid_inh})} + 10^{(pK_{a_base_inh} - pH_{lum33})}),$
 $PS_{pass_lum_a33_inh} = P_{pass_lum_a33_inh} ME_{Sent33},$
 $PS_{pass_a33_inh} = P_{invivo_inh} ME_{Sent33},$
 $PS_{pass_b33_inh} = P_{invivo_inh} Sent33,$
 $PS_{ap33_inh} = PS_{pass_lum_a33_inh},$
 $PS_{bp33_inh} = PS_{pass_b33_inh},$
 $PS_{bx33_inh} = PS_{pass_b33_inh},$
 $PS_{pgp33_inh} = \frac{psf_Pgp * V_{max_Pgp_inh} * A_{rel_Pgp33}}{(K_{m_Pgp_inh} + f_{ent_inh} * y_{263} / V_{ent33})},$
 $PS_{ax33_inh} = (PS_{pass_a33_inh} + PS_{pgp33_inh}),$
 $CL_{33_inh} = \frac{V_{max_3A4_inh} * A_{rel_3A4_33}}{(K_{m_3A4_inh} + f_{ent_inh} * y_{263} / V_{ent33})},$

$$P_{\text{pass_lum_a34_inh}} = P_{\text{invivo_inh}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum34}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_lum34})})}$$

$$+10^{(\text{pKa_base_inh}-\text{pH_lum34})},$$

$$P_{\text{Spass_lum_a34_inh}} = P_{\text{pass_lum_a34_inh}} \text{ ME Sent34},$$

$$P_{\text{Spass_a34_inh}} = P_{\text{invivo_inh}} \text{ ME Sent34},$$

$$P_{\text{Spass_b34_inh}} = P_{\text{invivo_inh}} \text{ Sent34},$$

$$P_{\text{Sap34_inh}} = P_{\text{Spass_lum_a34_inh}},$$

$$P_{\text{Sbp34_inh}} = P_{\text{Spass_b34_inh}},$$

$$P_{\text{Sbx34_inh}} = P_{\text{Spass_b34_inh}},$$

$$P_{\text{Spgp34_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp34}}$$

$$/(\text{Km_Pgp_inh} + \text{fent_inh} * y_{264} / V_{\text{ent34}}),$$

$$P_{\text{Sax34_inh}} = (P_{\text{Spass_a34_inh}} + P_{\text{Spgp34_inh}}),$$

$$CL_{34_inh} = V_{\text{max_3A4_inh}} * A_{\text{rel_3A4_34}} / (\text{Km_3A4_inh} + \text{fent_inh} * y_{264} / V_{\text{ent34}}),$$

$$P_{\text{pass_lum_a35_inh}} = P_{\text{invivo_inh}} \frac{(1+10^{(\text{pH_Caco2}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_Caco2})})}{(1+10^{(\text{pH_lum35}-\text{pKa_acid_inh})}+10^{(\text{pKa_base_inh}-\text{pH_lum35})})}$$

$$+10^{(\text{pKa_base_inh}-\text{pH_lum35})},$$

$$P_{\text{Spass_lum_a35_inh}} = P_{\text{pass_lum_a35_inh}} \text{ ME Sent35},$$

$$P_{\text{Spass_a35_inh}} = P_{\text{invivo_inh}} \text{ ME Sent35},$$

$$P_{\text{Spass_b35_inh}} = P_{\text{invivo_inh}} \text{ Sent35},$$

$$P_{\text{Sap35_inh}} = P_{\text{Spass_lum_a35_inh}},$$

$$P_{\text{Sbp35_inh}} = P_{\text{Spass_b35_inh}},$$

$$P_{\text{Sbx35_inh}} = P_{\text{Spass_b35_inh}},$$

$$P_{\text{Spgp35_inh}} = \text{psf_Pgp} * V_{\text{max_Pgp_inh}} * A_{\text{rel_Pgp35}}$$

$$/(\text{Km_Pgp_inh} + \text{fent_inh} * y_{265} / V_{\text{ent35}}),$$

$$PSax35_inh = (PSpass_a35_inh + PSpgp35_inh),$$

$$CL35_inh = Vmax_3A4_inh * Arel_3A4_35 / (Km_3A4_inh + fent_inh * y265 / Vent35),$$

$$Ppass_lum_a36_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum36 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum36)}),$$

$$PSpass_lum_a36_inh = Ppass_lum_a36_inh ME Sent36,$$

$$PSpass_a36_inh = P_invivo_inh ME Sent36,$$

$$PSpass_b36_inh = P_invivo_inh Sent36,$$

$$PSap36_inh = PSpass_lum_a36_inh,$$

$$PSbp36_inh = PSpass_b36_inh,$$

$$PSbx36_inh = PSpass_b36_inh,$$

$$PSpgp36_inh = psf_Pgp * Vmax_Pgp_inh * Arel_Pgp36$$

$$/ (Km_Pgp_inh + fent_inh * y266 / Vent36),$$

$$PSax36_inh = (PSpass_a36_inh + PSpgp36_inh),$$

$$CL36_inh = Vmax_3A4_inh * Arel_3A4_36 / (Km_3A4_inh + fent_inh * y266 / Vent36),$$

$$Ppass_lum_a37_inh = P_invivo_inh (1 + 10^{(pH_Caco2 - pKa_acid_inh)} + 10^{(pKa_base_inh - pH_Caco2)}) / (1 + 10^{(pH_lum37 - pKa_acid_inh)}$$

$$+ 10^{(pKa_base_inh - pH_lum37)}),$$

$$PSpass_lum_a37_inh = Ppass_lum_a37_inh ME Sent37,$$

$$PSpass_a37_inh = P_invivo_inh ME Sent37,$$

$$PSpass_b37_inh = P_invivo_inh Sent37,$$

$$PSap37_inh = PSpass_lum_a37_inh,$$

$$PSbp37_inh = PSpass_b37_inh,$$

PSbx37_inh = PSpass_b37_inh,

PSpgp37_inh = psf_Pgp*Vmax_Pgp_inh*Arel_Pgp37

/(Km_Pgp_inh+fent_inh*y267/Vent37),

PSax37_inh = (PSpass_a37_inh+ PSpgp37_inh),

CL37_inh = Vmax_3A4_inh*Arel_3A4_37/(Km_3A4_inh+fent_inh*y267/Vent37),

Ppass_lum_a38_inh = P_invivo_inh (1+10^(pH_Caco2-pKa_acid_inh)+10^(pKa_base_inh-

pH_Caco2))/(1+10^(pH_lum38-pKa_acid_inh)

+10^(pKa_base_inh-pH_lum38)),

PSpass_lum_a38_inh= Ppass_lum_a38_inh ME Sent38,

PSpass_a38_inh = P_invivo_inh ME Sent38,

PSpass_b38_inh = P_invivo_inh Sent38,

PSap38_inh = PSpass_lum_a38_inh,

PSbp38_inh = PSpass_b38_inh,

PSbx38_inh = PSpass_b38_inh,

PSpgp38_inh = psf_Pgp*Vmax_Pgp_inh*Arel_Pgp38

/(Km_Pgp_inh+fent_inh*y268/Vent38),

PSax38_inh = (PSpass_a38_inh+ PSpgp38_inh),

CL38_inh = Vmax_3A4_inh*Arel_3A4_38/(Km_3A4_inh+fent_inh*y268/Vent38),

Ppass_lum_a39_inh = P_invivo_inh (1+10^(pH_Caco2-pKa_acid_inh)+10^(pKa_base_inh-

pH_Caco2))/(1+10^(pH_lum39-pKa_acid_inh)

+10^(pKa_base_inh-pH_lum39)),

PSpass_lum_a39_inh= Ppass_lum_a39_inh ME Sent39,

PSpass_a39_inh = P_invivo_inh ME Sent39,

$PS_{pass_b39_inh} = P_{invivo_inh} \text{ Sent39},$
 $PS_{ap39_inh} = PS_{pass_lum_a39_inh},$
 $PS_{bp39_inh} = PS_{pass_b39_inh},$
 $PS_{bx39_inh} = PS_{pass_b39_inh},$
 $PS_{pgp39_inh} = \frac{psf_Pgp * V_{max_Pgp_inh} * A_{rel_Pgp39}}{(K_{m_Pgp_inh} + f_{ent_inh} * y_{269} / V_{ent39})},$
 $PS_{ax39_inh} = (PS_{pass_a39_inh} + PS_{pgp39_inh}),$
 $CL_{39_inh} = \frac{V_{max_3A4_inh} * A_{rel_3A4_39}}{(K_{m_3A4_inh} + f_{ent_inh} * y_{269} / V_{ent39})},$

$P_{pass_lum_a40_inh} = P_{invivo_inh} \frac{(1 + 10^{(pH_{Caco2} - pK_{a_acid_inh})} + 10^{(pK_{a_base_inh} - pH_{Caco2})})}{(1 + 10^{(pH_{lum40} - pK_{a_acid_inh})} + 10^{(pK_{a_base_inh} - pH_{lum40})})},$
 $PS_{pass_lum_a40_inh} = P_{pass_lum_a40_inh} \text{ ME Sent40},$
 $PS_{pass_a40_inh} = P_{invivo_inh} \text{ ME Sent40},$
 $PS_{pass_b40_inh} = P_{invivo_inh} \text{ Sent40},$
 $PS_{ap40_inh} = PS_{pass_lum_a40_inh},$
 $PS_{bp40_inh} = PS_{pass_b40_inh},$
 $PS_{bx40_inh} = PS_{pass_b40_inh},$
 $PS_{pgp40_inh} = \frac{psf_Pgp * V_{max_Pgp_inh} * A_{rel_Pgp40}}{(K_{m_Pgp_inh} + f_{ent_inh} * y_{270} / V_{ent40})},$
 $PS_{ax40_inh} = (PS_{pass_a40_inh} + PS_{pgp40_inh}),$
 $CL_{40_inh} = \frac{V_{max_3A4_inh} * A_{rel_3A4_40}}{(K_{m_3A4_inh} + f_{ent_inh} * y_{270} / V_{ent40})},$

; Drug concentration in the lumen

$y_{191}' = (kg * y_{313}) * V_g \text{ div} / V + c_{3a_1} * y_{191} + c_{4a_2} * y_{192} + c_{5_3} * y_{193} -$
 $PSap1_inh * y_{191} / y_1 + PSax1_inh * fent_inh * y_{231} / Vent1 / (V / \text{div}),$
 if $y_{191} < 0$ then $y_{191} = 0$ endif,
 $y_{192}' = c_{2a_1} * y_{191} + c_{3_2} * y_{192} + c_{4_3} * y_{193} + c_{5_4} * y_{194} -$
 $PSap2_inh * y_{192} / y_2 + PSax2_inh * fent_inh * y_{232} / Vent2 / (V / \text{div}),$
 if $y_{192} < 0$ then $y_{192} = 0$ endif,
 $y_{193}' = c_{1_1} * y_{191} + c_{2_2} * y_{192} + c_{3_3} * y_{193} + c_{4_4} * y_{194} + c_{5_5} * y_{195} -$
 $PSap3_inh * y_{193} / y_3 + PSax3_inh * fent_inh * y_{233} / Vent3 / (V / \text{div}),$
 if $y_{193} < 0$ then $y_{193} = 0$ endif,
 $y_{194}' = c_{1_2} * y_{192} + c_{2_3} * y_{193} + c_{3_4} * y_{194} + c_{4_5} * y_{195} + c_{5_6} * y_{196} -$
 $PSap4_inh * y_{194} / y_4 + PSax4_inh * fent_inh * y_{234} / Vent4 / (V / \text{div}),$
 if $y_{194} < 0$ then $y_{194} = 0$ endif,
 $y_{195}' = c_{1_3} * y_{193} + c_{2_4} * y_{194} + c_{3_5} * y_{195} + c_{4_6} * y_{196} + c_{5_7} * y_{197} -$
 $PSap5_inh * y_{195} / y_5 + PSax5_inh * fent_inh * y_{235} / Vent5 / (V / \text{div}),$
 if $y_{195} < 0$ then $y_{195} = 0$ endif,
 $y_{196}' = c_{1_4} * y_{194} + c_{2_5} * y_{195} + c_{3_6} * y_{196} + c_{4_7} * y_{197} + c_{5_8} * y_{198} -$
 $PSap6_inh * y_{196} / y_6 + PSax6_inh * fent_inh * y_{236} / Vent6 / (V / \text{div}),$
 if $y_{196} < 0$ then $y_{196} = 0$ endif,
 $y_{197}' = c_{1_5} * y_{195} + c_{2_6} * y_{196} + c_{3_7} * y_{197} + c_{4_8} * y_{198} + c_{5_9} * y_{199} -$
 $PSap7_inh * y_{197} / y_7 + PSax7_inh * fent_inh * y_{237} / Vent7 / (V / \text{div}),$
 if $y_{197} < 0$ then $y_{197} = 0$ endif,
 $y_{198}' = c_{1_6} * y_{196} + c_{2_7} * y_{197} + c_{3_8} * y_{198} + c_{4_9} * y_{199} + c_{5_10} * y_{200} -$
 $PSap8_inh * y_{198} / y_8 + PSax8_inh * fent_inh * y_{238} / Vent8 / (V / \text{div}),$
 if $y_{198} < 0$ then $y_{198} = 0$ endif,

$y_{199}' = c_{1_7} * y_{197} + c_{2_8} * y_{198} + c_{3_9} * y_{199} + c_{4_10} * y_{200} + c_{5_11} * y_{201} -$
 $PSap9_inh * y_{199} / y_9 + PSax9_inh * fent_inh * y_{239} / Vent9 / (V/div),$
 if $y_{199} < 0$ then $y_{199} = 0$ endif,

$y_{200}' = c_{1_8} * y_{198} + c_{2_9} * y_{199} + c_{3_10} * y_{200} + c_{4_11} * y_{201} + c_{5_12} * y_{202} -$
 $PSap10_inh * y_{200} / y_{10} + PSax10_inh * fent_inh * y_{240} / Vent10 / (V/div),$
 if $y_{200} < 0$ then $y_{200} = 0$ endif,

$y_{201}' = c_{1_9} * y_{199} + c_{2_10} * y_{200} + c_{3_11} * y_{201} + c_{4_12} * y_{202} + c_{5_13} * y_{203} -$
 $PSap11_inh * y_{201} / y_{11} + PSax11_inh * fent_inh * y_{241} / Vent11 / (V/div),$
 if $y_{201} < 0$ then $y_{201} = 0$ endif,

$y_{202}' = c_{1_10} * y_{200} + c_{2_11} * y_{201} + c_{3_12} * y_{202} + c_{4_13} * y_{203} + c_{5_14} * y_{204} -$
 $PSap12_inh * y_{202} / y_{12} + PSax12_inh * fent_inh * y_{242} / Vent12 / (V/div),$
 if $y_{202} < 0$ then $y_{202} = 0$ endif,

$y_{203}' = c_{1_11} * y_{201} + c_{2_12} * y_{202} + c_{3_13} * y_{203} + c_{4_14} * y_{204} + c_{5_15} * y_{205} -$
 $PSap13_inh * y_{203} / y_{13} + PSax13_inh * fent_inh * y_{243} / Vent13 / (V/div),$
 if $y_{203} < 0$ then $y_{203} = 0$ endif,

$y_{204}' = c_{1_12} * y_{202} + c_{2_13} * y_{203} + c_{3_14} * y_{204} + c_{4_15} * y_{205} + c_{5_16} * y_{206} -$
 $PSap14_inh * y_{204} / y_{14} + PSax14_inh * fent_inh * y_{244} / Vent14 / (V/div),$
 if $y_{204} < 0$ then $y_{204} = 0$ endif,

$y_{205}' = c_{1_13} * y_{203} + c_{2_14} * y_{204} + c_{3_15} * y_{205} + c_{4_16} * y_{206} + c_{5_17} * y_{207} -$
 $PSap15_inh * y_{205} / y_{15} + PSax15_inh * fent_inh * y_{245} / Vent15 / (V/div),$
 if $y_{205} < 0$ then $y_{205} = 0$ endif,

$y_{206}' = c_{1_14} * y_{204} + c_{2_15} * y_{205} + c_{3_16} * y_{206} + c_{4_17} * y_{207} + c_{5_18} * y_{208} -$
 $PSap16_inh * y_{206} / y_{16} + PSax16_inh * fent_inh * y_{246} / Vent16 / (V/div),$
 if $y_{206} < 0$ then $y_{206} = 0$ endif,

$y_{207}' = c_{1_15} * y_{205} + c_{2_16} * y_{206} + c_{3_17} * y_{207} + c_{4_18} * y_{208} + c_{5_19} * y_{209} -$
 $PSap_{17_inh} * y_{207} / y_{17} + PSax_{17_inh} * fent_inh * y_{247} / Vent_{17} / (V / div),$
 if $y_{207} < 0$ then $y_{207} = 0$ endif,

$y_{208}' = c_{1_16} * y_{206} + c_{2_17} * y_{207} + c_{3_18} * y_{208} + c_{4_19} * y_{209} + c_{5_20} * y_{210} -$
 $PSap_{18_inh} * y_{208} / y_{18} + PSax_{18_inh} * fent_inh * y_{248} / Vent_{18} / (V / div),$
 if $y_{208} < 0$ then $y_{208} = 0$ endif,

$y_{209}' = c_{1_17} * y_{207} + c_{2_18} * y_{208} + c_{3_19} * y_{209} + c_{4_20} * y_{210} + c_{5_21} * y_{211} -$
 $PSap_{19_inh} * y_{209} / y_{19} + PSax_{19_inh} * fent_inh * y_{249} / Vent_{19} / (V / div),$
 if $y_{209} < 0$ then $y_{209} = 0$ endif,

$y_{210}' = c_{1_18} * y_{208} + c_{2_19} * y_{209} + c_{3_20} * y_{210} + c_{4_21} * y_{211} + c_{5_22} * y_{212} -$
 $PSap_{20_inh} * y_{210} / y_{20} + PSax_{20_inh} * fent_inh * y_{250} / Vent_{20} / (V / div),$
 if $y_{210} < 0$ then $y_{210} = 0$ endif,

$y_{211}' = c_{1_19} * y_{209} + c_{2_20} * y_{210} + c_{3_21} * y_{211} + c_{4_22} * y_{212} + c_{5_23} * y_{213} -$
 $PSap_{21_inh} * y_{211} / y_{21} + PSax_{21_inh} * fent_inh * y_{251} / Vent_{21} / (V / div),$
 if $y_{211} < 0$ then $y_{211} = 0$ endif,

$y_{212}' = c_{1_20} * y_{210} + c_{2_21} * y_{211} + c_{3_22} * y_{212} + c_{4_23} * y_{213} + c_{5_24} * y_{214} -$
 $PSap_{22_inh} * y_{212} / y_{22} + PSax_{22_inh} * fent_inh * y_{252} / Vent_{22} / (V / div),$
 if $y_{212} < 0$ then $y_{212} = 0$ endif,

$y_{213}' = c_{1_21} * y_{211} + c_{2_22} * y_{212} + c_{3_23} * y_{213} + c_{4_24} * y_{214} + c_{5_25} * y_{215} -$
 $PSap_{23_inh} * y_{213} / y_{23} + PSax_{23_inh} * fent_inh * y_{253} / Vent_{23} / (V / div),$
 if $y_{213} < 0$ then $y_{213} = 0$ endif,

$y_{214}' = c_{1_22} * y_{212} + c_{2_23} * y_{213} + c_{3_24} * y_{214} + c_{4_25} * y_{215} + c_{5_26} * y_{216} -$
 $PSap_{24_inh} * y_{214} / y_{24} + PSax_{24_inh} * fent_inh * y_{254} / Vent_{24} / (V / div),$
 if $y_{214} < 0$ then $y_{214} = 0$ endif,

$y_{215}' = c_{1_23} * y_{213} + c_{2_24} * y_{214} + c_{3_25} * y_{215} + c_{4_26} * y_{216} + c_{5_27} * y_{217} -$
 $PSap_{25_inh} * y_{215} / y_{25} + PSax_{25_inh} * fent_inh * y_{255} / Vent_{25} / (V / div),$
 if $y_{215} < 0$ then $y_{215} = 0$ endif,

$y_{216}' = c_{1_24} * y_{214} + c_{2_25} * y_{215} + c_{3_26} * y_{216} + c_{4_27} * y_{217} + c_{5_28} * y_{218} -$
 $PSap_{26_inh} * y_{216} / y_{26} + PSax_{26_inh} * fent_inh * y_{256} / Vent_{26} / (V / div),$
 if $y_{216} < 0$ then $y_{216} = 0$ endif,

$y_{217}' = c_{1_25} * y_{215} + c_{2_26} * y_{216} + c_{3_27} * y_{217} + c_{4_28} * y_{218} + c_{5_29} * y_{219} -$
 $PSap_{27_inh} * y_{217} / y_{27} + PSax_{27_inh} * fent_inh * y_{257} / Vent_{27} / (V / div),$
 if $y_{217} < 0$ then $y_{217} = 0$ endif,

$y_{218}' = c_{1_26} * y_{216} + c_{2_27} * y_{217} + c_{3_28} * y_{218} + c_{4_29} * y_{219} + c_{5_30} * y_{220} -$
 $PSap_{28_inh} * y_{218} / y_{28} + PSax_{28_inh} * fent_inh * y_{258} / Vent_{28} / (V / div),$
 if $y_{218} < 0$ then $y_{218} = 0$ endif,

$y_{219}' = c_{1_27} * y_{217} + c_{2_28} * y_{218} + c_{3_29} * y_{219} + c_{4_30} * y_{220} + c_{5_31} * y_{221} -$
 $PSap_{29_inh} * y_{219} / y_{29} + PSax_{29_inh} * fent_inh * y_{259} / Vent_{29} / (V / div),$
 if $y_{219} < 0$ then $y_{219} = 0$ endif,

$y_{220}' = c_{1_28} * y_{218} + c_{2_29} * y_{219} + c_{3_30} * y_{220} + c_{4_31} * y_{221} + c_{5_32} * y_{222} -$
 $PSap_{30_inh} * y_{220} / y_{30} + PSax_{30_inh} * fent_inh * y_{260} / Vent_{30} / (V / div),$
 if $y_{220} < 0$ then $y_{220} = 0$ endif,

$y_{221}' = c_{1_29} * y_{219} + c_{2_30} * y_{220} + c_{3_31} * y_{221} + c_{4_32} * y_{222} + c_{5_33} * y_{223} -$
 $PSap_{31_inh} * y_{221} / y_{31} + PSax_{31_inh} * fent_inh * y_{261} / Vent_{31} / (V / div),$
 if $y_{221} < 0$ then $y_{221} = 0$ endif,

$y_{222}' = c_{1_30} * y_{220} + c_{2_31} * y_{221} + c_{3_32} * y_{222} + c_{4_33} * y_{223} + c_{5_34} * y_{224} -$
 $PSap_{32_inh} * y_{222} / y_{32} + PSax_{32_inh} * fent_inh * y_{262} / Vent_{32} / (V / div),$
 if $y_{222} < 0$ then $y_{222} = 0$ endif,

$y_{223}' = c_{1_31} * y_{221} + c_{2_32} * y_{222} + c_{3_33} * y_{223} + c_{4_34} * y_{224} + c_{5_35} * y_{225} -$
 $PSap_{33_inh} * y_{223} / y_{33} + PSax_{33_inh} * fent_inh * y_{263} / Vent_{33} / (V / div),$
 if $y_{223} < 0$ then $y_{223} = 0$ endif,

$y_{224}' = c_{1_32} * y_{222} + c_{2_33} * y_{223} + c_{3_34} * y_{224} + c_{4_35} * y_{225} + c_{5_36} * y_{226} -$
 $PSap_{34_inh} * y_{224} / y_{34} + PSax_{34_inh} * fent_inh * y_{264} / Vent_{34} / (V / div),$
 if $y_{224} < 0$ then $y_{224} = 0$ endif,

$y_{225}' = c_{1_33} * y_{223} + c_{2_34} * y_{224} + c_{3_35} * y_{225} + c_{4_36} * y_{226} + c_{5_37} * y_{227} -$
 $PSap_{35_inh} * y_{225} / y_{35} + PSax_{35_inh} * fent_inh * y_{265} / Vent_{35} / (V / div),$
 if $y_{225} < 0$ then $y_{225} = 0$ endif,

$y_{226}' = c_{1_34} * y_{224} + c_{2_35} * y_{225} + c_{3_36} * y_{226} + c_{4_37} * y_{227} + c_{5_38} * y_{228} -$
 $PSap_{36_inh} * y_{226} / y_{36} + PSax_{36_inh} * fent_inh * y_{266} / Vent_{36} / (V / div),$
 if $y_{226} < 0$ then $y_{226} = 0$ endif,

$y_{227}' = c_{1_35} * y_{225} + c_{2_36} * y_{226} + c_{3_37} * y_{227} + c_{4_38} * y_{228} + c_{5_39} * y_{229} -$
 $PSap_{37_inh} * y_{227} / y_{37} + PSax_{37_inh} * fent_inh * y_{267} / Vent_{37} / (V / div),$
 if $y_{227} < 0$ then $y_{227} = 0$ endif,

$y_{228}' = c_{1_36} * y_{226} + c_{2_37} * y_{227} + c_{3_38} * y_{228} + c_{4_39} * y_{229} + c_{5_40} * y_{230} -$
 $PSap_{38_inh} * y_{228} / y_{38} + PSax_{38_inh} * fent_inh * y_{268} / Vent_{38} / (V / div),$
 if $y_{228} < 0$ then $y_{228} = 0$ endif,

$y_{229}' = c_{1_37} * y_{227} + c_{2_38} * y_{228} + c_{3_39} * y_{229} + c_{4a_40} * y_{230} -$
 $PSap_{39_inh} * y_{229} / y_{39} + PSax_{39_inh} * fent_inh * y_{269} / Vent_{39} / (V / div),$
 if $y_{229} < 0$ then $y_{229} = 0$ endif,

$y_{230}' = c_{1_38} * y_{228} + c_{2b_39} * y_{229} + c_{3b_40} * y_{230} -$
 $PSap_{40_inh} * y_{230} / y_{40} + PSax_{40_inh} * fent_inh * y_{270} / Vent_{40} / (V / div),$
 if $y_{230} < 0$ then $y_{230} = 0$ endif,

; Drug amount in the enterocytes

$y_{231}' = PS_{ap1_inh} * y_{191} * (V/div) / y_1 -$

$(PS_{ax1_inh} + CL_{1_inh} + PS_{bp1_inh}) * fent_inh * y_{231} / Vent_1 + PS_{bx1_inh} * y_{271} / V_{lam1},$

if $y_{231} < 0$ then $y_{231} = 0$ endif,

$y_{232}' = PS_{ap2_inh} * y_{192} * (V/div) / y_2 -$

$(PS_{ax2_inh} + CL_{2_inh} + PS_{bp2_inh}) * fent_inh * y_{232} / Vent_2 + PS_{bx2_inh} * y_{272} / V_{lam2},$

if $y_{232} < 0$ then $y_{232} = 0$ endif,

$y_{233}' = PS_{ap3_inh} * y_{193} * (V/div) / y_3 -$

$(PS_{ax3_inh} + CL_{3_inh} + PS_{bp3_inh}) * fent_inh * y_{233} / Vent_3 + PS_{bx3_inh} * y_{273} / V_{lam3},$

if $y_{233} < 0$ then $y_{233} = 0$ endif,

$y_{234}' = PS_{ap4_inh} * y_{194} * (V/div) / y_4 -$

$(PS_{ax4_inh} + CL_{4_inh} + PS_{bp4_inh}) * fent_inh * y_{234} / Vent_4 + PS_{bx4_inh} * y_{274} / V_{lam4},$

if $y_{234} < 0$ then $y_{234} = 0$ endif,

$y_{235}' = PS_{ap5_inh} * y_{195} * (V/div) / y_5 -$

$(PS_{ax5_inh} + CL_{5_inh} + PS_{bp5_inh}) * fent_inh * y_{235} / Vent_5 + PS_{bx5_inh} * y_{275} / V_{lam5},$

if $y_{235} < 0$ then $y_{235} = 0$ endif,

$y_{236}' = PS_{ap6_inh} * y_{196} * (V/div) / y_6 -$

$(PS_{ax6_inh} + CL_{6_inh} + PS_{bp6_inh}) * fent_inh * y_{236} / Vent_6 + PS_{bx6_inh} * y_{276} / V_{lam6},$

if $y_{236} < 0$ then $y_{236} = 0$ endif,

$y_{237}' = PS_{ap7_inh} * y_{197} * (V/div) / y_7 -$

$(PS_{ax7_inh} + CL_{7_inh} + PS_{bp7_inh}) * fent_inh * y_{237} / Vent_7 + PS_{bx7_inh} * y_{277} / V_{lam7},$

if $y_{237} < 0$ then $y_{237} = 0$ endif,

$y_{238}' = PS_{ap8_inh} * y_{198} * (V/div) / y_8 -$

$(PS_{ax8_inh} + CL_{8_inh} + PS_{bp8_inh}) * fent_inh * y_{238} / Vent_8 + PS_{bx8_inh} * y_{278} / V_{lam8},$

if $y_{238} < 0$ then $y_{238} = 0$ endif,

$y_{239} = PS_{ap9_inh} * y_{199} * (V/div) / y_9 -$
 $(PS_{ax9_inh} + CL_{9_inh} + PS_{bp9_inh}) * fent_inh * y_{239} / Vent_9 + PS_{bx9_inh} * y_{279} / Vlam_9,$
 if $y_{239} < 0$ then $y_{239} = 0$ endif,
 $y_{240} = PS_{ap10_inh} * y_{200} * (V/div) / y_{10} -$
 $(PS_{ax10_inh} + CL_{10_inh} + PS_{bp10_inh}) * fent_inh * y_{240} / Vent_{10} + PS_{bx10_inh} * y_{280} / Vlam_{10},$
 if $y_{240} < 0$ then $y_{240} = 0$ endif,
 $y_{241} = PS_{ap11_inh} * y_{201} * (V/div) / y_{11} -$
 $(PS_{ax11_inh} + CL_{11_inh} + PS_{bp11_inh}) * fent_inh * y_{241} / Vent_{11} + PS_{bx11_inh} * y_{281} / Vlam_{11},$
 if $y_{241} < 0$ then $y_{241} = 0$ endif,
 $y_{242} = PS_{ap12_inh} * y_{202} * (V/div) / y_{12} -$
 $(PS_{ax12_inh} + CL_{12_inh} + PS_{bp12_inh}) * fent_inh * y_{242} / Vent_{12} + PS_{bx12_inh} * y_{282} / Vlam_{12},$
 if $y_{242} < 0$ then $y_{242} = 0$ endif,
 $y_{243} = PS_{ap13_inh} * y_{203} * (V/div) / y_{13} -$
 $(PS_{ax13_inh} + CL_{13_inh} + PS_{bp13_inh}) * fent_inh * y_{243} / Vent_{13} + PS_{bx13_inh} * y_{283} / Vlam_{13},$
 if $y_{243} < 0$ then $y_{243} = 0$ endif,
 $y_{244} = PS_{ap14_inh} * y_{204} * (V/div) / y_{14} -$
 $(PS_{ax14_inh} + CL_{14_inh} + PS_{bp14_inh}) * fent_inh * y_{244} / Vent_{14} + PS_{bx14_inh} * y_{284} / Vlam_{14},$
 if $y_{244} < 0$ then $y_{244} = 0$ endif,
 $y_{245} = PS_{ap15_inh} * y_{205} * (V/div) / y_{15} -$
 $(PS_{ax15_inh} + CL_{15_inh} + PS_{bp15_inh}) * fent_inh * y_{245} / Vent_{15} + PS_{bx15_inh} * y_{285} / Vlam_{15},$
 if $y_{245} < 0$ then $y_{245} = 0$ endif,
 $y_{246} = PS_{ap16_inh} * y_{206} * (V/div) / y_{16} -$
 $(PS_{ax16_inh} + CL_{16_inh} + PS_{bp16_inh}) * fent_inh * y_{246} / Vent_{16} + PS_{bx16_inh} * y_{286} / Vlam_{16},$
 if $y_{246} < 0$ then $y_{246} = 0$ endif,

$y_{247} = PS_{ap17_inh} * y_{207} * (V/div) / y_{17} -$
 $(PS_{ax17_inh} + CL_{17_inh} + PS_{bp17_inh}) * f_{ent_inh} * y_{247} / Vent_{17} + PS_{bx17_inh} * y_{287} / V_{lam17},$
 if $y_{247} < 0$ then $y_{247} = 0$ endif,

$y_{248} = PS_{ap18_inh} * y_{208} * (V/div) / y_{18} -$
 $(PS_{ax18_inh} + CL_{18_inh} + PS_{bp18_inh}) * f_{ent_inh} * y_{248} / Vent_{18} + PS_{bx18_inh} * y_{288} / V_{lam18},$
 if $y_{248} < 0$ then $y_{248} = 0$ endif,

$y_{249} = PS_{ap19_inh} * y_{209} * (V/div) / y_{19} -$
 $(PS_{ax19_inh} + CL_{19_inh} + PS_{bp19_inh}) * f_{ent_inh} * y_{249} / Vent_{19} + PS_{bx19_inh} * y_{289} / V_{lam19},$
 if $y_{249} < 0$ then $y_{249} = 0$ endif,

$y_{250} = PS_{ap20_inh} * y_{210} * (V/div) / y_{20} -$
 $(PS_{ax20_inh} + CL_{20_inh} + PS_{bp20_inh}) * f_{ent_inh} * y_{250} / Vent_{20} + PS_{bx20_inh} * y_{290} / V_{lam20},$
 if $y_{250} < 0$ then $y_{250} = 0$ endif,

$y_{251} = PS_{ap21_inh} * y_{211} * (V/div) / y_{21} -$
 $(PS_{ax21_inh} + CL_{21_inh} + PS_{bp21_inh}) * f_{ent_inh} * y_{251} / Vent_{21} + PS_{bx21_inh} * y_{291} / V_{lam21},$
 if $y_{251} < 0$ then $y_{251} = 0$ endif,

$y_{252} = PS_{ap22_inh} * y_{212} * (V/div) / y_{22} -$
 $(PS_{ax22_inh} + CL_{22_inh} + PS_{bp22_inh}) * f_{ent_inh} * y_{252} / Vent_{22} + PS_{bx22_inh} * y_{292} / V_{lam22},$
 if $y_{252} < 0$ then $y_{252} = 0$ endif,

$y_{253} = PS_{ap23_inh} * y_{213} * (V/div) / y_{23} -$
 $(PS_{ax23_inh} + CL_{23_inh} + PS_{bp23_inh}) * f_{ent_inh} * y_{253} / Vent_{23} + PS_{bx23_inh} * y_{293} / V_{lam23},$
 if $y_{253} < 0$ then $y_{253} = 0$ endif,

$y_{254} = PS_{ap24_inh} * y_{214} * (V/div) / y_{24} -$
 $(PS_{ax24_inh} + CL_{24_inh} + PS_{bp24_inh}) * f_{ent_inh} * y_{254} / Vent_{24} + PS_{bx24_inh} * y_{294} / V_{lam24},$
 if $y_{254} < 0$ then $y_{254} = 0$ endif,

$y255 = PSap25_inh * y215 * (V/div) / y25 -$
 $(PSax25_inh + CL25_inh + PSbp25_inh) * fent_inh * y255 / Vent25 + PSbx25_inh * y295 / Vlam25,$
 if $y255 < 0$ then $y255 = 0$ endif,
 $y256 = PSap26_inh * y216 * (V/div) / y26 -$
 $(PSax26_inh + CL26_inh + PSbp26_inh) * fent_inh * y256 / Vent26 + PSbx26_inh * y296 / Vlam26,$
 if $y256 < 0$ then $y256 = 0$ endif,
 $y257 = PSap27_inh * y217 * (V/div) / y27 -$
 $(PSax27_inh + CL27_inh + PSbp27_inh) * fent_inh * y257 / Vent27 + PSbx27_inh * y297 / Vlam27,$
 if $y257 < 0$ then $y257 = 0$ endif,
 $y258 = PSap28_inh * y218 * (V/div) / y28 -$
 $(PSax28_inh + CL28_inh + PSbp28_inh) * fent_inh * y258 / Vent28 + PSbx28_inh * y298 / Vlam28,$
 if $y258 < 0$ then $y258 = 0$ endif,
 $y259 = PSap29_inh * y219 * (V/div) / y29 -$
 $(PSax29_inh + CL29_inh + PSbp29_inh) * fent_inh * y259 / Vent29 + PSbx29_inh * y299 / Vlam29,$
 if $y259 < 0$ then $y259 = 0$ endif,
 $y260 = PSap30_inh * y220 * (V/div) / y30 -$
 $(PSax30_inh + CL30_inh + PSbp30_inh) * fent_inh * y260 / Vent30 + PSbx30_inh * y300 / Vlam30,$
 if $y260 < 0$ then $y260 = 0$ endif,
 $y261 = PSap31_inh * y221 * (V/div) / y31 -$
 $(PSax31_inh + CL31_inh + PSbp31_inh) * fent_inh * y261 / Vent31 + PSbx31_inh * y301 / Vlam31,$
 if $y261 < 0$ then $y261 = 0$ endif,
 $y262 = PSap32_inh * y222 * (V/div) / y32 -$
 $(PSax32_inh + CL32_inh + PSbp32_inh) * fent_inh * y262 / Vent32 + PSbx32_inh * y302 / Vlam32,$
 if $y262 < 0$ then $y262 = 0$ endif,

$y_{263} = PS_{ap33_inh} * y_{223} * (V/div) / y_{33}$ -
 $(PS_{ax33_inh} + CL_{33_inh} + PS_{bp33_inh}) * f_{ent_inh} * y_{263} / Vent_{33} + PS_{bx33_inh} * y_{303} / V_{lam33}$,
 if $y_{263} < 0$ then $y_{263} = 0$ endif,
 $y_{264} = PS_{ap34_inh} * y_{224} * (V/div) / y_{34}$ -
 $(PS_{ax34_inh} + CL_{34_inh} + PS_{bp34_inh}) * f_{ent_inh} * y_{264} / Vent_{34} + PS_{bx34_inh} * y_{304} / V_{lam34}$,
 if $y_{264} < 0$ then $y_{264} = 0$ endif,
 $y_{265} = PS_{ap35_inh} * y_{225} * (V/div) / y_{35}$ -
 $(PS_{ax35_inh} + CL_{35_inh} + PS_{bp35_inh}) * f_{ent_inh} * y_{265} / Vent_{35} + PS_{bx35_inh} * y_{305} / V_{lam35}$,
 if $y_{265} < 0$ then $y_{265} = 0$ endif,
 $y_{266} = PS_{ap36_inh} * y_{226} * (V/div) / y_{36}$ -
 $(PS_{ax36_inh} + CL_{36_inh} + PS_{bp36_inh}) * f_{ent_inh} * y_{266} / Vent_{36} + PS_{bx36_inh} * y_{306} / V_{lam36}$,
 if $y_{266} < 0$ then $y_{266} = 0$ endif,
 $y_{267} = PS_{ap37_inh} * y_{227} * (V/div) / y_{37}$ -
 $(PS_{ax37_inh} + CL_{37_inh} + PS_{bp37_inh}) * f_{ent_inh} * y_{267} / Vent_{37} + PS_{bx37_inh} * y_{307} / V_{lam37}$,
 if $y_{267} < 0$ then $y_{267} = 0$ endif,
 $y_{268} = PS_{ap38_inh} * y_{228} * (V/div) / y_{38}$ -
 $(PS_{ax38_inh} + CL_{38_inh} + PS_{bp38_inh}) * f_{ent_inh} * y_{268} / Vent_{38} + PS_{bx38_inh} * y_{308} / V_{lam38}$,
 if $y_{268} < 0$ then $y_{268} = 0$ endif,
 $y_{269} = PS_{ap39_inh} * y_{229} * (V/div) / y_{39}$ -
 $(PS_{ax39_inh} + CL_{39_inh} + PS_{bp39_inh}) * f_{ent_inh} * y_{269} / Vent_{39} + PS_{bx39_inh} * y_{309} / V_{lam39}$,
 if $y_{269} < 0$ then $y_{269} = 0$ endif,
 $y_{270} = PS_{ap40_inh} * y_{230} * (V/div) / y_{40}$ -
 $(PS_{ax40_inh} + CL_{40_inh} + PS_{bp40_inh}) * f_{ent_inh} * y_{270} / Vent_{40} + PS_{bx40_inh} * y_{310} / V_{lam40}$,
 if $y_{270} < 0$ then $y_{270} = 0$ endif,

; Drug amount in the lamina propria

$$y271' = \text{PSbp1_inh} * \text{fent_inh} * y231 / \text{Vent1} - (\text{Qlam1} / \text{fb_inh} + \text{PSbx1_inh}) * y271 / \text{Vlam1},$$

if $y271 < 0$ then $y271=0$ endif,

$$y272' = \text{PSbp2_inh} * \text{fent_inh} * y232 / \text{Vent2} - (\text{Qlam2} / \text{fb_inh} + \text{PSbx2_inh}) * y272 / \text{Vlam2},$$

if $y272 < 0$ then $y272=0$ endif,

$$y273' = \text{PSbp3_inh} * \text{fent_inh} * y233 / \text{Vent3} - (\text{Qlam3} / \text{fb_inh} + \text{PSbx3_inh}) * y273 / \text{Vlam3},$$

if $y273 < 0$ then $y273=0$ endif,

$$y274' = \text{PSbp4_inh} * \text{fent_inh} * y234 / \text{Vent4} - (\text{Qlam4} / \text{fb_inh} + \text{PSbx4_inh}) * y274 / \text{Vlam4},$$

if $y274 < 0$ then $y274=0$ endif,

$$y275' = \text{PSbp5_inh} * \text{fent_inh} * y235 / \text{Vent5} - (\text{Qlam5} / \text{fb_inh} + \text{PSbx5_inh}) * y275 / \text{Vlam5},$$

if $y275 < 0$ then $y275=0$ endif,

$$y276' = \text{PSbp6_inh} * \text{fent_inh} * y236 / \text{Vent6} - (\text{Qlam6} / \text{fb_inh} + \text{PSbx6_inh}) * y276 / \text{Vlam6},$$

if $y276 < 0$ then $y276=0$ endif,

$$y277' = \text{PSbp7_inh} * \text{fent_inh} * y237 / \text{Vent7} - (\text{Qlam7} / \text{fb_inh} + \text{PSbx7_inh}) * y277 / \text{Vlam7},$$

if $y277 < 0$ then $y277=0$ endif,

$$y278' = \text{PSbp8_inh} * \text{fent_inh} * y238 / \text{Vent8} - (\text{Qlam8} / \text{fb_inh} + \text{PSbx8_inh}) * y278 / \text{Vlam8},$$

if $y278 < 0$ then $y278=0$ endif,

$$y279' = \text{PSbp9_inh} * \text{fent_inh} * y239 / \text{Vent9} - (\text{Qlam9} / \text{fb_inh} + \text{PSbx9_inh}) * y279 / \text{Vlam9},$$

if $y279 < 0$ then $y279=0$ endif,

$$y280' = \text{PSbp10_inh} * \text{fent_inh} * y240 / \text{Vent10} - (\text{Qlam10} / \text{fb_inh} + \text{PSbx10_inh}) * y280 / \text{Vlam10},$$

if $y280 < 0$ then $y280=0$ endif,

$$y281' = \text{PSbp11_inh} * \text{fent_inh} * y241 / \text{Vent11} - (\text{Qlam11} / \text{fb_inh} + \text{PSbx11_inh}) * y281 / \text{Vlam11},$$

if $y281 < 0$ then $y281=0$ endif,

$$y282' = \text{PSbp12_inh} * \text{fent_inh} * y242 / \text{Vent12} - (\text{Qlam12} / \text{fb_inh} + \text{PSbx12_inh}) * y282 / \text{Vlam12},$$

if $y282 < 0$ then $y282=0$ endif,

$y_{283}' = PS_{bp13_inh} * f_{ent_inh} * y_{243} / Vent_{13} - (Q_{lam13} / fb_{inh} + PS_{bx13_inh}) * y_{283} / V_{lam13}$,
 if $y_{283} < 0$ then $y_{283} = 0$ endif,
 $y_{284}' = PS_{bp14_inh} * f_{ent_inh} * y_{244} / Vent_{14} - (Q_{lam14} / fb_{inh} + PS_{bx14_inh}) * y_{284} / V_{lam14}$,
 if $y_{284} < 0$ then $y_{284} = 0$ endif,
 $y_{285}' = PS_{bp15_inh} * f_{ent_inh} * y_{245} / Vent_{15} - (Q_{lam15} / fb_{inh} + PS_{bx15_inh}) * y_{285} / V_{lam15}$,
 if $y_{285} < 0$ then $y_{285} = 0$ endif,
 $y_{286}' = PS_{bp16_inh} * f_{ent_inh} * y_{246} / Vent_{16} - (Q_{lam16} / fb_{inh} + PS_{bx16_inh}) * y_{286} / V_{lam16}$,
 if $y_{286} < 0$ then $y_{286} = 0$ endif,
 $y_{287}' = PS_{bp17_inh} * f_{ent_inh} * y_{247} / Vent_{17} - (Q_{lam17} / fb_{inh} + PS_{bx17_inh}) * y_{287} / V_{lam17}$,
 if $y_{287} < 0$ then $y_{287} = 0$ endif,
 $y_{288}' = PS_{bp18_inh} * f_{ent_inh} * y_{248} / Vent_{18} - (Q_{lam18} / fb_{inh} + PS_{bx18_inh}) * y_{288} / V_{lam18}$,
 if $y_{288} < 0$ then $y_{288} = 0$ endif,
 $y_{289}' = PS_{bp19_inh} * f_{ent_inh} * y_{249} / Vent_{19} - (Q_{lam19} / fb_{inh} + PS_{bx19_inh}) * y_{289} / V_{lam19}$,
 if $y_{289} < 0$ then $y_{289} = 0$ endif,
 $y_{290}' = PS_{bp20_inh} * f_{ent_inh} * y_{250} / Vent_{20} - (Q_{lam20} / fb_{inh} + PS_{bx20_inh}) * y_{290} / V_{lam20}$,
 if $y_{290} < 0$ then $y_{290} = 0$ endif,
 $y_{291}' = PS_{bp21_inh} * f_{ent_inh} * y_{251} / Vent_{21} - (Q_{lam21} / fb_{inh} + PS_{bx21_inh}) * y_{291} / V_{lam21}$,
 if $y_{291} < 0$ then $y_{291} = 0$ endif,
 $y_{292}' = PS_{bp22_inh} * f_{ent_inh} * y_{252} / Vent_{22} - (Q_{lam22} / fb_{inh} + PS_{bx22_inh}) * y_{292} / V_{lam22}$,
 if $y_{292} < 0$ then $y_{292} = 0$ endif,
 $y_{293}' = PS_{bp23_inh} * f_{ent_inh} * y_{253} / Vent_{23} - (Q_{lam23} / fb_{inh} + PS_{bx23_inh}) * y_{293} / V_{lam23}$,
 if $y_{293} < 0$ then $y_{293} = 0$ endif,
 $y_{294}' = PS_{bp24_inh} * f_{ent_inh} * y_{254} / Vent_{24} - (Q_{lam24} / fb_{inh} + PS_{bx24_inh}) * y_{294} / V_{lam24}$,
 if $y_{294} < 0$ then $y_{294} = 0$ endif,
 $y_{295}' = PS_{bp25_inh} * f_{ent_inh} * y_{255} / Vent_{25} - (Q_{lam25} / fb_{inh} + PS_{bx25_inh}) * y_{295} / V_{lam25}$,

if $y_{295} < 0$ then $y_{295}=0$ endif,
 $y_{296}' = PS_{bp26_inh} * f_{ent_inh} * y_{256} / Vent_{26} - (Q_{lam26} / fb_{inh} + PS_{bx26_inh}) * y_{296} / V_{lam26}$,
 if $y_{296} < 0$ then $y_{296}=0$ endif,
 $y_{297}' = PS_{bp27_inh} * f_{ent_inh} * y_{257} / Vent_{27} - (Q_{lam27} / fb_{inh} + PS_{bx27_inh}) * y_{297} / V_{lam27}$,
 if $y_{297} < 0$ then $y_{297}=0$ endif,
 $y_{298}' = PS_{bp28_inh} * f_{ent_inh} * y_{258} / Vent_{28} - (Q_{lam28} / fb_{inh} + PS_{bx28_inh}) * y_{298} / V_{lam28}$,
 if $y_{298} < 0$ then $y_{298}=0$ endif,
 $y_{299}' = PS_{bp29_inh} * f_{ent_inh} * y_{259} / Vent_{29} - (Q_{lam29} / fb_{inh} + PS_{bx29_inh}) * y_{299} / V_{lam29}$,
 if $y_{299} < 0$ then $y_{299}=0$ endif,
 $y_{300}' = PS_{bp30_inh} * f_{ent_inh} * y_{260} / Vent_{30} - (Q_{lam30} / fb_{inh} + PS_{bx30_inh}) * y_{300} / V_{lam30}$,
 if $y_{300} < 0$ then $y_{300}=0$ endif,
 $y_{301}' = PS_{bp31_inh} * f_{ent_inh} * y_{261} / Vent_{31} - (Q_{lam31} / fb_{inh} + PS_{bx31_inh}) * y_{301} / V_{lam31}$,
 if $y_{301} < 0$ then $y_{301}=0$ endif,
 $y_{302}' = PS_{bp32_inh} * f_{ent_inh} * y_{262} / Vent_{32} - (Q_{lam32} / fb_{inh} + PS_{bx32_inh}) * y_{302} / V_{lam32}$,
 if $y_{302} < 0$ then $y_{302}=0$ endif,
 $y_{303}' = PS_{bp33_inh} * f_{ent_inh} * y_{263} / Vent_{33} - (Q_{lam33} / fb_{inh} + PS_{bx33_inh}) * y_{303} / V_{lam33}$,
 if $y_{303} < 0$ then $y_{303}=0$ endif,
 $y_{304}' = PS_{bp34_inh} * f_{ent_inh} * y_{264} / Vent_{34} - (Q_{lam34} / fb_{inh} + PS_{bx34_inh}) * y_{304} / V_{lam34}$,
 if $y_{304} < 0$ then $y_{304}=0$ endif,
 $y_{305}' = PS_{bp35_inh} * f_{ent_inh} * y_{265} / Vent_{35} - (Q_{lam35} / fb_{inh} + PS_{bx35_inh}) * y_{305} / V_{lam35}$,
 if $y_{305} < 0$ then $y_{305}=0$ endif,
 $y_{306}' = PS_{bp36_inh} * f_{ent_inh} * y_{266} / Vent_{36} - (Q_{lam36} / fb_{inh} + PS_{bx36_inh}) * y_{306} / V_{lam36}$,
 if $y_{306} < 0$ then $y_{306}=0$ endif,
 $y_{307}' = PS_{bp37_inh} * f_{ent_inh} * y_{267} / Vent_{37} - (Q_{lam37} / fb_{inh} + PS_{bx37_inh}) * y_{307} / V_{lam37}$,
 if $y_{307} < 0$ then $y_{307}=0$ endif,

$y_{308}' = PS_{bp38_inh} * f_{ent_inh} * y_{268} / V_{ent38} - (Q_{lam38} / f_{b_inh} + PS_{bx38_inh}) * y_{308} / V_{lam38}$,

if $y_{308} < 0$ then $y_{308} = 0$ endif,

$y_{309}' = PS_{bp39_inh} * f_{ent_inh} * y_{269} / V_{ent39} - (Q_{lam39} / f_{b_inh} + PS_{bx39_inh}) * y_{309} / V_{lam39}$,

if $y_{309} < 0$ then $y_{309} = 0$ endif,

$y_{310}' = PS_{bp40_inh} * f_{ent_inh} * y_{270} / V_{ent40} - (Q_{lam40} / f_{b_inh} + PS_{bx40_inh}) * y_{310} / V_{lam40}$,

if $y_{310} < 0$ then $y_{310} = 0$ endif,

; Drug amount in the colon

$y_{311}' = ((9.0 y_{230} - y_{229}) / 8.0) Q - k_{rec} * y_{311}$,

; Drug amount in the feces

$y_{312}' = k_{rec} * y_{311} * V_c$,

; Drug concentration in the stomach

$y_{313}' = k_a * y_{320} * V_{es} / V_g - k_g * y_{313}$,

; % of dose in stomach (not used in this study)

$y_{314} = y_{313} V_g / \text{dose_inh} * 100$,

; % of dose in jejunum (not used in this study)

$y_{315} = (y_{191} + y_{192} + y_{193} + y_{194} + y_{195} + y_{196} + y_{197} + y_{198} + y_{199} + y_{200} + y_{201} + y_{202} + y_{203} + y_{204} + y_{205} + y_{206} + y_{207} + y_{208} + y_{209} + y_{210}) V / \text{div} / \text{dose_inh} * 100$,

; % of dose in ileum (not used in this study)

$y_{316} = (y_{211} + y_{212} + y_{213} + y_{214} + y_{215} + y_{216} + y_{217} + y_{218} + y_{219} + y_{220} + y_{221} + y_{222} + y_{223} + y_{224} + y_{225} + y_{226} + y_{227} + y_{228} + y_{229} + y_{230}) V / \text{div} / \text{dose_inh} * 100,$

; % of dose in colon(not used in this study)

$y_{317} = y_{311} V_c / \text{dose_inh} * 100,$

; % of dose in whole lumen (not used in this study)

$y_{318} = y_{315} + y_{316} + y_{317},$

; Drug amount in the gastrointestinal tract (not used in this study)

$y_{319} = y_{314} + y_{315} + y_{316} + y_{317},$

; Drug concentration in the esophagus

$y_{320}' = -k_a * y_{320},$

; not used in this study

$y_{321} = y_{320}$

; Drug amount in the enterocytes

$y_{322} = (y_{231} + y_{232} + y_{233} + y_{234} + y_{235} + y_{236} + y_{237} + y_{238} + y_{239} + y_{240} + y_{241} + y_{242} + y_{243} + y_{244} + y_{245} + y_{246} + y_{247} + y_{248} + y_{249} + y_{250} + y_{251} + y_{252} + y_{253} + y_{254} + y_{255} + y_{256} + y_{257} + y_{258} + y_{259} + y_{260} + y_{261} + y_{262} + y_{263} + y_{264} + y_{265} + y_{266} + y_{267} + y_{268} + y_{269} + y_{270}),$

; Drug amount in the lamina propria

$$y_{323} = (y_{231} + y_{232} + y_{233} + y_{234} + y_{235} + y_{236} + y_{237} + y_{238} + y_{239} + y_{240} + y_{241} + y_{242} + y_{243} + y_{244} + y_{245} + y_{246} + y_{247} + y_{248} + y_{249} + y_{250} + y_{251} + y_{252} + y_{253} + y_{254} + y_{255} + y_{256} + y_{257} + y_{258} + y_{259} + y_{260} + y_{261} + y_{262} + y_{263} + y_{264} + y_{265} + y_{266} + y_{267} + y_{268} + y_{269} + y_{270}),$$

; Drug accumulated amount in the portal vein

$$y_{324}' =$$

$$(y_{271}/V_{lam1} * Q_{lam1} + y_{272}/V_{lam2} * Q_{lam2} + y_{273}/V_{lam3} * Q_{lam3} + y_{274}/V_{lam4} * Q_{lam4} + y_{275}/V_{lam5} * Q_{lam5} + y_{276}/V_{lam6} * Q_{lam6} + y_{277}/V_{lam7} * Q_{lam7} + y_{278}/V_{lam8} * Q_{lam8} + y_{279}/V_{lam9} * Q_{lam9} + y_{280}/V_{lam10} * Q_{lam10} + y_{281}/V_{lam11} * Q_{lam11} + y_{282}/V_{lam12} * Q_{lam12} + y_{283}/V_{lam13} * Q_{lam13} + y_{284}/V_{lam14} * Q_{lam14} + y_{285}/V_{lam15} * Q_{lam15} + y_{286}/V_{lam16} * Q_{lam16} + y_{287}/V_{lam17} * Q_{lam17} + y_{288}/V_{lam18} * Q_{lam18} + y_{289}/V_{lam19} * Q_{lam19} + y_{290}/V_{lam20} * Q_{lam20} + y_{291}/V_{lam21} * Q_{lam21} + y_{292}/V_{lam22} * Q_{lam22} + y_{293}/V_{lam23} * Q_{lam23} + y_{294}/V_{lam24} * Q_{lam24} + y_{295}/V_{lam25} * Q_{lam25} + y_{296}/V_{lam26} * Q_{lam26} + y_{297}/V_{lam27} * Q_{lam27} + y_{298}/V_{lam28} * Q_{lam28} + y_{299}/V_{lam29} * Q_{lam29} + y_{300}/V_{lam30} * Q_{lam30} + y_{301}/V_{lam31} * Q_{lam31} + y_{302}/V_{lam32} * Q_{lam32} + y_{303}/V_{lam33} * Q_{lam33} + y_{304}/V_{lam34} * Q_{lam34} + y_{305}/V_{lam35} * Q_{lam35} + y_{306}/V_{lam36} * Q_{lam36} + y_{307}/V_{lam37} * Q_{lam37} + y_{308}/V_{lam38} * Q_{lam38} + y_{309}/V_{lam39} * Q_{lam39} + y_{310}/V_{lam40} * Q_{lam40})/fb_inh,$$

; F_A of an inhibitor

$$y_{325} = 1 - y_{311}/dose_inh,$$

; F_{AFG} of an inhibitor

$$y_{326} = y_{324}/dose_inh,$$

; F_G of an inhibitor

$$y_{327} = y_{326} / y_{325},$$

; Intestinal clearance amount

$$y_{328}' = \text{CL1_inh} * y_{231} / \text{Vent1} + \text{CL2_inh} * y_{232} / \text{Vent2} + \text{CL3_inh} * y_{233} / \text{Vent3} + \text{CL4_inh} * y_{234} / \text{Vent4} + \text{CL5_inh} * y_{235} / \text{Vent5} + \text{CL6_inh} * y_{236} / \text{Vent6} + \text{CL7_inh} * y_{237} / \text{Vent7} + \text{CL8_inh} * y_{238} / \text{Vent8} + \text{CL9_inh} * y_{239} / \text{Vent9} + \text{CL10_inh} * y_{240} / \text{Vent10} + \text{CL11_inh} * y_{241} / \text{Vent11} + \text{CL12_inh} * y_{242} / \text{Vent12} + \text{CL13_inh} * y_{243} / \text{Vent13} + \text{CL14_inh} * y_{244} / \text{Vent14} + \text{CL15_inh} * y_{245} / \text{Vent15} + \text{CL16_inh} * y_{246} / \text{Vent16} + \text{CL17_inh} * y_{247} / \text{Vent17} + \text{CL18_inh} * y_{248} / \text{Vent18} + \text{CL19_inh} * y_{249} / \text{Vent19} + \text{CL20_inh} * y_{250} / \text{Vent20} + \text{CL21_inh} * y_{251} / \text{Vent21} + \text{CL22_inh} * y_{252} / \text{Vent22} + \text{CL23_inh} * y_{253} / \text{Vent23} + \text{CL24_inh} * y_{254} / \text{Vent24} + \text{CL25_inh} * y_{255} / \text{Vent25} + \text{CL26_inh} * y_{256} / \text{Vent26} + \text{CL27_inh} * y_{257} / \text{Vent27} + \text{CL28_inh} * y_{258} / \text{Vent28} + \text{CL29_inh} * y_{259} / \text{Vent29} + \text{CL30_inh} * y_{260} / \text{Vent30} + \text{CL31_inh} * y_{261} / \text{Vent31} + \text{CL32_inh} * y_{262} / \text{Vent32} + \text{CL33_inh} * y_{263} / \text{Vent33} + \text{CL34_inh} * y_{264} / \text{Vent34} + \text{CL35_inh} * y_{265} / \text{Vent35} + \text{CL36_inh} * y_{266} / \text{Vent36} + \text{CL37_inh} * y_{267} / \text{Vent37} + \text{CL38_inh} * y_{268} / \text{Vent38} + \text{CL39_inh} * y_{269} / \text{Vent39} + \text{CL40_inh} * y_{270} / \text{Vent40},$$

; Drug amount in the portal vein

$$y_{329}'$$

$$= (y_{271} / \text{Vlam1} * \text{Qlam1} + y_{272} / \text{Vlam2} * \text{Qlam2} + y_{273} / \text{Vlam3} * \text{Qlam3} + y_{274} / \text{Vlam4} * \text{Qlam4} + y_{275} / \text{Vlam5} * \text{Qlam5} + y_{276} / \text{Vlam6} * \text{Qlam6} + y_{277} / \text{Vlam7} * \text{Qlam7} + y_{278} / \text{Vlam8} * \text{Qlam8} + y_{279} / \text{Vlam9} * \text{Qlam9} + y_{280} / \text{Vlam10} * \text{Qlam10} + y_{281} / \text{Vlam11} * \text{Qlam11} + y_{282} / \text{Vlam12} * \text{Qlam12} + y_{283} / \text{Vlam13} * \text{Qlam13} + y_{284} / \text{Vlam14} * \text{Qlam14} + y_{285} / \text{Vlam15} * \text{Qlam15} + y_{286} / \text{Vlam16} * \text{Qlam16} + y_{287} / \text{Vlam17} * \text{Qlam17} + y_{288} / \text{Vlam18} * \text{Qlam18} + y_{289} / \text{Vlam19} * \text{Qlam19} + y_{290} / \text{Vlam20} * \text{Qlam20} + y_{291} / \text{Vlam21} * \text{Qlam21} + y_{292} / \text{Vlam22} * \text{Qlam22} + y_{293} / \text{Vlam23} * \text{Qlam23} + y_{294} / \text{Vlam24} * \text{Qlam24} + y_{295} / \text{Vlam25} * \text{Qlam25} + y_{296} / \text{Vlam26} * \text{Qlam26} + y_{297} / \text{Vlam27} * \text{Qlam27} + y_{298} / \text{Vlam28} * \text{Qlam28} + y_{299} / \text{Vlam29} * \text{Qlam29} + y_{300} / \text{Vlam30} * \text{Qlam30} + y_{301} / \text{Vlam31} * \text{Qlam31} + y_{302} / \text{Vlam32} * \text{Qlam32} + y_{303} / \text{Vlam33} * \text{Qlam33} + y_{304} / \text{Vlam34} * \text{Qlam34} + y_{305} / \text{Vlam35} * \text{Qlam35} + y_{306} / \text{Vlam36} * \text{Qlam36} + y_{307} / \text{Vlam37} * \text{Qlam37} + y_{308} / \text{Vlam38} * \text{Qlam38} + y_{309} / \text{Vlam39} * \text{Qlam39} + y_{310} / \text{Vlam40} * \text{Qlam40})$$

$m_{32} \cdot Q_{lam32+y303} / V_{lam33} \cdot Q_{lam33+y304} / V_{lam34} \cdot Q_{lam34+y305} / V_{lam35} \cdot Q_{lam35+y306}$
 $/ V_{lam36} \cdot Q_{lam36+y307} / V_{lam37} \cdot Q_{lam37+y308} / V_{lam38} \cdot Q_{lam38+y309} / V_{lam39} \cdot Q_{lam39+y310} / V_{lam40} \cdot Q_{lam40} / fb_inh - Q_{pv} \cdot y_{329} / V_{pv},$

; Drug concentration in the liver

$y_{330}' = (Q_{pv} \cdot y_{329} / V_{pv} - Q_h \cdot y_{330} / K_{p_liver_inh} \cdot R_{b_inh} -$
 $fb_inh \cdot R_{b_inh} / K_{p_liver_inh} \cdot CL_{int_h_inh} \cdot y_{330} + Q_{ha} \cdot y_{331}) / V_{liver},$

; Drug concentration in the blood

$y_{331}' = (Q_h \cdot y_{330} / K_{p_liver_inh} \cdot R_{b_inh} - Q_{ha} \cdot y_{331} -$
 $k_{12_inh} \cdot y_{331} \cdot V_b + k_{21_inh} \cdot y_{332}) / V_{b_inh},$

; Drug concentration in the peripheral compartment 1

; The number of peripheral compartments can be increased as necessary.

$y_{332}' = k_{12_inh} \cdot y_{331} \cdot V_{b_inh} - k_{21} \cdot y_{332},$

; Drug concentration in the blood (unit: ug/L)

$y_{333} = y_{331} \cdot 1000,$

; Whole drug concentration of a substrate in the enterocytes

$y_{334} =$

$(y_{101} + y_{102} + y_{103} + y_{104} + y_{105} + y_{106} + y_{107} + y_{108} + y_{109} + y_{110} + y_{111} + y_{112} + y_{113} + y_{114} + y_{115} + y_{116} + y_{117} + y_{118} + y_{119} + y_{120} + y_{121} + y_{122} + y_{123} + y_{124} + y_{125} + y_{126} + y_{127} + y_{128} + y_{129} + y_{130} + y_{131} + y_{132} + y_{133} + y_{134} + y_{135} + y_{136} + y_{137} + y_{138} + y_{139} + y_{140}) / (V_{ent1} + V_{ent2} + V_{ent3} + V_{ent4} + V_{ent5} + V_{ent6} + V_{ent7} + V_{ent8} + V_{ent9} + V_{ent10} + V_{ent11} + V_{ent12} + V_{ent13} + V_{ent14} + V_e$

nt15+Vent16+Vent17+Vent18+Vent19+Vent20+Vent21+Vent22+Vent23+Vent24+Vent25+
Vent26+Vent27+Vent28+Vent29+Vent30+Vent31+Vent32+Vent33+Vent34+Vent35+Vent3
6+Vent37+Vent38+Vent39+Vent40)

; Drug concentration of a substrate in each compartment of the enterocytes

$$y335 = y101/Vent1,$$

$$y336 = y102/Vent2,$$

$$y337 = y103/Vent3,$$

$$y338 = y104/Vent4,$$

$$y339 = y105/Vent5,$$

$$y340 = y106/Vent6,$$

$$y341 = y107/Vent7,$$

$$y342 = y108/Vent8,$$

$$y343 = y109/Vent9,$$

$$y344 = y110/Vent10,$$

$$y345 = y111/Vent11,$$

$$y346 = y112/Vent12,$$

$$y347 = y113/Vent13,$$

$$y348 = y114/Vent14,$$

$$y349 = y115/Vent15,$$

$$y350 = y116/Vent16,$$

$$y351 = y117/Vent17,$$

$$y352 = y118/Vent18,$$

$$y353 = y119/Vent19,$$

$$y354 = y120/Vent20,$$

$$y355 = y121/Vent21,$$

$$y356 = y122/Vent22,$$

$$y357 = y123/Vent23,$$

$$y358 = y124/Vent24,$$

$$y359 = y125/Vent25,$$

$$y360 = y126/Vent26,$$

$$y361 = y127/Vent27,$$

$$y362 = y128/Vent28,$$

$$y363 = y129/Vent29,$$

$$y364 = y130/Vent30,$$

$$y365 = y131/Vent31,$$

$$y366 = y132/Vent32,$$

$$y367 = y133/Vent33,$$

$$y368 = y134/Vent34,$$

$$y369 = y135/Vent35,$$

$$y370 = y136/Vent36,$$

$$y371 = y137/Vent37,$$

$$y372 = y138/Vent38,$$

$$y373 = y139/Vent39,$$

$$y374 = y140/Vent40,$$

; Drug accumulation of a substrate in each compartment of the portal vein

$$y375' = y141/Vlam1 * Qlam1 / fb / dose,$$

$$y376' = y142/Vlam2 * Qlam2 / fb / dose,$$

$$y377' = y143/Vlam3 * Qlam3 / fb / dose,$$

y378'=y144/Vlam4*Qlam4/fb/dose,
y379'=y145/Vlam5*Qlam5/fb/dose,
y380'=y146/Vlam6*Qlam6/fb/dose,
y381'=y147/Vlam7*Qlam7/fb/dose,
y382'=y148/Vlam8*Qlam8/fb/dose,
y383'=y149/Vlam9*Qlam9/fb/dose,
y384'=y150/Vlam10*Qlam10/fb/dose,
y385'=y151/Vlam11*Qlam11/fb/dose,
y386'=y152/Vlam12*Qlam12/fb/dose,
y387'=y153/Vlam13*Qlam13/fb/dose,
y388'=y154/Vlam14*Qlam14/fb/dose,
y389'=y155/Vlam15*Qlam15/fb/dose,
y390'=y156/Vlam16*Qlam16/fb/dose,
y391'=y157/Vlam17*Qlam17/fb/dose,
y392'=y158/Vlam18*Qlam18/fb/dose,
y393'=y159/Vlam19*Qlam19/fb/dose,
y394'=y160/Vlam20*Qlam20/fb/dose,
y395'=y161/Vlam21*Qlam21/fb/dose,
y396'=y162/Vlam22*Qlam22/fb/dose,
y397'=y163/Vlam23*Qlam23/fb/dose,
y398'=y164/Vlam24*Qlam24/fb/dose,
y399'=y165/Vlam25*Qlam25/fb/dose,
y400'=y166/Vlam26*Qlam26/fb/dose,
y401'=y167/Vlam27*Qlam27/fb/dose,
y402'=y168/Vlam28*Qlam28/fb/dose,

$y_{403}' = y_{169} / V_{lam29} * Q_{lam29} / fb / dose,$
 $y_{404}' = y_{170} / V_{lam30} * Q_{lam30} / fb / dose,$
 $y_{405}' = y_{171} / V_{lam31} * Q_{lam31} / fb / dose,$
 $y_{406}' = y_{172} / V_{lam32} * Q_{lam32} / fb / dose,$
 $y_{407}' = y_{173} / V_{lam33} * Q_{lam33} / fb / dose,$
 $y_{408}' = y_{174} / V_{lam34} * Q_{lam34} / fb / dose,$
 $y_{409}' = y_{175} / V_{lam35} * Q_{lam35} / fb / dose,$
 $y_{410}' = y_{176} / V_{lam36} * Q_{lam36} / fb / dose,$
 $y_{411}' = y_{177} / V_{lam37} * Q_{lam37} / fb / dose,$
 $y_{412}' = y_{178} / V_{lam38} * Q_{lam38} / fb / dose,$
 $y_{413}' = y_{179} / V_{lam39} * Q_{lam39} / fb / dose,$
 $y_{414}' = y_{180} / V_{lam40} * Q_{lam40} / fb / dose,$

; ***** Preparative Calculation *****div = 40,

; 40 is number of segments

; in this model, dispersion is defined by volume not by length

$b = Q \text{ div} / V,$

$k_{wn} = k_w / \text{div},$

; section 1

$D_{sp_1} = A * \exp(-B * x_1) + 0.005,$

$a_1 = D_{sp_1} Q \text{ div} / V,$

$c_{1_1} = -a_1 / 12 - b / 12,$

$c_{2_1} = a_1^{4/3} + b^{2/3},$

$$c3_1 = -a_1^{5/2}, ; -ke,$$

$$c4_1 = a_1^{4/3} - b^{2/3},$$

$$c5_1 = -a_1/12 + b/12,$$

$$c3a_1 = -c1_1 + c3_1 + c4_1 + c5_1,$$

$$c4a_1 = c4_1 + c5_1,$$

$$c2a_1 = c1_1 + c2_1,$$

$$kw_1 = kw,$$

$$sw_1 = sw,$$

; section 2

$$Dsp_2 = A * \exp(-B * x_2) + 0.005,$$

$$a_2 = Dsp_2 Q \text{ div div} / V,$$

$$c1_2 = -a_2/12 - b/12,$$

$$c2_2 = a_2^{4/3} + b^{2/3},$$

$$c3_2 = -a_2^{5/2}, ; -ke,$$

$$c4_2 = a_2^{4/3} - b^{2/3},$$

$$c5_2 = -a_2/12 + b/12,$$

$$c3a_2 = -c1_2 + c3_2 + c4_2 + c5_2,$$

$$c4a_2 = c4_2 + c5_2,$$

$$c2a_2 = c1_2 + c2_2,$$

$$c3_2_kw = c3_2 - kw,$$

$$sw_2 = sw,$$

; section 3

$$Dsp_3 = A*\exp(-B*x_3)+0.005,$$

$$a_3 = Dsp_3 Q \text{ div div} / V,$$

$$c1_3 = -a_3/12 - b/12,$$

$$c2_3 = a_3^{4/3} + b^{2/3},$$

$$c3_3 = -a_3^{5/2}, ; - ke,$$

$$c4_3 = a_3^{4/3} - b^{2/3},$$

$$c5_3 = -a_3/12 + b/12,$$

$$c3_3_kw = c3_3 - kw,$$

$$sw_3 = sw,$$

; section 4

$$Dsp_4 = A*\exp(-B*x_4)+0.005,$$

$$a_4 = Dsp_4 Q \text{ div div} / V,$$

$$c1_4 = -a_4/12 - b/12,$$

$$c2_4 = a_4^{4/3} + b^{2/3},$$

$$c3_4 = -a_4^{5/2}, ; - ke,$$

$$c4_4 = a_4^{4/3} - b^{2/3},$$

$$c5_4 = -a_4/12 + b/12,$$

$$c3_4_kw = c3_4 - kw,$$

$$sw_4 = sw,$$

; section 5

$$Dsp_5 = A*\exp(-B*x_5)+0.005,$$

$$a_5 = Dsp_5 Q \text{ div div} / V,$$

$$c1_5 = -a_5/12 - b/12,$$

$$c2_5 = a_5^{4/3} + b^{2/3},$$

$$c3_5 = -a_5^{5/2}, ; - ke,$$

$$c4_5 = a_5^{4/3} - b^{2/3},$$

$$c5_5 = -a_5/12 + b/12,$$

$$c3_5_{kw} = c3_5 - kw,$$

$$sw_5 = sw,$$

; section 6

$$Dsp_6 = A * \exp(-B * x_6) + 0.005,$$

$$a_6 = Dsp_6 Q \text{ div div} / V,$$

$$c1_6 = -a_6/12 - b/12,$$

$$c2_6 = a_6^{4/3} + b^{2/3},$$

$$c3_6 = -a_6^{5/2}, ; - ke,$$

$$c4_6 = a_6^{4/3} - b^{2/3},$$

$$c5_6 = -a_6/12 + b/12,$$

$$c3_6_{kw} = c3_6 - kw,$$

$$sw_6 = sw,$$

; section 7

$$Dsp_7 = A * \exp(-B * x_7) + 0.005,$$

$$a_7 = Dsp_7 Q \text{ div div} / V,$$

$$c1_7 = -a_7/12 - b/12,$$

$$c2_7 = a_7^{4/3} + b^{2/3},$$

$$c3_7 = -a_7^{5/2}, ; - ke,$$

$$c4_7 = a_7^{4/3} - b^{2/3},$$

$$c5_7 = -a_7/12 + b/12,$$

$$c3_7_{kw} = c3_7 - kw,$$

$$sw_7 = sw,$$

; section 8

$$Dsp_8 = A * \exp(-B * x_8) + 0.005,$$

$$a_8 = Dsp_8 Q \text{ div div} / V,$$

$$c1_8 = -a_8/12 - b/12,$$

$$c2_8 = a_8^{4/3} + b^{2/3},$$

$$c3_8 = -a_8^{5/2}, ; - ke,$$

$$c4_8 = a_8^{4/3} - b^{2/3},$$

$$c5_8 = -a_8/12 + b/12,$$

$$c3_8_{kw} = c3_8 - kw,$$

$$sw_8 = sw,$$

; section 9

$$Dsp_9 = A * \exp(-B * x_9) + 0.005,$$

$$a_9 = Dsp_9 Q \text{ div div} / V,$$

$$c1_9 = -a_9/12 - b/12,$$

$$c2_9 = a_9^{4/3} + b^{2/3},$$

$$c3_9 = -a_9^{5/2}, ; - ke,$$

$$c4_9 = a_9^{4/3} - b^{2/3},$$

$$c5_9 = -a_9/12 + b/12,$$

$$c3_9_kw = c3_9 - kw,$$

$$sw_9 = sw,$$

; section 10

$$Dsp_10 = A * \exp(-B * x_10) + 0.005,$$

$$a_10 = Dsp_10 Q \text{ div div} / V,$$

$$c1_10 = -a_10/12 - b/12,$$

$$c2_10 = a_10^{4/3} + b^{2/3},$$

$$c3_10 = -a_10^{5/2}, ; - ke,$$

$$c4_10 = a_10^{4/3} - b^{2/3},$$

$$c5_10 = -a_10/12 + b/12,$$

$$c3_10_kw = c3_10 - kw,$$

$$sw_10 = sw,$$

; section 11

$$Dsp_11 = A * \exp(-B * x_11) + 0.005,$$

$$a_11 = Dsp_11 Q \text{ div div} / V,$$

$$c1_11 = -a_11/12 - b/12,$$

$$c2_{11} = a_{11}^{4/3} + b^{2/3},$$

$$c3_{11} = -a_{11}^{5/2}, ; -ke,$$

$$c4_{11} = a_{11}^{4/3} - b^{2/3},$$

$$c5_{11} = -a_{11}/12 + b/12,$$

$$c3_{11_kw} = c3_{11} - kw,$$

$$sw_{11} = sw,$$

; section 12

$$Dsp_{12} = A * \exp(-B * x_{12}) + 0.005,$$

$$a_{12} = Dsp_{12} Q \text{ div div} / V,$$

$$c1_{12} = -a_{12}/12 - b/12,$$

$$c2_{12} = a_{12}^{4/3} + b^{2/3},$$

$$c3_{12} = -a_{12}^{5/2}, ; -ke,$$

$$c4_{12} = a_{12}^{4/3} - b^{2/3},$$

$$c5_{12} = -a_{12}/12 + b/12,$$

$$c3_{12_kw} = c3_{12} - kw,$$

$$sw_{12} = sw,$$

; section 13

$$Dsp_{13} = A * \exp(-B * x_{13}) + 0.005,$$

$$a_{13} = Dsp_{13} Q \text{ div div} / V,$$

$$c1_{13} = -a_{13}/12 - b/12,$$

$$c2_{13} = a_{13}^{4/3} + b^{2/3},$$

$$c3_{13} = -a_{13}^{5/2}, ; - ke,$$

$$c4_{13} = a_{13}^{4/3} - b^{2/3},$$

$$c5_{13} = -a_{13}/12 + b/12,$$

$$c3_{13_kw} = c3_{13} - kw,$$

$$sw_{13} = sw,$$

; section 14

$$Dsp_{14} = A * \exp(-B * x_{14}) + 0.005,$$

$$a_{14} = Dsp_{14} Q \text{ div div} / V,$$

$$c1_{14} = -a_{14}/12 - b/12,$$

$$c2_{14} = a_{14}^{4/3} + b^{2/3},$$

$$c3_{14} = -a_{14}^{5/2}, ; - ke,$$

$$c4_{14} = a_{14}^{4/3} - b^{2/3},$$

$$c5_{14} = -a_{14}/12 + b/12,$$

$$c3_{14_kw} = c3_{14} - kw,$$

$$sw_{14} = sw,$$

; section 15

$$Dsp_{15} = A * \exp(-B * x_{15}) + 0.005,$$

$$a_{15} = Dsp_{15} Q \text{ div div} / V,$$

$$c1_{15} = -a_{15}/12 - b/12,$$

$$c2_{15} = a_{15}^{4/3} + b^{2/3},$$

$$c3_{15} = -a_{15}^{5/2}, ; - ke,$$

$$c4_{15} = a_{15}^{4/3} - b^{2/3},$$

$$c5_{15} = -a_{15}/12 + b/12,$$

$$c3_{15_kw} = c3_{15} - kw,$$

$$sw_{15} = sw,$$

; section 16

$$Dsp_{16} = A * \exp(-B * x_{16}) + 0.005,$$

$$a_{16} = Dsp_{16} Q \text{ div div} / V,$$

$$c1_{16} = -a_{16}/12 - b/12,$$

$$c2_{16} = a_{16}^{4/3} + b^{2/3},$$

$$c3_{16} = -a_{16}^{5/2}, ; - ke,$$

$$c4_{16} = a_{16}^{4/3} - b^{2/3},$$

$$c5_{16} = -a_{16}/12 + b/12,$$

$$c3_{16_kw} = c3_{16} - kw,$$

$$sw_{16} = sw,$$

; section 17

$$Dsp_{17} = A * \exp(-B * x_{17}) + 0.005,$$

$$a_{17} = Dsp_{17} Q \text{ div div} / V,$$

$$c1_{17} = -a_{17}/12 - b/12,$$

$$c2_{17} = a_{17}^{4/3} + b^{2/3},$$

$$c3_{17} = -a_{17}^{5/2}, ; - ke,$$

$$c4_{17} = a_{17}^{4/3} - b^{2/3},$$

$$c5_{17} = -a_{17}/12 + b/12,$$

$$c3_{17_kw} = c3_{17} - kw,$$

$$sw_{17} = sw,$$

; section 18

$$Dsp_{18} = A * \exp(-B * x_{18}) + 0.005,$$

$$a_{18} = Dsp_{18} Q \text{ div div} / V,$$

$$c1_{18} = -a_{18}/12 - b/12,$$

$$c2_{18} = a_{18}^{4/3} + b^{2/3},$$

$$c3_{18} = -a_{18}^{5/2}, ; - ke,$$

$$c4_{18} = a_{18}^{4/3} - b^{2/3},$$

$$c5_{18} = -a_{18}/12 + b/12,$$

$$c3_{18_kw} = c3_{18} - kw,$$

$$sw_{18} = sw,$$

; section 19

$$Dsp_{19} = A * \exp(-B * x_{19}) + 0.005,$$

$$a_{19} = Dsp_{19} Q \text{ div div} / V,$$

$$c1_{19} = -a_{19}/12 - b/12,$$

$$c2_{19} = a_{19}^{4/3} + b^{2/3},$$

$$c3_{19} = -a_{19}^{5/2}, ; - ke,$$

$$c4_{19} = a_{19}^{4/3} - b^{2/3},$$

$$c5_{19} = -a_{19}/12 + b/12,$$

$$c3_{19_kw} = c3_{19-kw},$$

$$sw_{19}=sw,$$

; section 20

$$Dsp_{20}=A*\exp(-B*x_{20})+0.005,$$

$$a_{20} = Dsp_{20} Q \text{ div div} / V,$$

$$c1_{20}= -a_{20}/12 - b/12,$$

$$c2_{20}= a_{20}^{4/3} + b^{2/3},$$

$$c3_{20}= -a_{20}^{5/2}, ; - ke,$$

$$c4_{20}= a_{20}^{4/3} - b^{2/3},$$

$$c5_{20}= -a_{20}/12 + b/12,$$

$$c3_{20_kw} = c3_{20-kw},$$

$$sw_{20}=sw,$$

; section 21

$$Dsp_{21}= A*\exp(-B*x_{21})+0.005,$$

$$a_{21} = Dsp_{21} Q \text{ div div} / V,$$

$$c1_{21}= -a_{21}/12 - b/12,$$

$$c2_{21}= a_{21}^{4/3} + b^{2/3},$$

$$c3_{21}= -a_{21}^{5/2}, ; - ke,$$

$$c4_{21}= a_{21}^{4/3} - b^{2/3},$$

$$c5_{21}= -a_{21}/12 + b/12,$$

$$c3_{21_kw} = c3_{21-kw},$$

$$sw_21=sw,$$

; section 22

$$Dsp_22= A*\exp(-B*x_22)+0.005,$$

$$a_22 = Dsp_22 Q \text{ div div } / V,$$

$$c1_22= -a_22/12 - b/12,$$

$$c2_22= a_22^{4/3} + b^{2/3},$$

$$c3_22= -a_22^{5/2}, ; - ke,$$

$$c4_22= a_22^{4/3} - b^{2/3},$$

$$c5_22= -a_22/12 + b/12,$$

$$c3_22_kw = c3_22-kw,$$

$$sw_22=sw,$$

; section 23

$$Dsp_23= A*\exp(-B*x_23)+0.005,$$

$$a_23 = Dsp_23 Q \text{ div div } / V,$$

$$c1_23= -a_23/12 - b/12,$$

$$c2_23= a_23^{4/3} + b^{2/3},$$

$$c3_23= -a_23^{5/2}, ; - ke,$$

$$c4_23= a_23^{4/3} - b^{2/3},$$

$$c5_23= -a_23/12 + b/12,$$

$$c3_23_kw = c3_23-kw,$$

$$sw_23=sw,$$

; section 24

$$Dsp_24 = A * \exp(-B * x_24) + 0.005,$$

$$a_24 = Dsp_24 \cdot Q \cdot \text{div} \cdot \text{div} / V,$$

$$c1_24 = -a_24/12 - b/12,$$

$$c2_24 = a_24^{4/3} + b^{2/3},$$

$$c3_24 = -a_24^{5/2}, ; - ke,$$

$$c4_24 = a_24^{4/3} - b^{2/3},$$

$$c5_24 = -a_24/12 + b/12,$$

$$c3_24_kw = c3_24 - kw,$$

$$sw_24 = sw,$$

; section 25

$$Dsp_25 = A * \exp(-B * x_25) + 0.005,$$

$$a_25 = Dsp_25 \cdot Q \cdot \text{div} \cdot \text{div} / V,$$

$$c1_25 = -a_25/12 - b/12,$$

$$c2_25 = a_25^{4/3} + b^{2/3},$$

$$c3_25 = -a_25^{5/2}, ; - ke,$$

$$c4_25 = a_25^{4/3} - b^{2/3},$$

$$c5_25 = -a_25/12 + b/12,$$

$$c3_25_kw = c3_25 - kw,$$

$$sw_25 = sw,$$

; section 26

$$Dsp_{26} = A * \exp(-B * x_{26}) + 0.005,$$

$$a_{26} = Dsp_{26} Q \text{ div div} / V,$$

$$c1_{26} = -a_{26}/12 - b/12,$$

$$c2_{26} = a_{26}^{4/3} + b^{2/3},$$

$$c3_{26} = -a_{26}^{5/2}, ; - ke,$$

$$c4_{26} = a_{26}^{4/3} - b^{2/3},$$

$$c5_{26} = -a_{26}/12 + b/12,$$

$$c3_{26_kw} = c3_{26} - kw,$$

$$sw_{26} = sw,$$

; section 27

$$Dsp_{27} = A * \exp(-B * x_{27}) + 0.005,$$

$$a_{27} = Dsp_{27} Q \text{ div div} / V,$$

$$c1_{27} = -a_{27}/12 - b/12,$$

$$c2_{27} = a_{27}^{4/3} + b^{2/3},$$

$$c3_{27} = -a_{27}^{5/2}, ; - ke,$$

$$c4_{27} = a_{27}^{4/3} - b^{2/3},$$

$$c5_{27} = -a_{27}/12 + b/12,$$

$$c3_{27_kw} = c3_{27} - kw,$$

$$sw_{27} = sw,$$

; section 28

$$Dsp_{28} = A \cdot \exp(-B \cdot x_{28}) + 0.005,$$

$$a_{28} = Dsp_{28} \cdot Q \cdot \text{div div} / V,$$

$$c1_{28} = -a_{28}/12 - b/12,$$

$$c2_{28} = a_{28}^{4/3} + b^{2/3},$$

$$c3_{28} = -a_{28}^{5/2}, ; - ke,$$

$$c4_{28} = a_{28}^{4/3} - b^{2/3},$$

$$c5_{28} = -a_{28}/12 + b/12,$$

$$c3_{28_kw} = c3_{28} - kw,$$

$$sw_{28} = sw,$$

; section 29

$$Dsp_{29} = A \cdot \exp(-B \cdot x_{29}) + 0.005,$$

$$a_{29} = Dsp_{29} \cdot Q \cdot \text{div div} / V,$$

$$c1_{29} = -a_{29}/12 - b/12,$$

$$c2_{29} = a_{29}^{4/3} + b^{2/3},$$

$$c3_{29} = -a_{29}^{5/2}, ; - ke,$$

$$c4_{29} = a_{29}^{4/3} - b^{2/3},$$

$$c5_{29} = -a_{29}/12 + b/12,$$

$$c3_{29_kw} = c3_{29} - kw,$$

$$sw_{29} = sw,$$

; section 30

$$Dsp_{30} = A \cdot \exp(-B \cdot x_{30}) + 0.005,$$

$$a_{30} = \text{Dsp}_{30} Q \text{ div div} / V,$$

$$c1_{30} = -a_{30}/12 - b/12,$$

$$c2_{30} = a_{30}^{4/3} + b^{2/3},$$

$$c3_{30} = -a_{30}^{5/2}, ; - ke,$$

$$c4_{30} = a_{30}^{4/3} - b^{2/3},$$

$$c5_{30} = -a_{30}/12 + b/12,$$

$$c3_{30_kw} = c3_{30} - kw,$$

$$sw_{30} = sw,$$

; section 31

$$\text{Dsp}_{31} = A * \exp(-B * x_{31}) + 0.005,$$

$$a_{31} = \text{Dsp}_{31} Q \text{ div div} / V,$$

$$c1_{31} = -a_{31}/12 - b/12,$$

$$c2_{31} = a_{31}^{4/3} + b^{2/3},$$

$$c3_{31} = -a_{31}^{5/2}, ; - ke,$$

$$c4_{31} = a_{31}^{4/3} - b^{2/3},$$

$$c5_{31} = -a_{31}/12 + b/12,$$

$$c3_{31_kw} = c3_{31} - kw,$$

$$sw_{31} = sw,$$

; section 32

$$\text{Dsp}_{32} = A * \exp(-B * x_{32}) + 0.005,$$

$$a_{32} = \text{Dsp}_{32} Q \text{ div div} / V,$$

$$c1_{32} = -a_{32}/12 - b/12,$$

$$c2_{32} = a_{32}^{4/3} + b^{2/3},$$

$$c3_{32} = -a_{32}^{5/2}, ; - ke,$$

$$c4_{32} = a_{32}^{4/3} - b^{2/3},$$

$$c5_{32} = -a_{32}/12 + b/12,$$

$$c3_{32_kw} = c3_{32} - kw,$$

$$sw_{32} = sw,$$

; section 33

$$Dsp_{33} = A * \exp(-B * x_{33}) + 0.005,$$

$$a_{33} = Dsp_{33} Q \text{ div div} / V,$$

$$c1_{33} = -a_{33}/12 - b/12,$$

$$c2_{33} = a_{33}^{4/3} + b^{2/3},$$

$$c3_{33} = -a_{33}^{5/2}, ; - ke,$$

$$c4_{33} = a_{33}^{4/3} - b^{2/3},$$

$$c5_{33} = -a_{33}/12 + b/12,$$

$$c3_{33_kw} = c3_{33} - kw,$$

$$sw_{33} = sw,$$

; section 34

$$Dsp_{34} = A * \exp(-B * x_{34}) + 0.005,$$

$$a_{34} = Dsp_{34} Q \text{ div div} / V,$$

$$c1_{34} = -a_{34}/12 - b/12,$$

$$c2_{34} = a_{34}^{4/3} + b^{2/3},$$

$$c3_{34} = -a_{34}^{5/2}, \quad ; -ke,$$

$$c4_{34} = a_{34}^{4/3} - b^{2/3},$$

$$c5_{34} = -a_{34}/12 + b/12,$$

$$c3_{34_kw} = c3_{34} - kw,$$

$$sw_{34} = sw,$$

; section 35

$$Dsp_{35} = A * \exp(-B * x_{35}) + 0.005,$$

$$a_{35} = Dsp_{35} Q \text{ div div} / V,$$

$$c1_{35} = -a_{35}/12 - b/12,$$

$$c2_{35} = a_{35}^{4/3} + b^{2/3},$$

$$c3_{35} = -a_{35}^{5/2}, \quad ; -ke,$$

$$c4_{35} = a_{35}^{4/3} - b^{2/3},$$

$$c5_{35} = -a_{35}/12 + b/12,$$

$$c3_{35_kw} = c3_{35} - kw,$$

$$sw_{35} = sw,$$

; section 36

$$Dsp_{36} = A * \exp(-B * x_{36}) + 0.005,$$

$$a_{36} = Dsp_{36} Q \text{ div div} / V,$$

$$c1_{36} = -a_{36}/12 - b/12,$$

$$c2_{36} = a_{36}^{4/3} + b^{2/3},$$

$$c3_{36} = -a_{36}^{5/2}, ; -ke,$$

$$c4_{36} = a_{36}^{4/3} - b^{2/3},$$

$$c5_{36} = -a_{36}/12 + b/12,$$

$$c3_{36_kw} = c3_{36} - kw,$$

$$sw_{36} = sw,$$

; section 37

$$Dsp_{37} = A * \exp(-B * x_{37}) + 0.005,$$

$$a_{37} = Dsp_{37} Q \text{ div div} / V,$$

$$c1_{37} = -a_{37}/12 - b/12,$$

$$c2_{37} = a_{37}^{4/3} + b^{2/3},$$

$$c3_{37} = -a_{37}^{5/2}, ; -ke,$$

$$c4_{37} = a_{37}^{4/3} - b^{2/3},$$

$$c5_{37} = -a_{37}/12 + b/12,$$

$$c3_{37_kw} = c3_{37} - kw,$$

$$sw_{37} = sw,$$

; section 38

$$Dsp_{38} = A * \exp(-B * x_{38}) + 0.005,$$

$$a_{38} = Dsp_{38} Q \text{ div div} / V,$$

$$c1_{38} = -a_{38}/12 - b/12,$$

$$c2_{38} = a_{38}^{4/3} + b^{2/3},$$

$$c3_38 = -a_38^{5/2}, ; - ke,$$

$$c4_38 = a_38^{4/3} - b^{2/3},$$

$$c5_38 = -a_38/12 + b/12,$$

$$c3_38_kw = c3_38 - kw,$$

$$sw_38 = sw,$$

; section 39

$$Dsp_39 = A * \exp(-B * x_39) + 0.005,$$

$$a_39 = Dsp_39 Q \text{ div div} / V,$$

$$c1_39 = -a_39/12 - b/12,$$

$$c2_39 = a_39^{4/3} + b^{2/3},$$

$$c3_39 = -a_39^{5/2}, ; - ke,$$

$$c4_39 = a_39^{4/3} - b^{2/3},$$

$$c5_39 = -a_39/12 + b/12,$$

$$c4a_39 = c4_39 + c5_39,$$

$$c2b_39 = c2_39 + c5_39,$$

$$c3b_39 = c3_39 + c4_39,$$

$$c3_39_kw = c3_39 - kw,$$

$$sw_39 = sw,$$

; section 40

$$Dsp_40 = A * \exp(-B * x_40) + 0.005,$$

$$a_40 = Dsp_40 Q \text{ div div} / V,$$

$$c1_40 = -a_40/12 - b/12,$$

$$c2_40 = a_40^{4/3} + b^{2/3},$$

$$c3_40 = -a_40^{5/2}, \text{ ; - ke,}$$

$$c4_40 = a_40^{4/3} - b^{2/3},$$

$$c5_40 = -a_40/12 + b/12,$$

$$c4a_40 = c4_40 + c5_40,$$

$$c2b_40 = c2_40 + c5_40,$$

$$c3b_40 = c3_40 + c4_40,$$

$$kw_40 = kw,$$

$$sw_40 = sw,$$

; Translation from Permeability in Caco-2 cells to in vivo permeability (Substrate)

$$P_Caco2 = (1 + ME_Caco2) / ME_Caco2 \text{ Papp_Caco2},$$

$$P_invivo = P_Caco2 \text{ psf_passive},$$

; Translation from Permeability in Caco-2 cells to in vivo permeability (Perpetrator)

$$P_Caco2_inh = (1 + ME_Caco2) / ME_Caco2 \text{ Papp_Caco2_inh},$$

$$P_invivo_inh = P_Caco2_inh \text{ psf_passive},$$

; ratio of blood flow in lamina propria at each compartment

$$Qlam1 = Qlam * Sapi_ratio1,$$

$$Qlam2 = Qlam * Sapi_ratio2,$$

$$Qlam3 = Qlam * Sapi_ratio3,$$

$$Qlam4 = Qlam * Sapi_ratio4,$$

$$Qlam5 = Qlam * Sapi_ratio5,$$

$Q_{lam6} = Q_{lam} * Sapi_ratio6,$
 $Q_{lam7} = Q_{lam} * Sapi_ratio7,$
 $Q_{lam8} = Q_{lam} * Sapi_ratio8,$
 $Q_{lam9} = Q_{lam} * Sapi_ratio9,$
 $Q_{lam10} = Q_{lam} * Sapi_ratio10,$
 $Q_{lam11} = Q_{lam} * Sapi_ratio11,$
 $Q_{lam12} = Q_{lam} * Sapi_ratio12,$
 $Q_{lam13} = Q_{lam} * Sapi_ratio13,$
 $Q_{lam14} = Q_{lam} * Sapi_ratio14,$
 $Q_{lam15} = Q_{lam} * Sapi_ratio15,$
 $Q_{lam16} = Q_{lam} * Sapi_ratio16,$
 $Q_{lam17} = Q_{lam} * Sapi_ratio17,$
 $Q_{lam18} = Q_{lam} * Sapi_ratio18,$
 $Q_{lam19} = Q_{lam} * Sapi_ratio19,$
 $Q_{lam20} = Q_{lam} * Sapi_ratio20,$
 $Q_{lam21} = Q_{lam} * Sapi_ratio21,$
 $Q_{lam22} = Q_{lam} * Sapi_ratio22,$
 $Q_{lam23} = Q_{lam} * Sapi_ratio23,$
 $Q_{lam24} = Q_{lam} * Sapi_ratio24,$
 $Q_{lam25} = Q_{lam} * Sapi_ratio25,$
 $Q_{lam26} = Q_{lam} * Sapi_ratio26,$
 $Q_{lam27} = Q_{lam} * Sapi_ratio27,$
 $Q_{lam28} = Q_{lam} * Sapi_ratio28,$
 $Q_{lam29} = Q_{lam} * Sapi_ratio29,$
 $Q_{lam30} = Q_{lam} * Sapi_ratio30,$

$$Qlam31 = Qlam * Sapi_ratio31,$$

$$Qlam32 = Qlam * Sapi_ratio32,$$

$$Qlam33 = Qlam * Sapi_ratio33,$$

$$Qlam34 = Qlam * Sapi_ratio34,$$

$$Qlam35 = Qlam * Sapi_ratio35,$$

$$Qlam36 = Qlam * Sapi_ratio36,$$

$$Qlam37 = Qlam * Sapi_ratio37,$$

$$Qlam38 = Qlam * Sapi_ratio38,$$

$$Qlam39 = Qlam * Sapi_ratio39,$$

$$Qlam40 = Qlam * Sapi_ratio40,$$

; Volume of caecum and colon

$$Vcae_col = Vcae + Vc,$$

; Relative Expression of P-gp in the small intestine

$$Arel_Pgp1 = (1 + x_1/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{x_1/2},$$

$$Arel_Pgp2 = (1 + x_1/Lsi + 1 + x_2/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_2 - x_1)/2},$$

$$Arel_Pgp3 = (1 + x_2/Lsi + 1 + x_3/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_3 - x_2)/2},$$

$$Arel_Pgp4 = (1 + x_3/Lsi + 1 + x_4/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_4 - x_3)/2},$$

$$Arel_Pgp5 = (1 + x_4/Lsi + 1 + x_5/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_5 - x_4)/2},$$

$$Arel_Pgp6 = (1 + x_5/Lsi + 1 + x_6/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_6 - x_5)/2},$$

$$Arel_Pgp7 = (1 + x_6/Lsi + 1 + x_7/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_7 - x_6)/2},$$

$$Arel_Pgp8 = (1 + x_7/Lsi + 1 + x_8/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_8 - x_7)/2},$$

$$Arel_Pgp9 = (1 + x_8/Lsi + 1 + x_9/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_9 - x_8)/2},$$

$$Arel_Pgp10 = (1 + x_9/Lsi + 1 + x_{10}/Lsi)^2 * Tot_Pgp / (3 * Lsi)^{(x_{10} - x_9)/2},$$

$$\text{Arel_Pgp11}=(1+x_{10}/\text{Lsi}+1+x_{11}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{11}-x_{10})/2,$$

$$\text{Arel_Pgp12}=(1+x_{11}/\text{Lsi}+1+x_{12}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{12}-x_{11})/2,$$

$$\text{Arel_Pgp13}=(1+x_{12}/\text{Lsi}+1+x_{13}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{13}-x_{12})/2,$$

$$\text{Arel_Pgp14}=(1+x_{13}/\text{Lsi}+1+x_{14}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{14}-x_{13})/2,$$

$$\text{Arel_Pgp15}=(1+x_{14}/\text{Lsi}+1+x_{15}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{15}-x_{14})/2,$$

$$\text{Arel_Pgp16}=(1+x_{15}/\text{Lsi}+1+x_{16}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{16}-x_{15})/2,$$

$$\text{Arel_Pgp17}=(1+x_{16}/\text{Lsi}+1+x_{17}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{17}-x_{16})/2,$$

$$\text{Arel_Pgp18}=(1+x_{17}/\text{Lsi}+1+x_{18}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{18}-x_{17})/2,$$

$$\text{Arel_Pgp19}=(1+x_{18}/\text{Lsi}+1+x_{19}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{19}-x_{18})/2,$$

$$\text{Arel_Pgp20}=(1+x_{19}/\text{Lsi}+1+x_{20}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{20}-x_{19})/2,$$

$$\text{Arel_Pgp21}=(1+x_{20}/\text{Lsi}+1+x_{21}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{21}-x_{20})/2,$$

$$\text{Arel_Pgp22}=(1+x_{21}/\text{Lsi}+1+x_{22}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{22}-x_{21})/2,$$

$$\text{Arel_Pgp23}=(1+x_{22}/\text{Lsi}+1+x_{23}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{23}-x_{22})/2,$$

$$\text{Arel_Pgp24}=(1+x_{23}/\text{Lsi}+1+x_{24}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{24}-x_{23})/2,$$

$$\text{Arel_Pgp25}=(1+x_{24}/\text{Lsi}+1+x_{25}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{25}-x_{24})/2,$$

$$\text{Arel_Pgp26}=(1+x_{25}/\text{Lsi}+1+x_{26}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{26}-x_{25})/2,$$

$$\text{Arel_Pgp27}=(1+x_{26}/\text{Lsi}+1+x_{27}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{27}-x_{26})/2,$$

$$\text{Arel_Pgp28}=(1+x_{27}/\text{Lsi}+1+x_{28}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{28}-x_{27})/2,$$

$$\text{Arel_Pgp29}=(1+x_{28}/\text{Lsi}+1+x_{29}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{29}-x_{28})/2,$$

$$\text{Arel_Pgp30}=(1+x_{29}/\text{Lsi}+1+x_{30}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{30}-x_{29})/2,$$

$$\text{Arel_Pgp31}=(1+x_{30}/\text{Lsi}+1+x_{31}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{31}-x_{30})/2,$$

$$\text{Arel_Pgp32}=(1+x_{31}/\text{Lsi}+1+x_{32}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{32}-x_{31})/2,$$

$$\text{Arel_Pgp33}=(1+x_{32}/\text{Lsi}+1+x_{33}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{33}-x_{32})/2,$$

$$\text{Arel_Pgp34}=(1+x_{33}/\text{Lsi}+1+x_{34}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{34}-x_{33})/2,$$

$$\text{Arel_Pgp35}=(1+x_{34}/\text{Lsi}+1+x_{35}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{35}-x_{34})/2,$$

$$\text{Arel_Pgp36}=(1+x_{35}/\text{Lsi}+1+x_{36}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{36}-x_{35})/2,$$

$$\text{Arel_Pgp37}=(1+x_{36}/\text{Lsi}+1+x_{37}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{37}-x_{36})/2,$$

$$\text{Arel_Pgp38}=(1+x_{37}/\text{Lsi}+1+x_{38}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{38}-x_{37})/2,$$

$$\text{Arel_Pgp39}=(1+x_{38}/\text{Lsi}+1+x_{39}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{39}-x_{38})/2,$$

$$\text{Arel_Pgp40}=(1+x_{39}/\text{Lsi}+1+x_{40}/\text{Lsi})^2*\text{Tot_Pgp}/(3*\text{Lsi})*(x_{40}-x_{39})/2,$$

Supplementary Table

Supplemental Table S1 Optimized parameters for intestinal water movement in ATOM

Parameter	Value	Unit
k_{es}	114.41	/h
$k_{water,sto}$	0	/h
$Se_{water,sto}$	88.63	mL/h
$k_{water,abs}$	881.26	/h
$Se_{water,abs}$	1500.00	mL/h

k_{es} : transit rate of drug (or water) from esophagus to stomach, $k_{water,sto}$: water absorption rate in stomach, $Se_{water,sto}$: water secretion clearance in stomach, $k_{water,abs}$: water absorption rate in lumen, $Se_{water,abs}$: water secretion clearance in lumen

Supplemental Table S2 Optimized parameters for transit rate from stomach to intestine, dispersion constants and intestinal flow rates using ^{99m}Tc -DTPA distribution in the lumen in ATOM

Subject and fasted/fe d	k_{sto} (h^{-1})	D_z (h^{-1})			M_t (h^{-1})		
		A	B	C	D	t_{lag}	E
Subject A fasted	4.27	816.59	0.082	11.34	0 ^a	-	1 ^a
Subject B fasted	5.23	584.19	0.044	15.00	0.92	1.05	1.01
Subject A fed	1.29	524.22	0.028	16.90	0.98	2.35	3.43
Subject B fed	0.89	201.76	0.031	12.50	0.91	2.12	1.82

These parameters were obtained by fitting analysis using ^{99m}Tc -DTPA distribution in the lumen reported by Haruta et al. .

a: Constant flow rate ($D=0$ and $E=1$) was adopted because AIC values were similar with the simulated results by ATOM using time-dependent flow rate.

k_{sto} : transit rate of drug or water from stomach to intestine, D_z : location-dependent dispersion number, M_t : time-dependent intestinal flow rate

Supplemental Table S3 Reported and optimized transit times in CAT using ^{99m}Tc -DTPA distribution in the lumen in both fasted and fed state.

Parameters	Value				Unit	
	Reported	Optimized				
		Subject A fasted	Subject B fasted	Subject A fed		Subject B fed
k_{sto}	4.00	4.17	3.45	1.11	0.77	/h
$k_{t,1}$	3.85	3.03	1.33	2.94	62.50	/h
$k_{t,2}$	1.08	3.03	208.33	357.14	2.33	/h
$k_{t,3}$	1.35	3.03	2.86	31.25	14.08	/h
$k_{t,4}$	1.72	0.81	1.64	9.09	0.65	/h
$k_{t,5}$	2.38	0.81	13.16	2.94	0.58	/h
$k_{t,6}$	3.45	0.81	0.68	0.20	58.82	/h

Each transit rate was calculated using the equation, Transit rate = 1/ Transit time. Reported transit times were referred from the report by Heikkinen et al. Optimized transit times were obtained by fitting analysis using observed distribution of ^{99m}Tc -DTPA in the lumen by Haruta et al.

k_{sto} : transit rate of drug or water from stomach to intestine, $k_{t,n}$: transit rate of drug or water from nth compartment in the lumen

Supplemental Table S4 Pharmacokinetic parameters of compounds

Parameter	Value	Unit	Reference and comment
midazolam			
$P_{app,Caco-2}$	0.117	cm/h	2
pKa	14 (acid), 4.57 (base)	-	ADMET Predictor® ver. 9.5
f_b	0.056	-	2
f_{ent}	0.056	-	Assumed to be equal with f_b
$V_{max,CYP3A}$	0.44	$\mu\text{g /h pmol}$ CYP3A	2
$K_{m,CYP3A,u}$	1.08	$\mu\text{g/mL}$	2
$K_{p,liver}$	6.96	-	3
R_B	0.55	-	4
CL_{int}	587336	mL/h	5 Optimized using plasma concentration after iv dosing
CL_R	0	mL/h	Assumed to be 0
$V_{central}$	99888	mL	5 Optimized using plasma concentration after iv dosing
k_{12}	0.288	/h	5 Optimized using plasma concentration after iv dosing
k_{21}	0.0042	/h	5 Optimized using plasma concentration after iv dosing

k_{12}^*	0.288	/h	Assumed to be same with k_{12}
k_{21}^*	0.0042	/h	Assumed to be same with k_{21}
Digoxin			
$P_{app,Caco-2}$	0.00396	cm/h	6
pKa	14(acid), 1(base)	-	ADMET Predictor® ver. 9.5
f_p	0.75	-	Digoxin Elixir, Printed Labeling
f_b	0.697	-	Calculated as $f_b=f_p/R_B$
f_{ent}	0.697	-	Assumed to be equal with f_b
$V_{max,P-gp}$	1.0×10^7	$\mu\text{g} / \text{h pmol}$	7
		P-gp	Optimized to the range of reported F_A values
$K_{m,Pgp,u}$	57	$\mu\text{g}/\text{mL}$	8
$K_{p,liver}$	1.35	-	GastroPlus® ver. 9.7
R_B	1.08	-	ADMET Predictor® ver. 9.0
CL_{int}^a	4793	mL/h	9
$CL_{R,Pgp}$	4080	mL/h	10
			Assumed from the CL_R change in P-gp inhibitor administration
$CL_{R,nonPgp}$	7560	mL/h	10
			Assumed from the CL_R change in P-gp inhibitor administration
$V_{central}$	11800	mL	10

k_{12}	2	/h	10	Optimized using plasma concentration of digoxin in iv administration
k_{21}	0.029	/h	10	Optimized using plasma concentration of digoxin in iv administration
k_{13}	2	/h	10	Optimized using plasma concentration of digoxin in iv administration
k_{31}	0.432	/h	10	Optimized using plasma concentration of digoxin in iv administration
k_{12}^*	2	/h		Assumed to be same with k_{12}
k_{21}^*	0.029	/h		Assumed to be same with k_{21}
k_{13}^*	2	/h		Assumed to be same with k_{13}
k_{31}^*	0.432	/h		Assumed to be same with k_{31}
itraconazole				
$P_{app,Caco-2}$	0.0245	cm/h	12	
pKa	14(acid), 4.57(base)	-		ADMET Predictor® ver. 9.5
f_b	0.0034	-		Calculated as $f_b=f_p/R_B$
f_p	0.002	-	13	

f_{ent}	0.0034	-	Assumed to be equal with f_b
$V_{max,CYP3A}$	0.0114	$\mu\text{g} / \text{h pmol}$ CYP3A	13
$K_{m,CYP3A,u}$	0.0313	$\mu\text{g}/\text{mL}$	13
$K_{p,liver}$	6.67	-	14
R_B	0.58	-	14
CL_{int}	14700000	mL/h	14
CL_R	0	mL/h	Assumed to be 0
$V_{central}$	59200	mL	14
$K_{i,CYP3A}$	0.212	$\mu\text{g}/\text{mL}$	35
clarithromycin			
$P_{app,Caco-2}$	0.0138	cm/h	15
pK_a	13.1(acid), 8.2(base)	-	16
f_b	0.32	-	16
f_{ent}	0.32	-	Assumed to be equal with f_b
$V_{max,CYP3A}$	0.013	$\mu\text{g} / \text{h pmol}$ CYP3A	24
$K_{m,CYP3A,u}$	36.43	$\mu\text{g}/\text{mL}$	17
LogP	2.3	-	18
R_B	0.74	-	16
CL_{int}	68504	mL/h	11
Optimized using plasma concentration of clarithromycin after po administration			

CL_R	6000	mL/h	19
V_{central}	25193	mL	20
			Optimized using plasma concentration of clarithromycin after iv administration
$K_{i,CYP3A}$	4.52	$\mu\text{g/mL}$	17
$K_{i,Pgp}$	324.61	$\mu\text{g/mL}$	32
k_{12}	8.91	/h	11
			Optimized using plasma concentration of clarithromycin after po administration
k_{21}	2.51	/h	11
			Optimized using plasma concentration of clarithromycin after po administration

a: The value was calculated using the number of hepatocytes (1.2×10^8 cells/g liver) and the weight of the liver (25.7 g liver/kg) (Watari et al., 2019)

Supplemental Table S5 Physiological parameters used in ATOM and CAT

Parameter	Value	Unit	Reference
Q_{pro}	18000	mL/h	2
Q_{pv}	37170	mL/h	3
Q_h	107100	mL/h	3
Q_{ha}	69930	mL/h	Calculated as $Q_{ha} = Q_h - Q_{pv}$
V_{es}	78.5	mL	Assumed a column with 1 cm radius and 25 cm length
V_{sto}	48.92	mL	GastroPlus® ver. 9.7
V_{pv}	70	mL	3
V_{liver}	1687	mL	3
V_{cae}	50.49	mL	GastroPlus® ver. 9.7
V_{col}	53.55	mL	GastroPlus® ver. 9.7
V_{si}	105	mL	31

Q_{pro} : blood flow of the blood capillaries in lamina propria, Q_{pv} : blood flow in the portal vein, Q_h : blood flow in the liver, Q_{ha} : arterial blood flow in the liver, V_{sto} : volume in the stomach, V_{pv} : volume in the portal vein, V_{liver} : volume in the liver, V_{cae} : volume in the caecum, V_{col} : volume in the colon, V_{si} : volume in the small intestine

Supplemental Table S6 Dataset for FG prediction about CYP3A or P-gp/CYP3A substrates and predicted or reported FG values

Compound	Dose	K _{m,u}		V _{max}		P _{app,caco-2}	f _b	pK _a ^a		F _G		
		CYP3A	P-gp	CYP3A	P-gp			acid	base	ATOM	TLM	Reported
	nmol	μg/mL	μg/mL	μg/h	μg/h	cm/h						
				pmol	pmol P-							
				CYP3A	gp							
alfentanil	7220	9.51	-	0.542	0	0.105	0.137	-	6.72	0.76	0.72	0.60
alprazolam	1290	81.9	-	0.074	0	0.0918	0.341	-	3.01	0.99	0.99	0.99
buspirone	4150	3.08	-	0.401	0	0.0914	0.062	-	7.16	0.56	0.51	0.22
cisapride	16100	1.49	-	0.245	0	0.108	0.020	11.2	7.30	0.63	0.56	0.55
cyclosporin	474000	1.68	0.0682	0.040	1.66×10 ⁶	0.0286	0.014	-	-	0.99	0.99	0.35

felodipine	26000	2.04	-	2.86	0	0.0151	0.068	10.95	0.51	0.02	0.02	0.53
lovastatin	49400	3.16	-	9.23	0	0.0522	0.030	-	-	0.04	0.04	0.09
midazolam	9200	1.08	-	0.440	0	0.117	0.056	-	4.57	0.39	0.36	0.48
nifedipine	28900	3.81	-	0.502	0	0.0846	0.066	11.06	1.28	0.63	0.60	0.74
nisoldipine	12900	0.815	-	3.75	0	0.072	0.003	11.2	0.68	0.03	0.03	0.11
rifabutin	177000	9.23	-	0.286	0	0.0342	0.483	6.92	8.12	0.94	0.85	0.21
saquinavir	1490000	0.201	0.579	0.731	1.66×10 ⁶	0.0497	0.038	10.83	6.40	0.94	0.92	0.18
sildenafil	52600	7.13	-	0.480	0	0.0922	0.063	9.38	7.60	0.78	0.77	0.54
simvastatin	95500	1.42	-	5.95	0	0.0245	0.025	-	-	0.02	0.02	0.19
trazodone	202000	116	-	1.64	0	0.0871	0.070	-	7.15	0.93	0.90	0.83
triazolam	729	29.2	-	0.090	0	0.101	0.161	-	2.85	0.98	0.98	0.45

zolpidem	16300	43.0	-	0.057	0	0.115	0.105	-	4.99	0.99	0.99	0.81
----------	-------	------	---	-------	---	-------	-------	---	------	------	------	------

Dataset of each compound, predicted (TLM) and reported F_G values were referred from the previous report by Ando et al.

a: Obtained from ADMET Predictor® version 9.5 (Simulations Plus Inc.)

Supplemental Table S7 Predictive performance of F_G values using ATOM and TLM compared with reported F_G values

Parameters	ATOM	TLM
Within ±0.3 (%)	65	71
AFE	1.06	1.10
RMSE	0.373	0.357

AFE: average fold error, RMSE: root mean square error

AFE and RMSE was calculated using the following equations. Parameter N represents the number of drugs.

$$\text{AFE} = 10^{\frac{\sum \log(\text{reported}/\text{predicted})}{N}}, \quad \text{RMSE} = \sqrt{\frac{\sum[(\text{predicted}-\text{reported})^2]}{N}}$$

Supplemental Table S8 Summary of AUCR ratio and F_G or F_A changes of digoxin and midazolam during DIs

midazolam^a

Perpetrator	AUCR ratio (predicted AUCR / reported AUCR)	F_G changes ($F_{G,p}/F_{G,control}$)
50 mg itraconazole	1.19	2.15
200 mg itraconazole	0.63	2.50
400 mg itraconazole	0.58	2.58

digoxin^b

Perpetrator	AUCR ratio (predicted AUCR / reported AUCR)	F_A changes ($F_{A,p}/F_{A,control}$)
250 mg clarithromycin	1.64	1.25

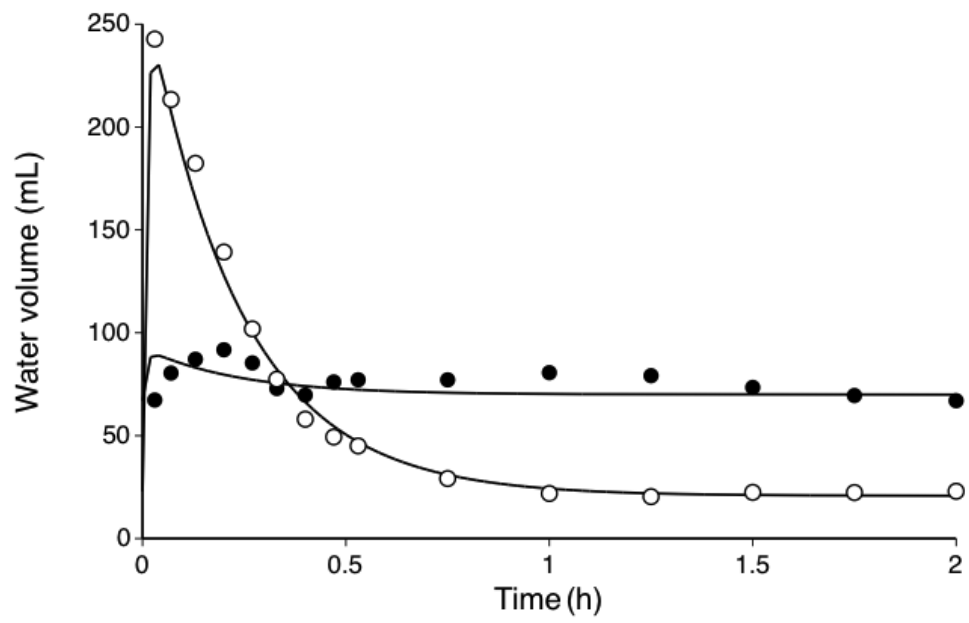
AUCR: AUC ratio, $F_{A,p}$: predicted F_A value of the substrate with the perpetrator, $F_{A,control}$: predicted F_A value of the substrate in the control, $F_{G,p}$: predicted F_G value of the substrate with the perpetrator, $F_{G,control}$: predicted F_G value of the substrate in the control

a: AUC_{inf} was used according to the report with the observed values by Templeton et al. (2010).

b: AUC_{0-24} was used according to the report with the observed values by Rengelshausen et al. (2003).

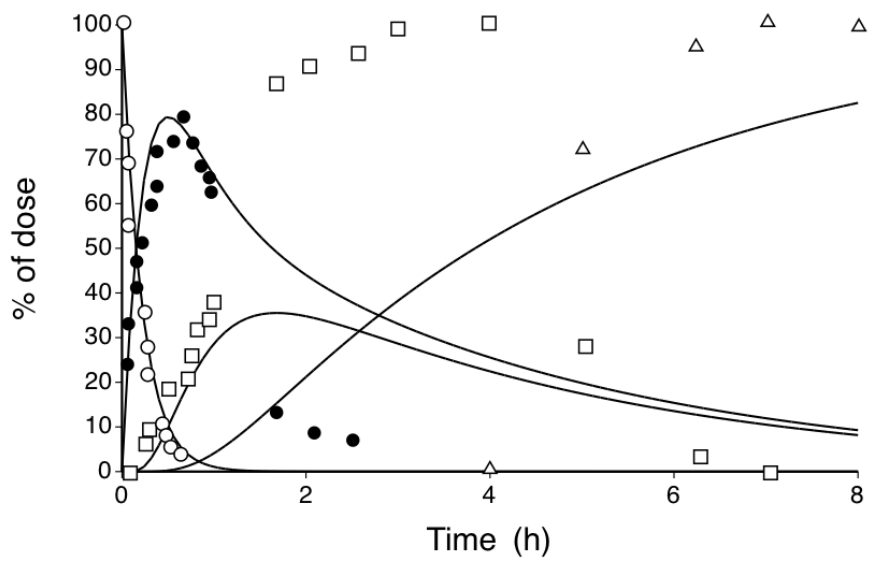
Supplementary Figures

Supplemental Fig. 1

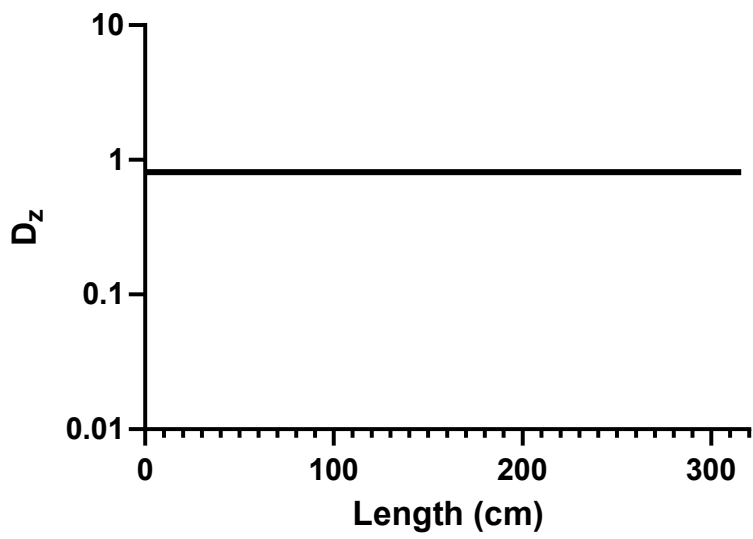


Supplemental Fig. 2

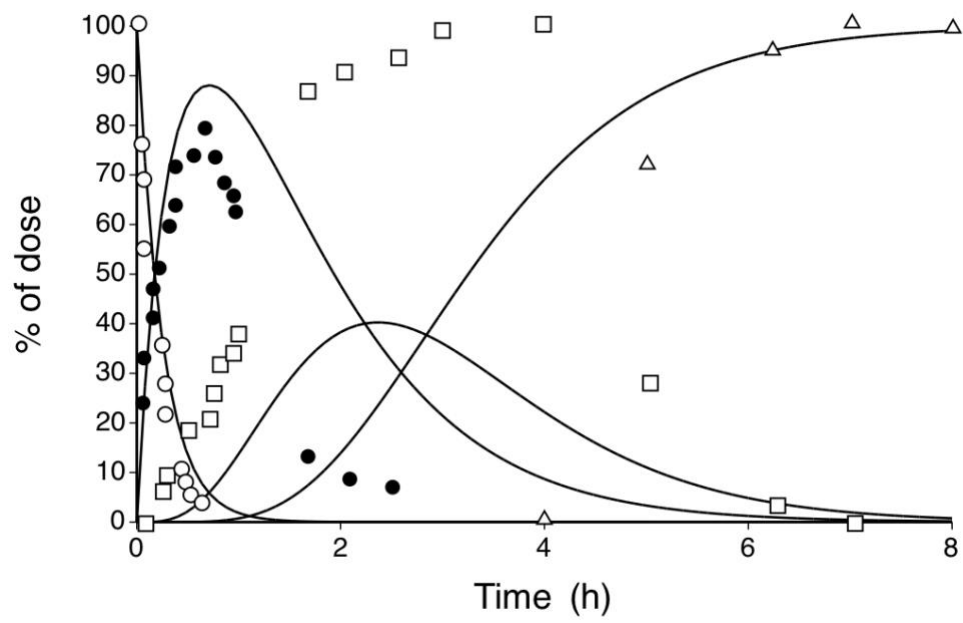
(A)



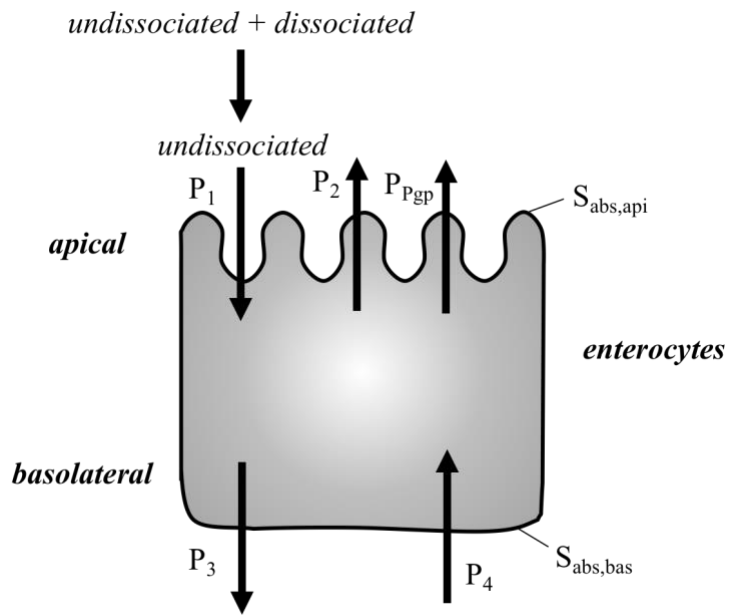
(B)



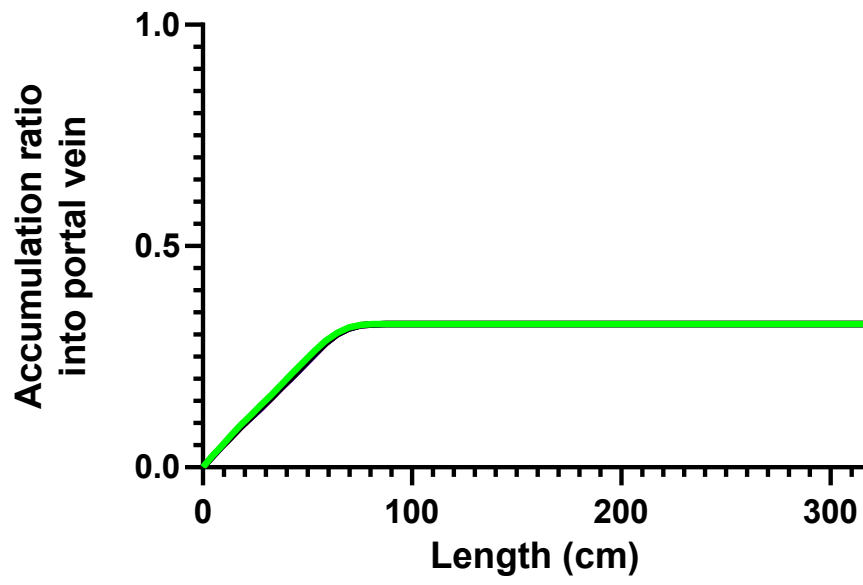
Supplemental Fig. 3



Supplemental Fig. 4

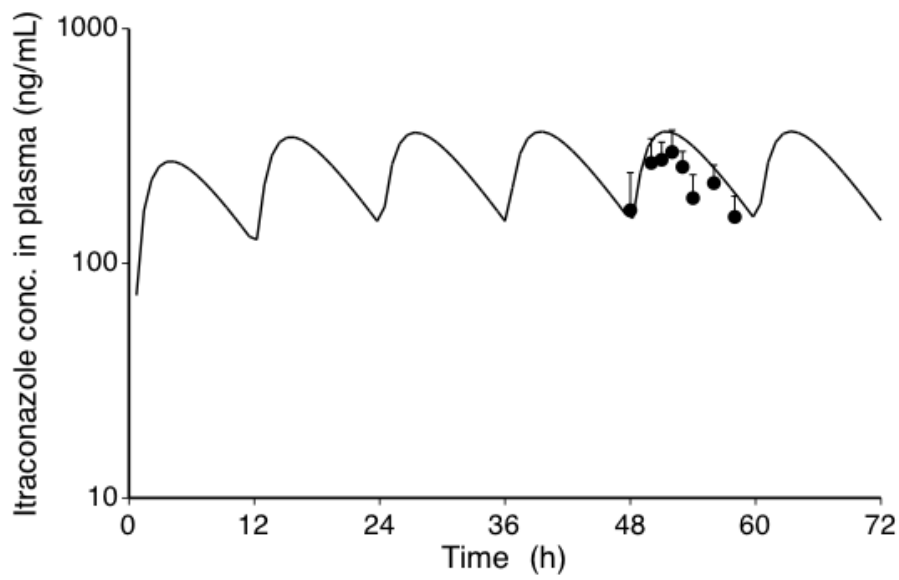


Supplemental Fig. 5



Supplemental Fig. 6

(A)



(B)

